# Exhibit N

#### 13.2.5 Industrial Wind Erosion

#### 13.2.5.1 General<sup>1-3</sup>

Dust emissions may be generated by wind erosion of open aggregate storage piles and exposed areas within an industrial facility. These sources typically are characterized by nonhomogeneous surfaces impregnated with nonerodible elements (particles larger than approximately 1 centimeter [cm] in diameter). Field testing of coal piles and other exposed materials using a portable wind tunnel has shown that (a) threshold wind speeds exceed 5 meters per second (m/s) (11 miles per hour [mph]) at 15 cm above the surface or 10 m/s (22 mph) at 7 m above the surface, and (b) particulate emission rates tend to decay rapidly (half-life of a few minutes) during an erosion event. In other words, these aggregate material surfaces are characterized by finite availability of erodible material (mass/area) referred to as the erosion potential. Any natural crusting of the surface binds the erodible material, thereby reducing the erosion potential.

#### 13.2.5.2 Emissions And Correction Parameters

If typical values for threshold wind speed at 15 cm are corrected to typical wind sensor height (7 - 10 m), the resulting values exceed the upper extremes of hourly mean wind speeds observed in most areas of the country. In other words, mean atmospheric wind speeds are not sufficient to sustain wind erosion from flat surfaces of the type tested. However, wind gusts may quickly deplete a substantial portion of the erosion potential. Because erosion potential has been found to increase rapidly with increasing wind speed, estimated emissions should be related to the gusts of highest magnitude.

The routinely measured meteorological variable that best reflects the magnitude of wind gusts is the fastest mile. This quantity represents the wind speed corresponding to the whole mile of wind movement that has passed by the 1 mile contact anemometer in the least amount of time. Daily measurements of the fastest mile are presented in the monthly Local Climatological Data (LCD) summaries. The duration of the fastest mile, typically about 2 minutes (for a fastest mile of 30 mph), matches well with the half-life of the erosion process, which ranges between 1 and 4 minutes. It should be noted, however, that peak winds can significantly exceed the daily fastest mile.

The wind speed profile in the surface boundary layer is found to follow a logarithmic distribution:

$$u(z) = \frac{u*}{0.4} \quad \ln \frac{z}{z_0} \qquad (z > z_0)$$
(1)

where:

u = wind speed, cm/s

- $u^* =$  friction velocity, cm/s
- z = height above test surface, cm
- $z_0$  = roughness height, cm 0.4 = von Karman's constant, dimensionless

The friction velocity  $(u^*)$  is a measure of wind shear stress on the erodible surface, as determined from the slope of the logarithmic velocity profile. The roughness height  $(z_0)$  is a measure of the roughness of the exposed surface as determined from the y intercept of the velocity profile, i. e., the height at which the wind speed is zero. These parameters are illustrated in Figure 13.2.5-1 for a roughness height of 0.1 cm.

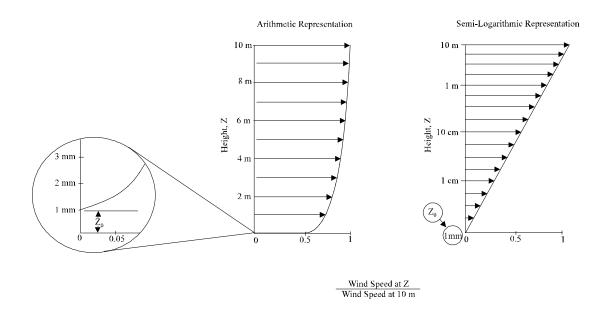


Figure 13.2.5-1. Illustration of logarithmic velocity profile.

Emissions generated by wind erosion are also dependent on the frequency of disturbance of the erodible surface because each time that a surface is disturbed, its erosion potential is restored. A disturbance is defined as an action that results in the exposure of fresh surface material. On a storage pile, this would occur whenever aggregate material is either added to or removed from the old surface. A disturbance of an exposed area may also result from the turning of surface material to a depth exceeding the size of the largest pieces of material present.

#### 13.2.5.3 Predictive Emission Factor Equation<sup>4</sup>

The emission factor for wind-generated particulate emissions from mixtures of erodible and nonerodible surface material subject to disturbance may be expressed in units of grams per square meter  $(g/m^2)$  per year as follows:

Emission factor = k 
$$\sum_{i=1}^{N} P_i$$
 (2)

where:

- k = particle size multiplier
- N = number of disturbances per year
- $P_i$  = erosion potential corresponding to the observed (or probable) fastest mile of wind for the ith period between disturbances, g/m<sup>2</sup>

The particle size multiplier (k) for Equation 2 varies with aerodynamic particle size, as follows:

Aerodynamic Particle Size Multipliers For Equation 2				
30 µm	<15 µm	<10 µm	<2.5 µm	
1.0	0.6	0.5	0.075 <sup>a</sup>	

a Multiplier for < 2.5 um taken from Reference 11.

This distribution of particle size within the under 30 micrometer ( $\mu$ m) fraction is comparable to the distributions reported for other fugitive dust sources where wind speed is a factor. This is illustrated, for example, in the distributions for batch and continuous drop operations encompassing a number of test aggregate materials (see Section 13.2.4).

In calculating emission factors, each area of an erodible surface that is subject to a different frequency of disturbance should be treated separately. For a surface disturbed daily, N = 365 per year, and for a surface disturbance once every 6 months, N = 2 per year.

The erosion potential function for a dry, exposed surface is:

$$P = 58 (u^* - u_t^*)^2 + 25 (u^* - u_t^*)$$

$$P = 0 \text{ for } u^* \le u_t^*$$
(3)

where:

u<sup>\*</sup> = friction velocity (m/s) u<sub>t</sub> = threshold friction velocity (m/s)

Because of the nonlinear form of the erosion potential function, each erosion event must be treated separately.

Equations 2 and 3 apply only to dry, exposed materials with limited erosion potential. The resulting calculation is valid only for a time period as long or longer than the period between disturbances. Calculated emissions represent intermittent events and should not be input directly into dispersion models that assume steady-state emission rates.

For uncrusted surfaces, the threshold friction velocity is best estimated from the dry aggregate structure of the soil. A simple hand sieving test of surface soil can be used to determine the mode of the surface aggregate size distribution by inspection of relative sieve catch amounts, following the procedure described below.

#### FIELD PROCEDURE FOR DETERMINATION OF THRESHOLD FRICTION VELOCITY (from a 1952 laboratory procedure published by W. S. Chepil):

- 1. Prepare a nest of sieves with the following openings: 4 mm, 2 mm, 1 mm, 0.5 mm, and 0.25 mm. Place a collector pan below the bottom (0.25 mm) sieve.
- 2. Collect a sample representing the surface layer of loose particles (approximately 1 cm in depth, for an encrusted surface), removing any rocks larger than about 1 cm in average physical diameter. The area to be sampled should be not less than 30 cm by 30 cm.
- 3. Pour the sample into the top sieve (4-mm opening), and place a lid on the top.
- 4. Move the covered sieve/pan unit by hand, using a broad circular arm motion in the horizontal plane. Complete 20 circular movements at a speed just necessary to achieve some relative horizontal motion between the sieve and the particles.
- 5. Inspect the relative quantities of catch within each sieve, and determine where the mode in the aggregate size distribution lies, i. e., between the opening size of the sieve with the largest catch and the opening size of the next largest sieve.
- 6. Determine the threshold friction velocity from Table 13.2.5-1.

The results of the sieving can be interpreted using Table 13.2.5-1. Alternatively, the threshold friction velocity for erosion can be determined from the mode of the aggregate size distribution using the graphical relationship described by Gillette.<sup>5-6</sup> If the surface material contains nonerodible elements that are too large to include in the sieving (i. e., greater than about 1 cm in diameter), the effect of the elements must be taken into account by increasing the threshold friction velocity.<sup>10</sup>

Tyler Sieve No.	Opening (mm)	Midpoint (mm)	$u_t^*$ (cm/s)
5	4		
9	2	3	100
16	1	1.5	76
32	0.5	0.75	58
60	0.25	0.375	43

# Table 13.2.5-1 (Metric Units). FIELD PROCEDURE FOR DETERMINATION OF THRESHOLD FRICTION VELOCITY

Threshold friction velocities for several surface types have been determined by field measurements with a portable wind tunnel. These values are presented in Table 13.2.5-2.

	Threshold Friction			nd Velocity At n (m/s)
Material	Velocity (m/s)	Roughness Height (cm)	z <sub>o</sub> = Act	$z_{0} = 0.5 \text{ cm}$
Overburden <sup>a</sup>	1.02	0.3	21	19
Scoria (roadbed material) <sup>a</sup>	1.33	0.3	27	25
Ground coal (surrounding coal pile) <sup>a</sup>	0.55	0.01	16	10
Uncrusted coal pile <sup>a</sup>	1.12	0.3	23	21
Scraper tracks on coal pile <sup>a,b</sup>	0.62	0.06	15	12
Fine coal dust on concrete pad <sup>c</sup>	0.54	0.2	11	10

Table 13.2.5-2 (Metric Units). THRESHOLD FRICTION VELOCITIES

<sup>a</sup> Western surface coal mine. Reference 2.

<sup>b</sup> Lightly crusted.

<sup>c</sup> Eastern power plant. Reference 3.

The fastest mile of wind for the periods between disturbances may be obtained from the monthly LCD summaries for the nearest reporting weather station that is representative of the site in question.<sup>7</sup> These summaries report actual fastest mile values for each day of a given month. Because the erosion potential is a highly nonlinear function of the fastest mile, mean values of the fastest mile are inappropriate. The anemometer heights of reporting weather stations are found in Reference 8, and should be corrected to a 10-m reference height using Equation 1.

To convert the fastest mile of wind  $(u^+)$  from a reference anemometer height of 10 m to the equivalent friction velocity  $(u^*)$ , the logarithmic wind speed profile may be used to yield the following equation:

$$u^* = 0.053 u_{10}^+$$
 (4)

where:

u<sup>\*</sup> = friction velocity (m/s)

 $u_{10}^{+}$  = fastest mile of reference anemometer for period between disturbances (m/s)

This assumes a typical roughness height of 0.5 cm for open terrain. Equation 4 is restricted to large relatively flat piles or exposed areas with little penetration into the surface wind layer.

If the pile significantly penetrates the surface wind layer (i. e., with a height-to-base ratio exceeding 0.2), it is necessary to divide the pile area into subareas representing different degrees of exposure to wind. The results of physical modeling show that the frontal face of an elevated pile is exposed to wind speeds of the same order as the approach wind speed at the top of the pile.

For 2 representative pile shapes (conical and oval with flattop, 37-degree side slope), the ratios of surface wind speed  $(u_s)$  to approach wind speed  $(u_r)$  have been derived from wind tunnel studies.<sup>9</sup> The results are shown in Figure 13.2.5-2 corresponding to an actual pile height of 11 m, a reference (upwind) anemometer height of 10 m, and a pile surface roughness height ( $z_0$ ) of 0.5 cm. The measured surface winds correspond to a height of 25 cm above the surface. The area fraction within each contour pair is specified in Table 13.2.5-3.

	Percent Of Pile Surface Area						
Pile Subarea	Pile A	Pile B1	Pile B2	Pile B3			
0.2a	5	5	3	3			
0.2b	35	2	28	25			
0.2c	NA	29	NA	NA			
0.6a	48	26	29	28			
0.6b	NA	24	22	26			
0.9	12	14	15	14			
1.1	NA	NA	3	4			

Table 13.2.5-3. SUBAREA DISTRIBUTION FOR REGIMES OF u<sub>s</sub>/u<sub>r</sub><sup>a</sup>

<sup>a</sup> NA = not applicable.

The profiles of  $u_s/u_r$  in Figure 13.2.5-2 can be used to estimate the surface friction velocity distribution around similarly shaped piles, using the following procedure:

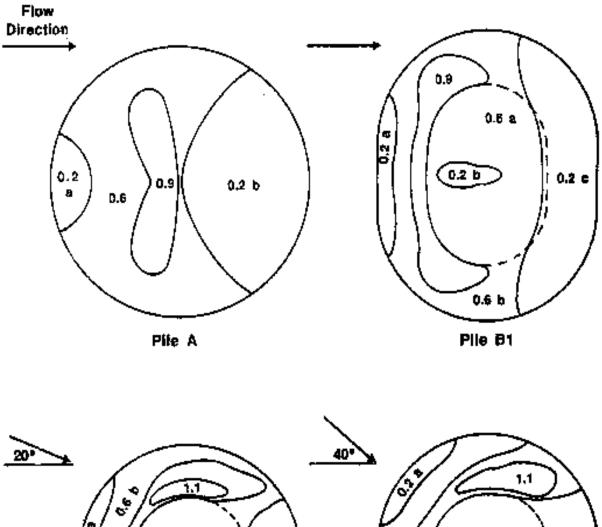
1. Correct the fastest mile value  $(u^+)$  for the period of interest from the anemometer height (z) to a reference height of 10 m  $u_{10}^+$  using a variation of Equation 1:

$$u_{10}^{+} = u^{+} \frac{\ln (10/0.005)}{\ln (z/0.005)}$$
(5)

where a typical roughness height of 0.5 cm (0.005 m) has been assumed. If a site-specific roughness height is available, it should be used.

2. Use the appropriate part of Figure 13.2.5-2 based on the pile shape and orientation to the fastest mile of wind, to obtain the corresponding surface wind speed distribution  $(u_s^+)$ 

$$u_{s}^{+} = \frac{(u_{s})}{u_{r}} \qquad u_{10}^{+}$$
 (6)



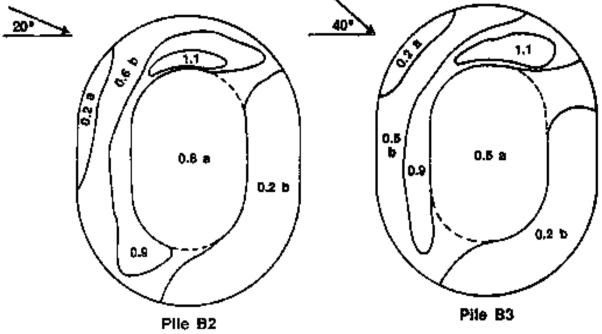


Figure 13.2.5-2. Contours of normalized surface windspeeds,  $u_s/u_r$ .

3. For any subarea of the pile surface having a narrow range of surface wind speed, use a variation of Equation 1 to calculate the equivalent friction velocity  $(u^*)$ :

$$u^{*} = \frac{0.4 u_{s}^{+}}{\frac{25}{\ln 0.5}} = 0.10 u_{s}^{+}$$
(7)

From this point on, the procedure is identical to that used for a flat pile, as described above.

Implementation of the above procedure is carried out in the following steps:

- 1. Determine threshold friction velocity for erodible material of interest (see Table 13.2.5-2 or determine from mode of aggregate size distribution).
- 2. Divide the exposed surface area into subareas of constant frequency of disturbance (N).
- 3. Tabulate fastest mile values  $(u^+)$  for each frequency of disturbance and correct them to 10 m  $(u^+)$  using Equation 5.5
- 4. Convert fastest mile values  $(u_{10})$  to equivalent friction velocities  $(u^*)$ , taking into account (a) the uniform wind exposure of nonelevated surfaces, using Equation 4, or (b) the nonuniform wind exposure of elevated surfaces (piles), using Equations 6 and 7.
- 5. For elevated surfaces (piles), subdivide areas of constant N into subareas of constant  $u^*$  (i. e., within the isopleth values of  $u_s/u_r$  in Figure 13.2.5-2 and Table 13.2.5-3) and determine the size of each subarea.
- 6. Treating each subarea (of constant N and  $u^*$ ) as a separate source, calculate the erosion potential (P<sub>i</sub>) for each period between disturbances using Equation 3 and the emission factor using Equation 2.
- 7. Multiply the resulting emission factor for each subarea by the size of the subarea, and add the emission contributions of all subareas. Note that the highest 24-hour (hr) emissions would be expected to occur on the windiest day of the year. Maximum emissions are calculated assuming a single event with the highest fastest mile value for the annual period.

The recommended emission factor equation presented above assumes that all of the erosion potential corresponding to the fastest mile of wind is lost during the period between disturbances. Because the fastest mile event typically lasts only about 2 minutes, which corresponds roughly to the half-life for the decay of actual erosion potential, it could be argued that the emission factor overestimates particulate emissions. However, there are other aspects of the wind erosion process that offset this apparent conservatism:

- 1. The fastest mile event contains peak winds that substantially exceed the mean value for the event.
- 2. Whenever the fastest mile event occurs, there are usually a number of periods of

slightly lower mean wind speed that contain peak gusts of the same order as the fastest mile wind speed.

Of greater concern is the likelihood of overprediction of wind erosion emissions in the case of surfaces disturbed infrequently in comparison to the rate of crust formation.

13.2.5.4 Example 1: Calculation for wind erosion emissions from conically shaped coal pile

A coal burning facility maintains a conically shaped surge pile 11 m in height and 29.2 m in base diameter, containing about 2000 megagrams (Mg) of coal, with a bulk density of 800 kilograms per cubic meter (kg/m<sup>3)</sup> (50 pounds per cubic feet [lb/ft<sup>3</sup>]). The total exposed surface area of the pile is calculated as follows:

Coal is added to the pile by means of a fixed stacker and reclaimed by front-end loaders operating

$$S = \pi r \sqrt{r^2 + h^2}$$
  
= 3.14(14.6) $\sqrt{(14.6)^2 + (11.0)^2}$   
= 838 m<sup>2</sup>

at the base of the pile on the downwind side. In addition, every 3 days 250 Mg (12.5 percent of the stored capacity of coal) is added back to the pile by a topping off operation, thereby restoring the full capacity of the pile. It is assumed that (a) the reclaiming operation disturbs only a limited portion of the surface area where the daily activity is occurring, such that the remainder of the pile surface remains intact, and (b) the topping off operation creates a fresh surface on the entire pile while restoring its original shape in the area depleted by daily reclaiming activity.

Because of the high frequency of disturbance of the pile, a large number of calculations must be made to determine each contribution to the total annual wind erosion emissions. This illustration will use a single month as an example.

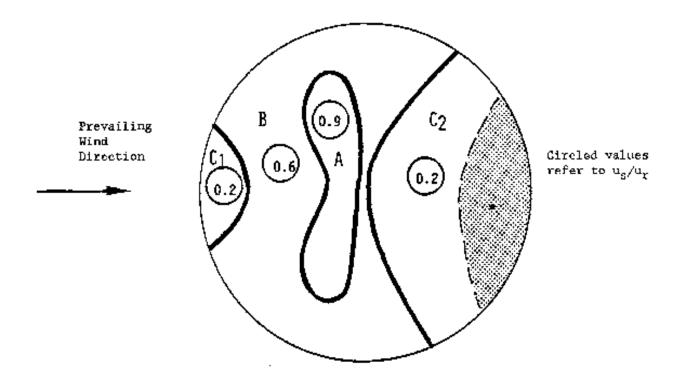
<u>Step 1</u>: In the absence of field data for estimating the threshold friction velocity, a value of 1.12 m/s is obtained from Table 13.2.5-2.

<u>Step 2</u>: Except for a small area near the base of the pile (see Figure 13.2.5-3), the entire pile surface is disturbed every 3 days, corresponding to a value of N = 120 per year. It will be shown that the contribution of the area where daily activity occurs is negligible so that it does not need to be treated separately in the calculations.

<u>Step 3</u>: The calculation procedure involves determination of the fastest mile for each period of disturbance. Figure 13.2.5-4 shows a representative set of values (for a 1-month period) that are assumed to be applicable to the geographic area of the pile location. The values have been separated into 3-day periods, and the highest value in each period is indicated. In this example, the anemometer height is 7 m, so that a height correction to 10 m is needed for the fastest mile values. From Equation 5,

$$u_{10}^{+} = u_{7}^{+} \left( \frac{\ln (10/0.005)}{\ln (7/0.005)} \right)$$
$$u_{10}^{+} = 1.05 u_{7}^{+}$$

<u>Step 4</u>: The next step is to convert the fastest mile value for each 3-day period into



\* A portion of  ${\rm G}_2$  is disturbed daily by reclaiming activities.

	$\frac{10}{A} \qquad \frac{u_r}{0.9}$	Pile_Surface				
Area ID	-u <u>s</u> -u <u>r</u>	X	Are	a (m <sup>2</sup> )		
A	0.9	12		101		
В	0.6	48		402		
c <sub>1</sub> + c <sub>2</sub>	0.2	40		<u>335</u>		
			Total	838		

Figure 13.2.5-3. Example 1: Pile surface areas within each wind speed regime.

**EMISSION FACTORS** 

	Mon	thly Sum	nary		
		Wind			
			Fas M		
5 Resultant Dir.	Resultant F Speed M.P.H.	Average Speed ص M.P.H.	16 Speed M.P.H.	17 Direction	Date
30	5.3	6.9	9	36	1
01	10.5	10.6	(14)	01	2
10	2.4	6.0	10	02	3
13	11.0	11.4	16	13	4
12	11.3	11.9	15	11	5
20	11.1	19.0	(29)	30	6
29	19.6	19.8	(30)	30	7
29	10.9	11.2	17	30	8
22	3.0	8.1	15	13	9
14	14.6	15.1	23	12 29	
29	22.3 7.9	23.3 13.5	$\begin{array}{c} (31) \\ 23 \end{array}$	29 17	11
17 21	7.9	15.5	18	17	12
$\frac{21}{10}$	4.5	9.6	(22)	13	
10	6.7	8.8	13	11	15
01	13.7	13.8	(21)	36	16
33	11.2	11.5	15	34	17
27	4.3	5.8	12	31	18
32	9.3	10.2	14	35	19
24	7.5	7.8	(16)	24	20
22	10.3	10.6	16	20	21
32	17.1	17.3	25	32	22
29	2.4	8.5	14	13	23
07	5.9	8.8	15	02	24
34	11.3	11.7	(17)	32	25
31	12.1	12.2	16	32	26
30	8.3	8.5	16	26 22	
30	8.2	8.3	(13)	32	
33	5.0	6.6 5.2	10	32 31	29
34 29	3.1 4.9	5.2 5.5	9 8	25	30
29	т.2	For the l		23	51
30	3.3	11.1	31	29	



Figure 13.2.5-4. Example daily fastest miles wind for periods of interest.

equivalent friction velocities for each surface wind regime (i. e.,  $u_s/u_r$  ratio) of the pile, using Equations 6 and 7. Figure 13.2.5-3 shows the surface wind speed pattern (expressed as a fraction of the approach wind speed at a height of 10 m). The surface areas lying within each wind speed regime are tabulated below the figure.

The calculated friction velocities are presented in Table 13.2.5-4. As indicated, only 3 of the periods contain a friction velocity which exceeds the threshold value of 1.12 m/s for an uncrusted coal pile. These 3 values all occur within the  $u_s/u_r = 0.9$  regime of the pile surface.

	u <sub>7</sub> +		$u^+_{10}$		$u^{*} = 0.1u^{+} (m/s)$		
3-Day Period	mph	m/s	mph	m/s	u <sub>s</sub> /u <sub>r</sub> : 0.2	u <sub>s</sub> /u <sub>r</sub> : 0.6	u <sub>s</sub> /u <sub>r</sub> : 0.9
1	14	6.3	15	6.6	0.13	0.40	0.59
2	29	13.0	31	13.7	0.27	0.82	1.23
3	30	13.4	32	14.1	0.28	0.84	1.27
4	31	13.9	33	14.6	0.29	0.88	1.31
5	22	9.8	23	10.3	0.21	0.62	0.93
6	21	9.4	22	9.9	0.20	0.59	0.89
7	16	7.2	17	7.6	0.15	0.46	0.68
8	25	11.2	26	11.8	0.24	0.71	1.06
9	17	7.6	18	8.0	0.16	0.48	0.72
10	13	5.8	14	6.1	0.12	0.37	0.55

#### Table 13.2.5-4 (Metric And English Units). EXAMPLE 1: CALCULATION OF FRICTION VELOCITIES

<u>Step 5</u>: This step is not necessary because there is only 1 frequency of disturbance used in the calculations. It is clear that the small area of daily disturbance (which lies entirely within the  $u_s/u_r = 0.2$  regime) is never subject to wind speeds exceeding the threshold value.

<u>Steps 6 and 7</u>: The final set of calculations (shown in Table 13.2.5-5) involves the tabulation and summation of emissions for each disturbance period and for the affected subarea. The erosion potential (P) is calculated from Equation 3.

For example, the calculation for the second 3-day period is:

$$P = 58(u^* - u_t^*)^2 + 25(u^* - u_t^*)$$
$$P_2 = 58(1.23 - 1.12)^2 + 25(1.23 - 1.12)$$
$$= 0.70 + 2.75 = 3.45 \text{ g/m}^2$$

**EMISSION FACTORS** 

3-Day Period	u <sup>*</sup> (m/s)	u* - u <sub>t</sub> * (m/s)	P (g/m <sup>2</sup> )	ID	Pile Surface Area (m <sup>2</sup> )	kPA (g)
2	1.23	0.11	3.45	А	101	170
3	1.27	0.15	5.06	А	101	260
4	1.31	0.19	6.84	А	101	350
TOTAL						780

Table 13.2.5-5 (Metric Units). EXAMPLE 1: CALCULATION OF PM-10 EMISSIONS<sup>a</sup>

<sup>a</sup> Where  $u_t^* = 1.12$  m/s for uncrusted coal and k = 0.5 for PM-10.

The emissions of particulate matter greater than 10  $\mu$ m (PM-10) generated by each event are found as the product of the PM-10 multiplier (k = 0.5), the erosion potential (P), and the affected area of the pile (A).

As shown in Table 13.2.5-5, the results of these calculations indicate a monthly PM-10 emission total of 780 g.

13.2.5.5 Example 2: Calculation for wind erosion from flat area covered with coal dust

A flat circular area 29.2 m in diameter is covered with coal dust left over from the total reclaiming of a conical coal pile described in the example above. The total exposed surface area is calculated as follows:

s =  $\frac{\pi}{4}$  d<sup>2</sup> = 0.785 (29.2)<sup>2</sup> = 670 m<sup>2</sup>

This area will remain exposed for a period of 1 month when a new pile will be formed.

<u>Step 1</u>: In the absence of field data for estimating the threshold friction velocity, a value of 0.54 m/s is obtained from Table 13.2.5-2.

<u>Step 2</u>: The entire surface area is exposed for a period of 1 month after removal of a pile and N = 1/yr.

<u>Step 3</u>: From Figure 13.2.5-4, the highest value of fastest mile for the 30-day period (31 mph) occurs on the 11th day of the period. In this example, the reference anemometer height is 7 m, so that a height correction is needed for the fastest mile value. From Step 3 of the previous example,  $u_{10}^+ = 1.05 u^+$ , so that  $u^+_{\overline{10}} 33$  mph.

<u>Step 4</u>: Equation 4 is used to convert the fastest mile value of 14.6 m/s (33 mph) to an equivalent friction velocity of 0.77 m/s. This value exceeds the threshold friction velocity from Step 1 so that erosion does occur.

<u>Step 5</u>: This step is not necessary, because there is only 1 frequency of disturbance for the entire source area.

<u>Steps 6 and 7</u>: The PM-10 emissions generated by the erosion event are calculated as the product of the PM-10 multiplier (k = 0.5), the erosion potential (P) and the source area (A). The erosion potential is calculated from Equation 3 as follows:

$$P = 58(u^* - u_t^*)^2 + 25(u^* - u_t^*)$$

$$P = 58(0.77 - 0.54)^2 + 25(0.77 - 0.54)$$

$$= 3.07 + 5.75$$

$$= 8.82 \text{ g/m}^2$$

Thus the PM-10 emissions for the 1-month period are found to be:

$$E = (0.5)(8.82 \text{ g/m}^2)(670 \text{ m}^2)$$
$$= 3.0 \text{ kg}$$

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11. C. Cowherd, *Background Document for Revisions to Fine Fraction Ratios Used for AP-42 Fugitive Dust Emission Factors.* Prepared by Midwest Research Institute for Western Governors Association, Western Regional Air Partnership, Denver, CO, February 1, 2006.

# Exhibit O



# CONSTRUCTION PERMIT APPLICATION FOR A FEDERALLY ENFORCEABLE STATE OPERATING PERMIT (FESOP) SOURCE

DTE CHICAGO FUELS TERMINAL, LLC 10730 SOUTH BURLEY AVENUE CHICAGO, ILLINOIS

DISCLAIMER: SOME FORMATTING CHANGES MAY HAVE OCCURRED WHEN THE ORIGINAL DOCUMENT WAS PRINTED TO PDF; HOWEVER, THE ORIGINAL CONTENT REMAINS UNCHANGED.

SEPTEMBER 2012 Ref. no. 052450 (2) Prepared by: Conestoga-Rovers & Associates

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Worldwide Engineering, Environmental, Construction, and IT Services

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## 1.0 **PROJECT NARRATIVE**

On February 13, 2008, the Illinois Environmental Protection Agency (IEPA) Bureau of Air (Agency) issued a Joint Construction and Operating Permit to DTE Chicago Fuels Terminal, LLC (DTE), Permit #07050082, ID# 031600CSF, for its facility located at 10730 South Burley Avenue in Chicago, Illinois (Facility). In this permit, the Agency determined that this Facility has potential to emit (PTE) more than 100 tons per year (ton/yr) of particulate matter of less than ten microns ( $PM_{10}$ ).

DTE filed a Federally Enforceable State Operating Permit (FESOP) application on February 2, 2009 and this application is still under review by the Agency. The FESOP application was deemed complete by the IEPA per the May 12, 2009 CAAPP Application Completeness Determination Letter. The purpose of this application is to request a modification to Construction Permit #07050082 issued on May 21, 2009 to allow the installation of additional equipment. DTE also requests that the FESOP application be updated to include the limitations contained in this application.

DTE proposes to construct four portable conveyors, fourteen storage piles, one 100-Horsepower (HP) air compressor, and five 15-HP light standards. Emissions from the 14 storage piles are fugitive and are not included in the 197-FEE form. The air compressor and five light standards are exempt from permitting under 35 IAC 201.146(i) are not included in the 197-FEE form.

Emissions from the proposed emission units including existing emission units are contained in Tables 1-12. Table 13 provides a listing of all emission units at the Facility.

In the permit application received by the IEPA on August 15, 2008, we noted that, upon review of Section 39.5 (2)(c)(ii) of the Illinois Environmental Protection Act (Act), the Facility is not one of the 28 categories of stationary sources listed there and is not subject to a standards promulgated under Section 111 or 112 of the Clean Air Act which would require them to include fugitive emissions. Therefore, the PTE does not include fugitive emissions.

DTE requests a control efficiency of 50% for the control of particulate matter using a water suppression system.

A list of State Rules and an applicability determination for each Rule are as follows:

212.123 – Visible Emissions Limitations for All Other Emission Units The source will achieve compliance through the Fugitive Dust Plan. 35 IAC Section 212.301 – Fugitive Particulate Matter The source will not allow fugitive particulate matter to leave the source's boundaries. This will be accomplished through control practices in the Fugitive Dust Plan.

35 IAC Section 212.302 – Fugitive Particulate Matter The source is located in Cook County, Illinois therefore it is subject to 35 IAC Sections 212.304 – 212.310 and 212.312.

35 IAC Section 212.304 – Storage Piles The storage piles located at the source will be sprayed with water via a water cannon to control fugitive dust emissions. The piles will be sprayed on an as needed basis.

35 IAC Section 212.305 – Conveyor Loading Operations The inherent moisture content of the coal/pet coke, telescoping chutes, and water suppression will provide adequate control for particulate matter emissions.

35 IAC Section 212.306 – Traffic Areas The source operates a water truck for dust suppression on traffic areas. The traffic areas will be sprayed with water on an as needed basis.

35 IAC Section 212.307 – Materials Collected By Pollution Control Equipment The source will recycle the coal/ pet coke dust collected in the dust collectors located at the facility.

35 IAC Section 212.308 – Spraying or Choke-Feeding Required The inherent moisture content of the coal/ pet coke and water suppression will provide adequate control for particulate matter emissions for all of the emission points at the facility except for the pet coke rail unloading operations which will employ choke loading to reduce particulate matter emissions.

35 IAC Section 212.309 – Operating Program A Fugitive Dust Plan has been created/updated.

35 IAC Section 212.310 – Minimum Operating Program The data is included in this Fugitive Dust Plan.

35 IAC Section 212.312 – Amendment to Operating Program A Fugitive Dust Plan has been created/updated to include the operating scenario at the Facility. If the Facility changes their operating scenario an amendment to the Operating Program will be submitted to the Agency.

35 IAC Section 212.316– Emission Limitations for Emission Units in Certain Areas The source, which is subject to the requirements set forth in this Section, will, as discussed in this Fugitive Dust Plan, maintain compliance with the limitations in this Section. Regarding the crushing and screening operations, it has been stated that the inherent moisture content of the materials being processed will provide adequate control of particulate matter emissions. The roadways will be sprayed with water on an as needed basis to control fugitive dust emissions. Water cannons will be used to control fugitive particulate matter emissions from the storage piles. The source will maintain records and provide reports as outlined in 35 IAC Section 212.316 (g).

35 IAC Section 212.321 – Process Emission Units for Which Construction or Modification Commenced on or After April 14, 1972.

To show compliance with the process weight rate rule a sample calculation is contained below using the throughput of a single transfer point.

 $E = A(P)^{B}$ 

Where: P = Process Weight Rate; and E = Allowable Emission Rate

 $E = 2.54(2500)^{0.531}$ 

E = 165.70 pounds per hour

The actual emissions from this transfer point are 0.79 pound per hour. Therefore, the source is in compliance with the Process Weight Rate Rule.

35 IAC Section 212.324 – Process Emission Units in Certain Areas The source is subject to the requirements in this section. See the response to 35 IAC Section 212.316.

The diesel fuel-fired engines are subject to 40 Code of Federal Regulations (CFR) Part 60 Subpart IIII. The source will comply with the requirements through the following:

40 CFR 60.4204 – Emission Standards for Non-Emergency Engines Manufacturer's certification.

40 CFR 60.4207 – Fuel Requirements for Non-Emergency Engines DTE will only use compliant fuels in the engines.

40 CFR 60.4209 – Monitoring Requirements for Non-Emergency Engines The use of a non-resettable hour meter.

40 CFR 60.4211 – Compliance Requirements for Non-Emergency Engines Manufacturer's certification.

40 CFR 60.4212 – Test Method Requirements for Non-Emergency Engines DTE will test the engines in a manner consistent with the requirements set forth in this regulation. 40 CFR 60.4214 - Notification, Reporting, and Recordkeeping Requirements for Non-**Emergency Engines** 

DTE will track hour usage on a rolling monthly basis and track fuel quality by purchase receipts and will record routine maintenance activities.

The PTE calculations in Table 1 indicates that the source is major, but the limitations set forth in Table 8A support the fact that this source is a synthetic minor source.

The emissions contained in Table 8A are based on the maximum facility throughput level of 11,000,000 tons of coal and petroleum coke and 250,000 ton/yr of salt. Therefore, please use the emissions listed in the tables below to establish the allowable emissions for FESOP limitations and for fee purposes.

0.00101

0.00034

N/A

N/A

0.03

0.01

0.25

0.05

	Throi	ughput		n Factor ton)	Number of	PM Em	ussions	
Material Handled	ton/ month	ton/yr	PM	$PM_{10}$	Transfer Points	ton/ month	ton/yr	
Coal & Pet Coke	1,100,000	11,000,000	0.00064	0.0003	58	10.3	102.5	
Salt	25,000	250,000	0.00064	0.0003	34	0.14	1.1	

Transfer and Conveying, and Loadout – Requested Permit Limitations

29,400

29,400

The emission factors are based on material unloading, all possible transfer points located at the facility, and loadout. The emission factors are derived from AP 42 Section 13.2.4.3. There is also a 50% control efficiency taken into account in the emission calculations based on the use of water suppression.

0.0033

0.00067

The equation is a follows:

Incidental Soil

Crushing Incidental Soil

Screening

 $E = k(0.0032) \times ((U/5)^{-2}) / ((M/2)^{1.4})$ Coal and Coke Handling PM Emission Factor 0.74(0.0032) x ((10.3/5) -?) / (10%/2)<sup>1,4</sup>) = 0.00064 Coal and Coke Handling PM<sub>10</sub> Emission Factor - 0.35(0.0032) x ((10.3/5)<sup>1/3</sup>) / (10%/2)<sup>1/4</sup>) = 0.0003

Coal and Coke Handling PM Emissions were calculated via the following formula:

294,000

294,000

11,000,000 ton/yr x 0.00064 lb/ton x 50% control efficiency x 58 transfers / 2,000 lb/ton = 102.5 ton/yr 102.5 ton/yr / 10 months = 10.3 ton/month

PM10 Emissions

ton/yr

48.5

0.6

0.08

0.03

ton/ month

4.9

0.06

0.01

0.01

	Emission Factor		_	
Pollutant	lb/bhp-hr	lb/hr	ton/month	ton∕yr
NO <sub>X</sub>	0.015	1.77	1.12	11.15
CO	0.00815	0.96	0.61	6.06
SO <sub>2</sub>	**	0.021	0.013	0.13
РМ	0.0005	0.06	0.04	0.37
PM <sub>10</sub>	0.0005	0.06	0.04	0.37
νом	0.00033	0.04	0.03	0.25

118 HP Diesel Engine Emissions (Diesel Generators 1-3) – Requested Permit Limitations

This Table provides the emissions for DG (1, 3).

Emissions are based on 4,200 hours of operation per year for each unit, or 12,600 hr/yr total (three units). (118 HP x 0.015 lb/bhp-hr x 4,200 hr/yr / 2,000 lb/ton x 3 units = 11.15 ton/yr). Emission factors are from 40 CFR 89.112 Table 1.

\*\* 5O<sub>2</sub> emissions calculated using 40 CFR 60.4207 maximum sulfur content of 0.015% per gallon of fuel and a fuel consumption rate of 10 gallons of diesel fuel per hour per engine.

12,600 hr/yr x 10 gal/hr x 7.1 lb/gal x 0.015% S / 2,000 lb/gal x 64 MW of SO\_2/32 MW of S - 0.13 ton/yr

	Emission Factor	Umissions				
Pollutant	lb/bhp-hr	lb/hr	ton/month	ton/yr		
NO <sub>N</sub>	0.015	7.5	6.30	63.00		
CO	0.00573	2.86	2.41	24.05		
SO <sub>2</sub>	**	0.043	0.036	0.36		
РМ	0.0003	0.15	0.13	1.26		
PM <sub>10</sub>	0.0003	0.15	0.16	1.26		
VOM	0.00033	0.17	0.14	1.39		

500 HP Diesel Engine Emissions (Diesel Generators 4-7) – Requested Permit Limitations

This Table provides the emissions for DG-(4-7).

Emissions are based on 4,200 hours of operation per year for each unit, or 16,800  $\,\rm hr/yr$  total

 $(500 \text{ HP} \ge 0.015 \text{ lb/bhp-hr} \ge 4,200 \text{ hr/yr} / 2,000 \text{ lb/ton} \ge 4 \text{ units} = 63.00 \text{ ton/yr})$ 

Emission factors are from 40 CFR 89.112 Table 1.

\*\* 5O<sub>2</sub> emissions calculated using 40 CFR 60.4207 maximum sulfur content of 0.015% per gallon of fuel and a fuel consumption rate of 20 gallons of diesel fuel per hour per engine.

16,800 hr/yr x 20 gal/hr x 7.1 lb/gal x 0.015% S / 2,000 lb/gal x 64 MW of SO<sub>2</sub>/32 MW of 5 = 0.36 ton/yr

	Emission Factor	Emissions		
Pollutant	lb/bhp-hr	lb/hr	ton/month	ton/yr
NO <sub>X</sub>	0.015	1.50	0,99	3,15
CO	0.00815	0.82	0.38	1.71
SO <sub>2</sub>	××	0.02	0.004	0.04
РМ	0.0005	0.05	0.02	0.11
PM10	0.0005	0.05	0.02	0.11
VOM	0.00033	0.03	0.16	0.07

100 HP Diesel Engine Emissions (Air Compressor) – Requested Permit Limitations

This Table provides the emissions for AC-1.

Emissions are based on 4,200 hours of operation per year.

(100 HP x 0.015 lb/bhp hr x 4,200 hr/yr / 2,000 lb/ton = 3.15 tons/yr)

Emission factors are from 40 CFR 89.112 Table 1.

\*\* 5O<sub>2</sub> emissions calculated using 40 CFR 60.4207 maximum sulfur content of 0.15% per gallon of fuel and a fuel consumption rate of 10 gallons of diesel fuel per hour per engine.

4,200 hr/yr x 10 gal/hr x 7.1 lb/gal x 0.015% S / 2,000 lb/gal x 61 MW of  $\rm SO_2/32$ 

MW of 5 = 0.04 ton/yr

	Emission Factor	Emissions		
Pollutant	lb/bhp-hr	lb/lir	ton/month	ton/yr
NO <sub>X</sub>	0.015	0.23	0.11	2.36
CO	0.00903	0.12	0.06	1.28
SO <sub>2</sub>	**	0.01	0.011	0.11
РМ	0.001	0.01	0.007	0.08
PM <sub>ID</sub>	0.001	0.01	0.007	0.08
VOM	0.00033	0.005	0.02	0.05

15 HP Diesel Engine Emissions (Light Standards 1-5) – Requested Permit Limitations

This Table provides the emissions for LS 1(5).

Emissions are based on 4,200 hours of operation per year for each unit, or 21,000  $\,\rm hr/yr$  total

(15 HP x 0.015 lb/bhp hr x 3,500 hr/yr / 2,000 lb/ton x 5 units - 2.36 tons/yr)

Emission factors are from 40 CFR 89.112 Table 1.

\*\*  $SO_2$  emissions calculated using 40 CFR 60.4207 maximum sulfur content of 0.015% per gallon of fuel and a fuel consumption rate of 5 gallons of diesel fuel per hour per engine.

21,000 hr/yr x 5 gal/hr x 7.1 lb/gal x 0.015% S / 2,000 lb/gal x 64 MW of SO\_2/32 MW of S - 0.11 ton/yr

	Emission Factor	Emissions		
Pollutant	lb/bhp-hr	lb/hr	ton/month	ton/yr
NO <sub>X</sub>	0.015	0.3	0.01	0.08
co	0.01079	0.22	0.005	0.05
SO <sub>2</sub>	××	0.01	0.0003	0.003
РМ	0.0013	0.03	0.0007	0.01
PM12	0.0013	0.03	0.0007	0.01
VOM	0.00033	0.01	0.001	0.01

20 HP Diesel Engine Emissions (Emergency Water Pump) – Requested Permit Limitations

This Table provides the emissions for DWP 1.

Emissions are based on 500 hours of operation per year.

(20 HP x 0.015 lb/bhp-hr x 500 hr/yr / 2,000 lb/ton = 0.08 ton/yr)

Emission factors are from 40 CFR 89.112 Table 1.

\*\* 5O<sub>2</sub> emissions calculated using 40 CFR 60.4207maximum sulfur content of 0.015% per gallon of fuel and a fuel consumption rate of 5 gallons of diesel fuel per hour per engine.

500 hr/yr x 5 gal/hr x 7.1 lb/gal x 0.015% S / 2,000 lb/gal  $\ge$  64 MW of 5O<sub>2</sub>/32 MW of 5 = 0.003 ton/yr



Illinois Environmental Protection Agency Division Of Air Pollution Control -- Permit Section P.O. Box 19506 Springfield, Illinois 62794-9506

# **Construction Permit Application** For a FESOP Source (FORM APC628)

For Illinois EPA use only

(BOA)?

BOA ID No .:

Application No.:

Date Received:

This form is to be used to supply information to obtain a construction permit for a proposed project involving a Federally Enforceable State Operating Permit (FESOP) or Synthetic Minor source, including construction of a new FESOP source. Other necessary information must accompany this form as discussed in the "General Instructions For Permit Applications," Form APC-201

1. Working	Name of Pro	posed Project:									
Conveyo	r Addition										
2. Is the pro	ject occurrin	g at a source that already has a pe	ermi	t froi	m th	e Bi	urea	lu of	f Air (	(BO,	A)?
🗌 🗌 N(	X Yes	If Yes, provide BOA ID Number:	_0	_3	_1	6	0	0	G	S	F

3. Does this application request a revision to an existing construction permit issued by the BOA? X Yes If Yes, provide Permit Number: 0 7 0 5 0 0 8 No No - 2

4. Does this application request that the new/modified emission units be incorporated into an existing FESOP issued by the BOA? \*\*

No No Yes If Yes, provide Permit Number:

Source Information						
5. Source name:* DTE Chicago Fuels Terminal,	LLC					
<ol> <li>Source street address:* 10730 South Burley Avenue</li> </ol>						
7. City: Chicago	8. County: Cook		9. Zip code: 60617			
	THE FOLLOWING FOR	A SOURCE WITH	OUT AN ID NUMBER.			
	10. Is the source located within city limits?					
11. Description of source and pro	11. Description of source and product(s) produced:       12. Primary Classification Code of source:         SIC:					
13. Latitude (DD:MM:SS.SSSS):     14. Longitude (DD:MM:SS.SSSS):						
<sup>*</sup> If this information different than previous information, then complete a new Form 200-CAAPP to change the source name in initial FESOP application for the source or Form APC-620 for Air Permit Name and/or Ownership Change if the FESOP has been previously issued.						

Applicant Information					
15. Who is the applicant? 16. All correspondence to: (check one)					
🛛 Owner 🗌 Operator 🔛 Owner 🗌 Operator 📄 Source					
17. Applicant's FEIN:	18. Attention name and/or title for written correspondence:				
204570538	Donald Januszek				

\*\*The FESOP has not been issued yet.

This Agency is authorized to require and you must disclose this information under 415 ILCS 5/39. Failure to do so could result in the application being denied and penalties under 415 ILCS 5 et seq. It is not necessary to use this form in providing this information. This form has been approved by the forms management center.

IL 532-2865 APC628 9/07

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**APPLICATION PAGE 8** 

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Owner Information*						
19. Name: DTE Chicago Fuels Terminal, LLC						
20. Address:						
414 South Main Stree	414 South Main Street					
21. City: Ann Arbor	22. State: Michigan	23. Zip code: 48104				

\* If this information different than previous information, then complete Form 272-CAAPP for a Request for Ownership Change for CAAPP Permit for an initial FESOP application for the source or Form APC-620 for Air Permit Name and/or Ownership Change if the FESOP has been previously issued.

Operato	Operator Information (If Different from Owner)*					
24. Name DTE Chicago Fuels	•		,			
25. Address: 10730 South Burley	Avenue					
26. City: Chicago	27. State: Illinois		28. Zip code: 60617			
<ul> <li>If this information different than previous information, then complete a new Form 200-CAAPP to change the source name in initia FESOP application for the source or Form APC-620 for Air Permit Name and/or Ownership Change if the FESOP has been previously issued.</li> </ul>						
Те	chnical Contacts	for Applica	tion			
29. Preferred technical contact:	(check one) 🛛 🛛 Ap	oplicant's conta	act 🗌 Consultant			
30. Applicant's technical contac Donald Januszek	t person for application	1.				
31. Contact person's telephone	number	32. Contact	person's email address:			
734-302-5344 januszekd@dteenergy.com						
33. Applicant's consultant for ap	plication:	-				
Conestoga-Rovers & Assoc	iates (Don Sutton)					
34. Consultant's telephone number: 217-717-900935. Consultant's email address: dsutton@craworld.com						
		·				
Rev	iew Of Contents o	of the Appli	cation			
36. Is the emission unit covered constructed?	by this application alre	eady	🗌 Yes 🔀 No			

If "yes", provide the date construction was completed:			
Note: The Illinois EPA is unable to issue a construction permit for a emission unit that hat a already been constructed.	as		
37. Does the application include a narrative description of the propose project?	ed 🛛 Yes	🗌 No	
38. Does the application contain a list or summary that clearly identifie the emission units and air pollution control equipment that are part of the project?		🗌 No	
39. Does the application include process flow diagram(s) for the project showing new and modified emission units and control equipment and related existing equipment and their relationships?	<sup>ct</sup> 🛛 Yes	🗌 No	
40. If the project is at a source that has not previously received a permit from the BOA, does the application include a source description, plot plan and site map?	Yes reformation pre	No No No	N/A*

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Review Of Contents of the Application (continued)					
41. Does the application include relevant information for the proposed project as requested on Illinois EPA, BOA application forms (or otherwise contain all the relevant information)?	🗙 Yes 🗌 No				
<ul> <li>42. Does the application identify and address all applicable or potentially applicable emissions standards, including:</li> <li>a. State emission standards (35 IAC Chapter I, Subtitle B);</li> <li>b. Federal New Source Performance Standards (40 CFR Part 60);</li> <li>c. Federal standards for HAPs (40 CFR Parts 61 and 63)?</li> </ul>	🗙 Yes 🗌 No				
43. Does the application address whether the proposed project or the source could be a major project for Prevention of Significant Deterioration (PSD), 40 CFR 52.21?	🗌 Yes 🗌 No . 🛛 N/A				
44. Does the application address for which pollutant(s) the proposed project or the source could be a major project for PSD, 40 CFR 52.21?	🗌 Yes 🗌 No . 🔀 N/A				
45. Does the application address whether the proposed project or the source could be a major project for "Nonattainment New Source Review," (NA NSR), 35 IAC Part 203?	🗌 Yes 🗌 No 🔀 N/A				
46. Does the application address for which pollutant(s) the proposed project or the source could be a major project for NA NSR, 35 IAC Part 203?	🗌 Yes 🗌 No 🔀 N/A				
47. Does the application address whether the proposed project or the source could potentially be subject to federal Maximum Achievable Control Technology (MACT) standard under 40 CFR Part 63 for Hazardous Air Pollutants (HAP) and identify the standard that could be applicable?	<ul> <li>Yes</li> <li>No</li> <li>N/A*</li> <li>* Source not major X</li> <li>Project not major X</li> </ul>				
48. Does the application identify the HAP(s) from the proposed project or the source that would trigger the applicability of a MACT standard under 40 CFR Part 63?	🗌 Yes 🗌 No 🔀 N/A				
49. Does the application include a summary of the current and the future potential emissions of the source after the proposed project has been completed for each criteria air pollutant and/or HAP (tons/year)?	X Yes No N/A* * Applicability of PSD. NA NSR or 40 CFR 63 not applicable to the source's emissions.				
50. Does the application include a summary of the requested permitted annual emissions of the proposed project for the new and modified emission units (tons/year)?	X Yes No N/A* * Project does not involve an increase in emissions from new or modified emission units.				
51. Does the application include a summary of the requested permitted production, throughput, fuel, or raw material usage limits that correspond to the annual emissions limits of the proposed project for the new and modified emission units?	Yes No N/A* * Project does not involve an increase in emissions from new or modified emission units.				
52. Does the application include sample calculations or methodology for the emission estimations and the requested emission limits?	🗙 Yes 🗌 No				
53. Does the application address the relationships with and implications of the proposed project for the source's FESOP?	□ Yes □ No ⊠ N/A* *FESOP not yet issued.				
54. If the application contains information that is considered a TRADE SECRET, has such information been properly marked and claimed and other requirements to perfect such a claim been satisfied in accordance with 35 IAC Part 130?	Yes No X N/A* • No information in the application is claimed to be a TRADE SECRET				
Note: "Claimed information will not be legally protected from disclosure to the public if it is not properly claimed or does not qualify as trade secret information.					

Review Of Contents of the Application (co	wénnec)	
55. If the source is located in a county other than Cook County, are two separate copies of this application being submitted?	🗍 Yəs	⊠ No
56. If the source is located in Cook County, are three separate copies of this application being submitted?	🖾 Yes	🗍 No
57. Does the application include a completed "FEE DETERMINATION FOR CONSTRUCTION PERMIT APPLICATION," Form 197-FEE, for the emission units and control equipment for which a permit for construction or modification is being sought?	🔀 Yes	🗋 No
58. Does the application include a check in the proper amount for payment of the Construction permit fee?	🔀 Yes	🗍 No

Note: Answering "No" to Items 36 through 58 may result in the application being deemed incomplete.

Signature Block					
Pursuant to 35 IAC 201.159, all applications and supplements thereto shall be signed by the owner and operator of the source, or their authorized agent, and shall be accompanied by evidence of authority to sign the application. Applications without a signed certification will be deemed incomplete.					
59. Authorized Signature:					
I certify under penalty of law that, based on informa inquiry, the statements and information contained in complete and that I am a responsible official for the Environmental Protection Act. In addition, the tech authorized to submit (by hard copy and/or by electr related to this application that may be requested by	n this application are true, accurate and source, as defined by Section 39.5(1) of the nical contact person identified above is onic copy) any supplemental information				
BY: State	Mice President				
AUTHORIZED SIGNATURE	THEE OF SIGNATORY				
Salver San Car Electron and and	e destruit de constant de cons				
TYPED OR PRINTED NAME OF SIGNATORY	DATE				

Revenue



Sureau of Air \* 1021 North Grand Avenue East \* P.O. Box 19508 \* Springlield \* Illingis \* 62794-9506

#### FEE DETERMINATION FOR CONSTRUCTION PERMIT APPLICATION

	FORA	GENCY USE ON	<i>u.y</i>
iD Norther		Permii ši	
Complete	focomplete	Date Complete:	
Check Number:		Account Mame:	

This form is to be used to supply lee information that must accompany all construction particle polications. This application must accur pay and a polication must accur pay and a polication must accur pay and a polication of the deamed complete. Make theory order payable to are illinois. Environmental Protection Agency, Division of Arr Porticion Componer Recent Section at the above address. Do NOT sector cash Refer to instructions (197-INST) for assistance.

#### Source Information

2	Source Name: Project Name: Contact Name,	DTE Chicago F Conveyor Addit Donald Janusz		3. Sc.	roe 10 #: (il app ca:( Phone #:		031600GF 02-5344
Fee	· Determinatio	n					
6. 1	The boxes below	are automatically ca	loutased.				
	Section 1 Sabtata	si <b>\$0</b>	<ul> <li>Section 2, 3 or</li> </ul>	1 Subtotal	\$7,000	55	\$7,000
7 3	Үриг арріясанон у		<b>se of Submittal</b> In al the following live Supposes of this form:	calogories desc	ribeci pelow - Ch	eok été p	Grand Total ox that applies.
	<ul> <li>Major So</li> </ul>	wroe is a source the	a is required to obtain	s CAAPP orm	ŧ.		
		c Minor Source is a ants (e.g.,FESOP)	source that has take	i Emits on poleni	ial to emit in a p	erenit to e	void CAAPP peant
	• Non-Maj	or Source is a sour	a that is not a major o	a synthetic mino	l'solace.		
1		without status chan Proceed to Section 2	ge or with status chan	ge from syntheti	e minor to mejor	Source	
	Existing represent	yor source (het will )	secone systemic a s	и 16-ивуся <del>ко</del> ско	e – Proceed to S	S2922-47	
$\square$	New Abjor or sy	нани твое зове	e. Process to Sector	. <del>.</del> .			\$0
	New non-major	source. Proceed to	Section 3.				Section i Subiolal
	legency error an	d 7 the request is re	request to correct an ceived within the dead nd 4 - Proceed Arrecti	Phe for a permit			
800	kaalise beeng riscie	ed to require end you d and resistlites under d by the forms manage	must stactissis role inform 415 4LCS 5 € ° SFC - 8 - smeatt center	ston man 455 t. s not necessory ex	08 5139, Fellon, 4 1986 944 4977 4 6	୦ ଏକ ଲେ କଳ ଭାରତାନ୍ତ୍ର ହିନ୍ତି	olo reson or Ris- s Information, "Pils
Sec	tion 2: Specia	l Case Filing Fee					
			addresses one or r actly to Section 5.		1.01		
	- Addition :	or replacement of	control devices on g	armited chits.			
		ects/trief burns by	a permitted unit				
	Land cerr	adiation projects					
	Revisions	s related to metho	dology or timing for	entission testin	9		
		anta batan Maria Araa a	transmission in a second				

Minor administrative-type change to a permit.

R. 832-1275 1927-1111 - Rev Rept.	Application Page	12

Page : ei 2

Sec.	êra S	t Fear an usered of Fishedral Helekinger Fampez	
в.	511	This epplication consists of a single only emission unit or no more then two modified emission units. (3500 fee)	\$.
3 <u>0.</u>		This application consists of more item one new endosion unit or more than two modified — units. (\$1.000 fee)	10.
11.		This application consists of a new source or emission unit aubject to Section 39.2 of the Act (i.e., Local Silling Review); a commondal incloantice or a municipal waste, hozardous weste, or weste the incloarator; a commercial power generator; or an emission unit designated as a complex source by agency rulemaking. (\$15,000 fee)	11. <u> </u>
12.	Ű	A public hearing is held (sen instructions). (\$10,000 fee)	12.
13.		Section 3 subtotal (lines 9 through 12 - entered on page 1)	13.

#### Section 4: Feee for Current or Projected Major or Synthetic Minor Sources

h ft the -	14. For the first modified emission unit, enter \$2,000.	14.	
Application contains modified emission units only	15. Mumber of additional modified emission units = x \$1,000.	15.	* * ), 7717/markstates at 1997 199
·	15. Line 14 plus line 15, or \$5,000, whichever is less.	16.	
Application contains	17. For the first new emission unit, caller \$4,000.	17.	\$4,000
new anti/or modified emission units	<ol> <li>Number of additional new and/or modified emission units = 3 x \$1,000.</li> </ol>	18.	\$3,000
	19. Line 17 plus line 18, or \$10,000, whichever is less.	19.	\$7,000
Application contains notiing exercise	<ol> <li>Number of individual pollutants that rely on a netting exercise or contemporaneous emissions decrease to avoid application of PSD or nonattainment area NSR = x \$3,000.</li> </ol>	20.	
	21. If the new source or emission unit is subject to Section 39.2 of the Act (i.e. signg); a commercial incinerator or other municipal waste, hazardous waste, or waste the incinerator; a commercial power generator; or one or more other emission units designated as a complex source by Agency n familiting, enter \$25,000.	21.	······································
Additiones Europismental	22. If the source is a nav major source subject to PSD, enter \$12,000,	22,	
Fees	23. If the project is a major modification subject to PSD, enter \$6,000.	25.	
	24. If this is a may major course subject to nonatisiriment and (NAA) NSR, actor \$20,000.	1 24. 1	
	23. If and the major modification subject to frace WSR, order \$28,000.		· · · ·
	36. If the opplication involves a determination of WACT in a pollutani and the project is not activate to DACT or CARR for the restand pollution under PSD or NSR (e.g., VCAR for ingenic MAP), enter 45,000 per unit in under a observation is required or otherwise required. a SEANO.		
	27. If a public hoaring is noted (see instructions), enter \$10,000.	27.	
20. Beckon 4 aubola	Hins 16 and lines (9 through 25) to be entered on paged	28	\$7.000

#### Section 5: Continention

NOTE: Applications without a signed contilection will be desmed incompation

29. I consign and panally of polyhet, based on information and belief formed after reasonable inquiry, the information consistent in this for application form is true, accurate and complete.
 39. I consign and panally of polyhet, based on information and belief formed after reasonable inquiry, the information consistent in this for application form is true, accurate and complete.
 39. I consign and polyhet, based on information and belief formed after reasonable inquiry, the information consistent is true, accurate and complete.
 39. I consistent in this for a state of the state of the

Andreas and the second

179.502



#### ILLINOIS ENVIRONMENTAL PROTECTION AGENCY DIVISION OF AIR POLLUTION CONTROL -- PERMIT SECTION P.O. BOX 19506 SPRINGFIELD, ILLINOIS 62794-9506

FOR	APPL	ICANT'S	USE

Revision #:				
Date:	_ / _		/ _	
Page		of		
Source Desi	gnati	on:		

FOR AGENCY USE ONLY

PROCESS EMISSION UNIT	ID NUMBER:
DATA AND INFORMATION	EMISSION POINT #:
	DATE:
	FORMATION
1) SOURCE NAME:	ORMATION
DTE Chicago Fuels Terminal, LLC	
2) DATE FORM PREPARED: March 12, 2012	3) SOURCE ID NO. (IF KNOWN): 031600GSF
GENERAL IN	IFORMATION
4) NAME OF EMISSION UNIT: Four additional portable conveyors	
5) NAME OF PROCESS:	
Material Handling	
6) DESCRIPTION OF PROCESS:	
Handling of coal, pet coke, and salt.	
7) DESCRIPTION OF ITEM OR MATERIAL PRODUCED OR A	CTIVITY ACCOMPLISHED:
Material transfer station	
8) FLOW DIAGRAM DESIGNATION OF EMISSION UNIT:	
See figure 1.	
9) MANUFACTURER OF EMISSION UNIT (IF KNOWN):	
To Be Determined 10) MODEL NUMBER (IF KNOWN):	
To Be Determined	11) SERIAL NUMBER (IF KNOWN): To Be Determined
12) DATES OF COMMENCING CONSTRUCTION.	a) CONSTRUCTION (MONTH/YEAR):
OPERATION AND/OR MOST RECENT MODIFICATION	Upon issuance of permit
OF THIS EMISSION UNIT (ACTUAL OR PLANNED)	b) OPERATION (MONTH/YEAR):
	Upon issuance of permit c) LATEST MODIFICATION (MONTH/YEAR):
	N/A
13) DESCRIPTION OF MODIFICATION (IF APPLICABLE):	1963
N/A	

THIS AGENCY IS AUTHORIZED TO REQUIRE THIS INFORMATION UNDER ILLINOIS REVISED STATUTES, 1991, AS AMENDED 1992, CHAPTER 111 1/2, PAR. 1039.5. DISCLOSURE OF THIS INFORMATION IS REQUIRED UNDER THAT SECTION. FAILURE TO DO SO MAY PREVENT THIS FORM FROM BEING PROCESSED AND COULD RESULT IN THE APPLICATION BEING DENIED. THIS FORM HAS BEEN APPROVED BY THE FORMS MANAGEMENT CENTER.

## APPLICATION PAGE \_\_\_\_14

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14) DOES THE EMISSION UNIT HAVE MORE THAN ONE MODE OF OPERATION?	) YES	
IF YES, EXPLAIN AND IDENTIFY WHICH MODE IS COVERED BY THIS FORM (NOTE: A SEPARATE PROCESS EMISSION UNIT FORM 220-CAAPP MUST BE COMPLETED FOR EACH MODE):		
AS PROVIDE THE NAME AND DESIGNATION OF ALL ARE POLITION CONTROL FOURDME		
15) PROVIDE THE NAME AND DESIGNATION OF ALL AIR POLLUTION CONTROL EQUIPME EMISSION UNIT, IF APPLICABLE (FORM 260-CAAPP AND THE APPROPRIATE 260-CAAP MUST BE COMPLETED FOR EACH ITEM OF AIR POLLUTION CONTROL EQUIPMENT):		
None, athough water suppression is used to control particulate emissions.		
16) WILL EMISSIONS DURING STARTUP EXCEED EITHER THE ALLOWABLE EMISSION RATE PURSUANT TO A SPECIFIC RULE, OR THE ALLOWABLE EMISSION LIMIT AS ESTABLISHED BY AN EXISTING OR PROPOSED PERMIT CONDITION?	YES	× NO
IF YES, COMPLETE AND ATTACH FORM 203-CAAPP, "REQUEST TO OPERATE WITH EXCESS EMISSIONS DURING STARTUP OF EQUIPMENT".		
17) PROVIDE ANY LIMITATIONS ON SOURCE OPERATION AFFECTING EMISSIONS OR AN STANDARDS (E.G., ONLY ONE UNIT IS OPERATED AT A TIME):	Y WORK PRACT	ICE
The source has limited their material throughput per year to obtain a FESOP.		

#### OPERATING INFORMATION

Γ

18) ATTACH THE CALCULATIONS. TO THE EXTENT THEY ARE AIR EMISSION RELATED, FROM WHICH THE FOLLOWING OPERATING INFORMATION, MATERIAL USAGE INFORMATION AND FUEL USAGE DATA WERE BASED AND LABEL AS EXHIBIT 220-1. REFER TO SPECIAL NOTES OF FORM 202-CAAPP.							
19a) MAXIMUM OPERATING HOURS HOURS/DAY: DAYS/WEEK: WEEKS/YEAR:							
	12	7			50		
b) TYPICAL OPERATING HOURS	HOURS/DAY:		DAYS/WEEK	St.	WEEK	(S/YEAR:	
	12 5.2 50					50	
20) ANNUAL THROUGHPUT	DEC-FEB(%):	MAR	-MAY(%):	JUN-AUG(%	b):	SEP-NOV(%):	
	25		25	25		25	

	MATERIAL USAGE INFORMATION							
	MAXIMU	JM RATES	TYPICA	L RATES				
21a) RAW MATERIALS	LBS/HR	TONS/YEAR	LBS/HR	TONS/YEAR				
See Tables 5 & 6								

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	MAXIMUM RATES		TYPICAL RATES	
21b) PRODUCTS	LBS/HR	TONS/YEAR	LBS/HR	TONS/YEAR
MAXIMUM RAT		1 RATES	TES TYPICAL RATES	
21c) BY-PRODUCT MATERIALS	LBS/HR	TONS/YEAR	LBS/HR	TONS/YEAR
FUEL USAGE DATA           22a) MAXIMUM FIRING RATE         b) TYPICAL FIRING RATE         c) DESIGN CAPACITY FIRING				
(MILLION BTU/HR): (MILLION BTU/HR):			RATE (MILLION BTU/HR):	
d) FUEL TYPE:				
NATURAL GAS O FUEL OIL: GRADE NUMBER O COAL O OTHER				
IF MORE THAN ONE FUEL IS USED, ATTACH AN EXPLANATION AND LABEL AS EXHIBIT 220-2.				
e) TYPICAL HEAT CONTENT OF FUEL (BTU/LB, BTU/GAL OR BTU/SCF):				
g) TYPICAL ASH CONTENT (WT %., NA FOR NATURAL h) ANNUAL FUEL USAGE (SPECIFY UNITS, E.G.,				
GAS): SCF/YEAR, GAL/YEAR, TON/YEAR):				
23) ARE COMBUSTION EMISSIONS DUCTED TO THE SAME STACK OR CONTROL AS VES NO				
IF NO, IDENTIFY THE EXHAUST POINT FOR COMBUSTION EMISSIONS:				

APPLICATION PAGE <sup>16</sup>

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See Narrative, Section 1.0.

	APPLICABLE RULES	
24) PROVIDE ANY SPECIFIC EMISSION STANDARD(S) REGULATED AIR POLLUTANT(S)	AND LIMITATION(S) SET BY RULE(S) WHICH ARE APPLIC EMISSION STANDARD(S)	ABLE TO THIS EMISSION UNIT (E.G., VOM, IAC 218.204(j)(4), 3.5 LBS/GAL): REQUIREMENT(S)
25) PROVIDE ANY SPECIFIC RECORDKEEPING RULE(	S) WHICH ARE APPLICABLE TO THIS EMISSION UNIT:	
REGULATED AIR POLLUTANT(S)	RECORDKEEPING RULE(S)	REQUIREMENT(S)
26) PROVIDE ANY SPECIFIC REPORTING RULE(S) WH		
26) PROVIDE ANY SPECIFIC REPORTING ROLE(3) WE REGULATED AIR POLLUTANT(S)		REQUIREMENT(S)
27) PROVIDE ANY SPECIFIC MONITORING RULE(S) W	HICH ARE APPLICABLE TO THIS EMISSION UNIT:	
REGULATED AIR POLLUTANT(S)	MONITORING RULE(S)	REQUIREMENT(S)
28) PROVIDE ANY SPECIEIC TESTING PULIES AND/OR	PROCEDURES WHICH ARE APPLICABLE TO THIS EMISS	
REGULATED AIR POLLUTANT(S)	TESTING RULE(S)	REQUIREMENT(S)
	47	
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29) DOES THE EMISSION UN OTHERWISE APPLICABL	NIT QUALIFY FOR AN EXEMP E RULE?	TION FROM AN	YES	NO NO
EXEMPTION. PROVIDE SUPPORTING DATA AND	THE RULE FROM WHICH IT A DETAILED EXPLANATION J CALCULATIONS. ATTACH A ADDRESS AND JUSTIFY THI	USTIFYING THE EXEMPTIO ND LABEL AS EXHIBIT 220-	N. INCLUDE DETA	ALED
	COMPLIANC	E INFORMATION		
30) IS THE EMISSION UNIT I REQUIREMENTS?	N COMPLIANCE WITH ALL AF	PLICABLE	🗙 yes	O NO
	CAAPP "COMPLIANCE PLAN/S JNITS" MUST BE COMPLETEI			OR NON
31) EXPLANATION OF HOW	INITIAL COMPLIANCE IS TO E	BE. OR WAS PREVIOUSLY.	DEMONSTRATED:	
See Narrative, Section	1.0.			
32) EXPLANATION OF HOW	ONGOING COMPLIANCE WIL	L BE DEMONSTRATED:		
See Narrative, Section	<b>U</b> .			
TEST	ING, MONITORING, REC	CORDKEEPING AND R	EPORTING	
33a) LIST THE PARAMETER	S THAT RELATE TO AIR EMIS	SIONS FOR WHICH RECOR	DS ARE BEING M	
	E APPLICABILITY OR COMPL MENT, AND THE FREQUENC			
	MENT, AND THE I REQUENCE		, HOORET, DAIET,	, WELKET).
PARAMETER	UNIT OF MEASUREMENT	METHOD OF MEASUREME		
Visible Emissions		Method 9		quest by the
	Percent Opacity	Method a	Agency	

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RECORDED PARAME	TER INCLUDE THE METHOD	CORDS WILL BE CREATED AND M OF RECORDKEEPING, TITLE OF DNTACT FOR REVIEW OF RECORD	PERSON RESPONSIBLE FOR
PARAMETER	METHOD OF RECORDKEEPING	TITLE OF PERSON RESPONSIBLE	TITLE OF CONTACT PERSON
Throughput	Log Book	Operations Manager	Operations Manager
c) IS COMPLIANCE OF THE THE RECORDS?	E EMISSION UNIT READILY	DEMONSTRATED BY REVIEW OF	X YES NO
IF NO. EXPLAIN:			
	ADILY AVAILABLE FOR INSP		
SUBMITTAL TO THE AGI		ECTION. COPTING AND	X YES 🗌 NO
IF NO, EXPLAIN:			
34a) DESCRIBE ANY MONIT COMPLIANCE:	ORS OR MONITORING ACT	IVITIES USED TO DETERMINE FEE	ES, RULE APPLICABILITY OR
N/A			
b) WHAT PARAMETER(S) I	S(ARE) BEING MONITORED	(E.G., VOM EMISSIONS TO ATMO	SPHERE)?
N/A			
c) DESCRIBE THE LOCATIO	ON OF EACH MONITOR (E.G	G., IN STACK MONITOR 3 FEET FRO	OM EXIT):
N/A	·		

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34d) IS EACH MONITOR EQUIPPED WITH A RECORDING DEVICE?	O YES	
IF NO, LIST ALL MONITORS WITHOUT A RECORDING DEVICE:		
N/A		
e) IS EACH MONITOR REVIEWED FOR ACCURACY ON AT LEAST A QUARTERLY BASIS?	YES	O NO
IF NO. EXPLAIN:		
N/A		
f) IS EACH MONITOR OPERATED AT ALL TIMES THE ASSOCIATED EMISSION UNIT IS	O YES	
IN OPERATION?		
IF NO. EXPLAIN:		
N/A		
35) PROVIDE INFORMATION ON THE MOST RECENT TESTS, IF ANY. IN WHICH THE RESU PURPOSES OF THE DETERMINATION OF FEES. RULE APPLICABILITY OR COMPLIANCE		
DATE, TEST METHOD USED, TESTING COMPANY, OPERATING CONDITIONS EXISTING SUMMARY OF RESULTS. IF ADDITIONAL SPACE IS NEEDED, ATTACH AND LABEL AS		EST AND A
TEST DATE TEST METHOD TESTING COMPANY CONDITIONS	SUMMARY OF	RESULTS
N/A		
36) DESCRIBE ALL REPORTING REQUIREMENTS AND PROVIDE THE TITLE AND FREQUEN		г
SUBMITTALS TO THE AGENCY:		I
REPORTING REQUIREMENTS TITLE OF REPORT	FREQUENCY	
A		

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### See Tables 1-12.

					(37)	EMISSION	INFC	DRMATI	ON						
		(	☐ <sup>1</sup> ACTUAL EM ☐ <sup>1</sup> UNCONTRO	ISSION RATE	NRATE		'	ALLOW	ABLE B	Y RULE EMISS	ION RATE		<sup>2</sup> PERM	ITTED EMIS	SION RATE
REGULATED AIR POLLUTANT		LBS PER HOUR (LBS/HR)	TONS PER YEAR (TONS/YR)	<sup>3</sup> OTHER TERMS	<sup>3</sup> OTHER TERMS	<sup>4</sup> DM	5	RATE	(UNITS)	APPLICABLE RULES	TONS PER YEAR (TONS/YR)		RATE	(UNITS)	TONS PER YEAR (TONS/YR)
CARBON	MAXIMUM							(	)						
MONOXIDE (CO)	LYP CAL							(	)						
LEAD	MAXIMUM.							(	)						
	TYP CAL.							(	)						
NITROGEN	MAXIM MI			-				(	)						
OXIDES (NOx)	TYP CAL							(	)						
PARTICULATE	MAXIMUM.							(	)						
MATTER (PART)	TYP CAL.							(	)						
PARTICULATE MATTER <= 10	MAXING M							(	)						
MICROMETERS (PM10)	TYP CAL.							(	)						
SULFUR	MAXIMUM.							(	)						
DIOXIDE (SO2)	TYP CAL.							(	)						
VOLATILE ORGANIC	MAXING M							(	)						
MATERIAL (VOM)	TYP CAL.							(	)						
OTHER, SPECIFY:	MAXIMUM							(	)						
	TYP CAL.							(	)						
EXAMPLE: PARTICULATE	MAXIMGM:	5.00	21.9	0.3 GR/DSCF		1		6.0 (LBS	S/HR)	212.321	26.28	] [	5.5 L	.BS/HR	22
MATTER	TYP:CAL	4.00	14.4	0.24 GR/DSCF		4		5.5 (LBS	S/HR)	212.321	19.80				

IMPORTANT: ATTACH CALCULATIONS, TO THE EXTENT THEY ARE AIR EMISSIONS RELATED, ON WHICH EMISSIONS WERE DETERMINED AND LABEL AS EXHIBIT 220-5.

<sup>1</sup>CHECK UNCONTROLLED EMISSION RATE BOX IF CONTROL EQUIPMENT IS USED. OTHERWISE CHECK AND PROVIDE THE ACTUAL EMISSION RATE TO ATMOSPHERE. INCLUDING INDOORS. SEE INSTRUCTIONS.

<sup>2</sup>PROVIDE THE EMISSION RATE BOX IF BOX IF BOX IF CONTROL EQUIPMENT IS USED. OTHER WISE CHECK AND PROVIDE THE ACTUAL EMISSION RATE TO A IMOSPHERE. INCLUDING INDOORS. SEE INSTRUCT <sup>2</sup>PROVIDE THE EMISSION RATE THAT WILL BE USED AS A PERMIT SPECIAL CONDITION. THIS LIMIT WILL BE USED TO DETERMINE THE PERMIT FEE. <sup>3</sup>PLEASE PROVIDE ANY OTHER EMISSION RATE WHICH IS COMMONLY USED, REQUIRED BY A SPECIFIC LIMITATION OR THAT WAS MEASURED (E.G. PPM, GR/DSCF, ETC.) <sup>4</sup>DM - DETERMINATION METHOD: 1) STACK TEST, 2) MATERIAL BALANCE, 3) STANDARD EMISSION FACTOR (AP-42 OR AIRS), 4) ENGINEERING ESTIMATE, 5) SPECIAL EMISSION FACTOR (NOT AP-42 OR AIRS) <sup>5</sup>RATE - ALLOWABLE EMISSION RATE SPECIFIED BY MOST STRINGENT APPLICABLE RULE.

APPLICATION PAGE \_\_\_\_\_

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		(3	8) HAZARDOUS	AIR POLLUTAI	IT EMISSION II	VFORMATI	ON .		
			□ <sup>1</sup> АСТИ/ □ <sup>1</sup> UNCO	AL EMISSION RA NTROLLED EMIS	TE SION RATE			ALLOWABLE BY RU	ILE
NAME OF HAP EMITTED	2 <sub>CAS</sub> NUMBER		POUNDS PER HOUR (LBS/HR)	TONS PER YEAR (TONS/YR)	<sup>3</sup> OTHER TERMS	<sup>4</sup> DM		<sup>5</sup> RATE OR STANDARD	APPLICABLE RULE
		MAXIMUM							
		TYP CAL:							
		MAXIMUM.							
		TYP CAL.							
		MAXIM M <sup>i</sup>							
		TYPICAL							
		MAXIMUM.							
		TYP CAL.							
		MAXIMONE							
		LYP CAL							
		MAXIMUM.							
		TYP CAL.							
		MAXIMUM							
		TYP CAL:							
		MAXIMUM.							
		TYP CAL.							
EXAMPLE:		MAXIMG VI:	10.0	1.2		2		98% by wt control device	CFR 61
Benzene	71432	TYP:OAL:	8.0	0.8		2		leak-tight trucks	61.302(b),(d)

IMPORTANT: ATTACH CALCULATIONS, TO THE EXTENT THEY ARE AIR EMISSIONS RELATED, ON WHICH EMISSIONS WERE DETERMINED AND LABEL AS EXHIBIT 220-6.

<sup>1</sup>PROVIDE UNCONTROLLED EMISSIONS IF CONTROL EQUIPMENT IS USED. OTHERWISE, PROVIDE ACTUAL EMISSIONS TO THE ATMOSPHERE, INCLUDING INDOORS. CHECK BOX TO SPECIFY. CAS - CHEMICAL ABSTRACT SERVICE NUMBER.

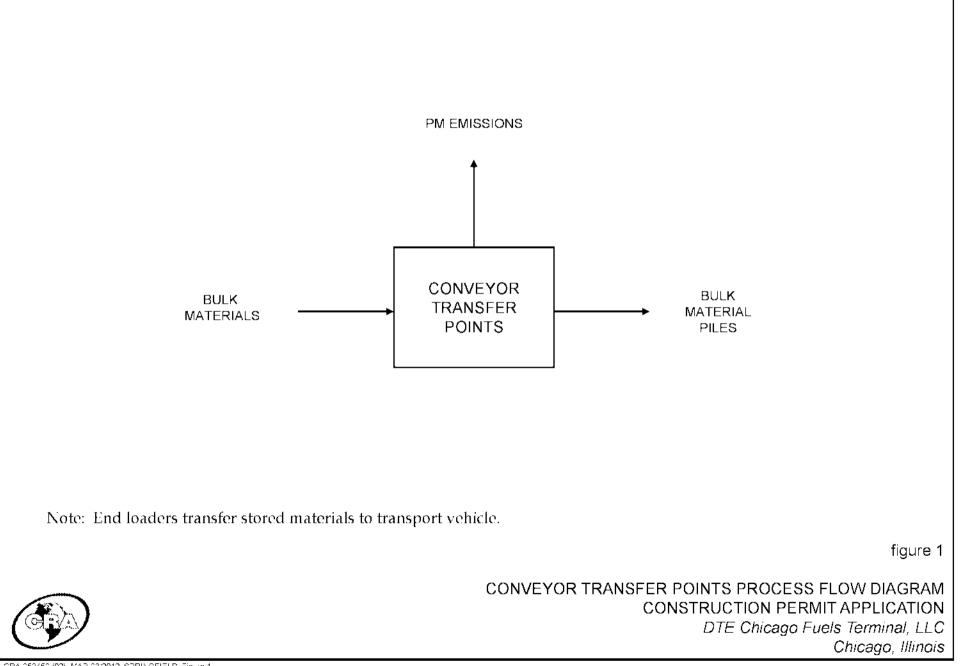
\*PLEASE PROVIDE ANY OTHER EMISSION RATE WHICH IS COMMONLY USED, REQUIRED BY A SPECIFIC LIMITATION OR THAT WAS MEASURED (E.G., PPM, GR/DSCF, ETC.).

<sup>(1</sup>DM - DETERMINATION METHOD: 1) STACK TEST, 2) MATERIAL BALANCE, 3) STANDARD EMISSION FACTOR (AP-42 OR AIRS, 4) ENGINEERING ESTIMATE, 5) SPECIAL EMISSION FACTOR (NOT AP-42 OR AIRS). <sup>(1</sup>RATE - ALLOWABLE EMISSION RATE OR STANDARD SPECIFIED BY MOST STRINGENT APPLICABLE RULE.

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	EXHAUST POINT INFORMA	TION
THIS SECTION SHOULD NOT BE COMPLETED	IF EMISSIONS ARE EXHAUSTED THRO	OUGH AIR POLLUTION CONTROL EQUIPMENT.
39) FLOW DIAGRAM DESIGNATION OF	EXHAUST POINT:	
See figure 1.		
40) DESCRIPTION OF EXHAUST POINT DISCHARGES INDOORS, DO NOT C		INDOORS, ETC.). IF THE EXHAUST POINT S.
Varies		
41) DISTANCE TO NEAREST PLANT BO	UNDARY FROM EXHAUST POINT	DISCHARGE (FT):
Varies		
42) DISCHARGE HEIGHT ABOVE GRADI	E (FT):	
Varies		
43) GOOD ENGINEERING PRACTICE (G	EP) HEIGHT, IF KNOWN (FT):	
44) DIAMETER OF EXHAUST POINT (FT)	: NOTE: FOR A NON CIRCULAR I	EXHAUST POINT, THE DIAMETER IS
1.128 TIMES THE SQUARE ROOT O	F THE AREA. N/A	
45) EXIT GAS FLOW RATE	a) MAXIMUM (ACFM):	b) TYPICAL (ACFM):
	N/A	N/A
46) EXIT GAS TEMPERATURE	a) MAXIMUM (°F):	b) TYPICAL ("F):
	N/A	N/A
47) DIRECTION OF EXHAUST (VERTICA	L, LATERAL, DOWNWARD):	
N/A		
48) LIST ALL EMISSION UNITS AND CON	NTROL DEVICES SERVED BY THIS	S EXHAUST POINT:
NAME		FLOW DIAGRAM DESIGNATION
<sup>a)</sup> See Table 13		
b)		
c)		
d)		
e)		
THE FOLLOWING INFORMATION NEED ONLY	BE SUPPLIED IF READILY AVAILABLE.	
49a) LATITUDE:	b) LONGITU	DE:
	,	
50) UTM ZONE:	b) UTM VERTICAL (KM):	c) UTM HORIZONTAL (KM):

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CRA 052450 (02), MAR 03/2012 SPRINGFIELD Figure 1

#### PROCESS UNITS POTENTIAL TO EMILICAT CLEATIONS.

DISCRIPTION		UM MATTRIAL DUNG RATL <sup>7</sup>	PARTIC MULTI	TE SIZE PLIER <sup>7</sup>	FAUS	SIONTACI	ORS <sup>1</sup>	CONTROJ		PALEMISS	HON RATE		MISSION AIT
	ton/hr	ton/yr	PM	$PM_{10}$	19M	$PM_{36}$	axiis	1 YPF	marc.	th√day	ton/yr	ll√day	ton/yr
Coul/Pet	coke Unloading In	tissions											
BT – To C (150) (Coal/ Percoke)	200	2,550,150	0.540	2.42	0.00064	0.00053	lb/son	Water Suppression	0.0%	2.05	0.57	0.96	0.18
KU/TU – to C (10) (Coal/Perecke)	2	2,550,150	0,540	3243	0.00064	0.00053	llø/son	Water Suppression	-0.0%	2.05	0.57	0.96	0.18
KU/TU = to C (1=0) (Coal/Perceke)	200	2,550,150	0.5310	0.490	0.00064	0.00053	lb/son	Bagnouse	90.05	0.41	0.07	0.19	0.005 0.005
KU 2 to C 7 (Coal/ Perceke)	2,000	171520.000	0.540	0.490	0.00064	0.00053	lb/son	Water Suppression	0.0%	15.28	2,579	0.25	1.2
RU Bre C 8 (Coal/ Pereke)	2,000	17620.000	0.40	0.550	0.00064	0.000230	lb/ton	Water Suppression	10.02	15.28	2019	7.2.4	1.2
	<i></i>					tmi	sions From	Coal/Petcoke Unloadin	ig∶Total>>	35.0	6.4	16.6	3.0
Controletion C	omrøyor Fransfør P 2,500	2 ,900,000	0.740	0.350	0.00064	0.00030	b/ten	Water Suppression	50.03.	0.0	3,16	0,23	
C21551	 -,	35,010,000	0.740	0.350	0.00064	2.22232	b/ten	Water Suppression	50.03	30.56	7.79	1,15	2.61
Cicita Ci2	- 000 - 1000	35,516,555	0.700	0.350	0.00064	2.22222	b/ten	Water Suppression	50.03	30.55	5.59	1,15	2.64
C = 168.5	2,500	2 ,900,000	0.740	0.350	0.00064	6.66636	b/ten	Water Suppression	50.0%	0. D	3,10	0,03	.115
S1116-014	2,500	2 ,000,000	0.740	0.350	0.00064	0.00030	b/len	Water Suppression	50.0%	9. D	3,10	0,03	.65
C416C F	2,500	2 ,600,000	0.740	0.350	0.00064	0.00030	b/ten	Water Suppression	50.03.	9, 2	3,10	6,03	
CB-1652	2,500	2 ,900,000	0.740	0.350	0.00064	2.22222	b/ten	Water Suppression	50.03.	9, 0	3,19	6,03	.u.5
AC TION 5	3,000	26,280,000	0.740	0.350	0.00064	0.00030	b/ten	Water Suppression	50.0%	22.62	1. 9	0.84	.08
20 2 to \$15	3,000	26,280,000	0.740	0.350	0.00064	0.00033	lb/ten	Water Suppression	56.63	22.62	1.18	10.84	.09
Reaction Carl	3,000	26,280,000	0.740	0.350	0.00064	0.00030	b/ten	Water Suppression	50.03.	22.62	1, 9	0.81	,68
2014 to \$1.5	3,000	26,280,000	0.750	0.350	0.00064	2.22232	b/ten	Water Suppression	50.03.	22.62	1, 9	0.81	,69
C / to C 9	2,000	7,520,000	0.750	0.350	0.00064	0.00030	b/ten	Water Suppression	50.0%	5.28	2,79	7.23	.32
C 8 to C 10	2,000	7,520,000	0.740	0.350	0.00064	0.00030	b/len	Water Suppression	50.0%	5.28	2,70	7.23	.32
V 916 C 11	2,000	7,520,000	0.740	0.350	0.00064	2.00030	b/len	Water Suppression	50.0%	5.28	2,70	7.23	.32
V 1016 C 11	2,000	7,520,000	0.730	0.350	0.00064	2.2222	b/len	Water Suppression	50.0%	5.28	2,70	7.23	.32
V 11 (o 19 (	2,000	7,520,000	0.730	0.350	0.00064	0.00030	b/ten	Water Suppression	50.03.	5.28	2,79	7.23	.32
1.2 1 to C 12	2,000	7,520,000	0.740	0.350	0.00064	2.22232	b/ten	Water Suppression	50.03.	5.28	2,76	7.23	.32
C 12 15 SET P 1	2,000	7,520,000	0.740	0.350	0.00064	0.00030	b/ten	Water Suppression	56.63	15.28	9,76	7.23	.32

### PROCESS UNITS POLENTIAL TO EMIL CALCULATIONS.

DISCRIPTION		UM MATERIAL )HING RATE <sup>T</sup>	1	PARTICI E SIZE MUI TIPI IER <sup>7</sup>		SIONTACI	ORS <sup>1</sup>	CONTROL		PALEMISS	ION RATT		aission Ait
	ton/hr	ton/yr	17.9	$-PM_{36}$	PM	$PM_{10}$	uxiis	18197	ment.	lb√day	ton∕yr	ll√day	ton/yr
SMTP 1 re S 1	2,000	17828.000	0.740	0.550	0.00064	0.000220	lb/ton	Water Suppression	90.0N	19.28	2.79	7.23	1.2
X611 Fe C 3	2,000	17820.000	0.740	0.550	0.00064	0.000220	lb/son	Water Suppression	90.0N	18.28	2/9	7.23	:2
2015 to 312		8./60.000	0.740	0.550	0.00064	0.000220	lb/son	Water Suppression	60.03	2.64	1.9	3.61	2.00
RC to re C 3	1.000	8.760.000	0.740	0.550	0.00064	0.000220	lb/son	Water Suppression	60.03	2.64	1.5	2.61	3,66
RC 7 to C 3	1.000	8.760.000	0.740	0.550	0.00064	0.000220	lb/son	Water Suppression	50.03	2.64	1.5	3.61	3.66
						t mission.	s From Coak	Petcoke Transfer Poin	s: Total>>	408.7	74.6	193.3	35.3
Coal/Belcok	e Portable Conveyo	or Fratissions T	1	r	1	r		r	-	1	,		r
PC Drep Point	2,500	21.900.000	0.740	0.550	0.00064	0.000270	llos/for:	Water Suppression	80.03	19.10	3,49	9.32	1.66
PC 2 Dreg Point	2,500	21.900.000	0./40	0.550	0.00064	0.000270	lis/for	Water Suppression	60.0N	19.10	5,49	9.32	1.88
PC 3 Drep Point	2,500	21.900.000	0.410	0.550	0.00064	0.000220	lbs/for	Water Suppression	60.0N	19.10	3.49	9.2.9	1.88
PC 4 Drep Point	2,500	21.900.000	0.40	0.550	0.00064	0.000220	lbs/for	Water Suppression	60.0N	19.13	5,49	9.22	1.00
PC 5 Drep Point	2,500	21.900.000	0.740	0.550	0.00064	0.000220	lis/for	Water Suppression	60.03	19.10	5,49	9.22	1.66
PC & Dreg Point	2,500	21.900.000	0.740	0.550	0.00064	0.000220	lis/for	Water Suppression	50.03	19.10	5,49	9.32	1.65
PC 7 Drep Point	2,500	21.900.000	0./40	0.550	0.00064	0.000220	lis/for	Water Suppression	60.03	19.10	5,49	9.32	1.88
PC S Drep Point	2,500	21.900.000	0.740	0.550	0.00064	0.000270	lis/for	Water Suppression	60.03	19.10	5,49	9.22	1.66
PC 6 Drep Point	2,500	21.900.000	0.740	0.550	0.00064	0.000070	lis/for	Water Suppression	80.03	19.10	5,49	9.32	1.66
Pc - 0 Drep Point	2,500	21.900.000	0.740	0.550	0.00064	0.000270	liss/for:	Water Suppression	60.0N	19.10	3.49	9.32	1.88
PC Drog Pertil	2,500	21.900.000	0./40	0.550	0.00064	2,222,2	lbs/for	Water Suppression	60.0N	19.13	3.49	9.32	1.68
RC 2 Dray Pertit	2,500	21.900.000	0.40	0.550	0.00064	2.222.12	lbs/for	Water Suppression	90.03	19.13	3.49	9.2.0	1.65
2211 - le 20 (1-12)	2,500	21.900.000	0.740	0,550	0.00064	2,222,2	lbs/for	Water Suppression	90.0N	19.10	3.49	9.32	1.65
эх на РС (1.12)	2,500	21.900.000	0.740	0.550	0.00064	0.000270	lis/for	Water Suppression	60.03	19.10	3.49	9.32	1.88
RPCS - to PC (1.12)	2,500	21.900.000	0.740	0.550	0.00064	0.000290	liss/forc	Water Suppression	90.0N	19.10	.5.49	9.2.9	1.88
			1	Emi	isions From	Coul/Petcok	e Portable C	onvegor Transfer Poin	s Total>>	286.5	52.3	135.5	24.7

LABLE 1
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#### PROCESS UNITS POTENTIAL TO EMILICAT CLEATIONS.

DISCRIPTION		UM MATURIAL D'ING RATU <sup>7</sup>	PARTIC MULTI	TESIZE PLIER <sup>7</sup>	PAUS	SIONTACI	ORS <sup>1</sup>	CONTROL		PALEMISS	DON RATE	PAL <sub>ET</sub> FA RA	aissida At
	ton/hr	ton/yr	PM	$PM_{36}$	PM	$PM_{10}$	axiis	1814	DYG.	ll√day	ton/yr	ll√day	ton/yr
	coke Stacker Emi		1										
S TIG VILP 3		35,010,000	0.730	0.350	0.00064	0.00030	lb/ten	Water Suppression	50.03	30.55	5.59	1,15	2.64
S CEP 1	12.000	19.010.000	0.740	0.350	0.00064	3.333.73	Bylton	Water Suppression	90.0%	.0.56	5.58	14,45	2.94
5.2 to CL2.2	2,500	2 ,000,000	0.740	0.350	0.00064	0.00030	b/ten	Water Suppression	50.03	9, 0	.3,10	0.03	ē
\$ 2 CLP 3	2.900	21.900.000	0.740	0.550	0.00064	3,333,13	Bylton -	Water Suppression	80.0N	19.10	3.49	9.22	1.66
5346CL24	2,500	2 ,900,000	0.740	0.350	0.00064	0.00030	b/len	Water Suppression	50.03	9, 0	3,16	0,03	.s.5
\$34a CEP 4	2.500	21.900.000	0.740	0,550	0.00064	3,222,23	Byten	Water Suppression	80.0%	19.10	3549	9.32	1.68
S 145 CL2 5	2,500	2 ,000,000	0.740	0.350	0.00064	2.2222	b/len	Water Suppression	50.03.	9, 0	3,10	0.03	.uā
S To CLP 7	2,500	21.900.000	0.740	0.550	0.00064	3,333,73	By/ten	Water Suppression	60.0N	19.10	3.49	9.32	1.68
S 145 CL2 S	2,500	2 ,000,000	0.700	0.350	0.00064	0.00030	b/ten	Water Suppression	50.03.	9, 0	3,10	0,02	.uā
S To CL2 8	2.500	21.900.000	0.40	0.550	0.00064	2,222,2	By/ten	Water Suppression	60.0X	19.10	3.49	9.02	1.68
S 146 CLP 10	2,500	2 ,900,000	0.740	0.350	0.00064	0.00030	lb/ten	Water Suppression	50.0%	9, 0	3,10	0,22	.u.5
S le CLP II	2.500	21.900.000	0.740	0.350	0.00064	3,333,73	lb/ton	Water Suppression	80.0%	19.10	.549	9.32	1.66
S 146 VLP 12	2,500	2 ,600,000	0.740	0.350	0.00064	0.00030	lb/ten	Water Suppression	50.0%	9, 2	3,10	6,23	.65
S Te CLP 15	2,500	21.900.000	0.740	0.550	0.00064	3,333,73	fs/ten	Water Suppression	60.0N	19.10	.549	9.22	1.00
S 146 CLP 14	2,500	2 ,600,000	0.740	0.350	0.00064	0.00030	le/ten	Water Suppression	50.03.	9, 0	3,10	6,23	.uā
S Te CLP 15	2.800	21.900.000	0.40	0.550	0.00064	3,333,73	lb/ten	Water Suppression	90.0N	19.10	.5.49	9.22	1.00
S 4 to VEP 1	2,000	7,520,000	0.740	0.350	0.00064	0.00030	lb/ten	Water Suppression	50.03.	5.29	2.70	7.23	.32
S 4 to CEP 2	2.000	173520.000	0.40	0.550	0.00064	0.000.0	fa/ten	Water Suppression	60.0X	16.28	2.79	7.2.9	1.2
S 4 to ChP 5	2,000	7,520,000	0.740	0.350	0.00064	0.00030	lb/ten	Water Suppression	50.03.	5.29	2.79	7.23	.32
S the CFP 1	2.000	173520.000	0.40	3250	0.00064	0.0002/0	lb/son	Water Suppression	10.02	15.28	2,59	7.25	1.2
5.4 to CEP +	2,000	7,520,000	0.740	0.350	2.22061	0.000230	lb/ten	Water Suppression	56.63	15.28	2,79	7,23	.32
Si the CEP o	2.000	17520.000	0.740	0.560	0.00064	0.000290	lb/ton	Water Suppression	10.0%	15.28	2,00	0.25	1.2
S 4 to CEP 2	2,000	7,520,000	0.700	0.350	2.00001	0.000230	lb/sen	Water Suppression	50.03.	15.28	2,79	7,23	.32
9 - 16 1 <b>9</b> 11	2.000	17820.000	2.42	3,50	2,22064	0.000220	llyton	Water Suppression	-0.0X	15.28	2,50	7.25	1.2
						۱ <u> </u>	i otissions Erc	l mi Coal/Petroke Stack	er: Total>>	450.7	<i>\$</i> 2.3	213.2	38,9
Coal Loadour to S-1	oadout Emission	s Finissions 35,040,000	0.750	0.350	0.00064	0.00030	b/ten	Water Suppression	50.03.	30.55	5.59	1,15	2.61
Coal/PetCoke Loadout to													
m. 2	550	1,9 9,000	0.740	0.350	0.000+1	0.00030	b/ten	Water Suppression	50.03	1.20	0.77		2.36
Percoke Loadout to S-1	-,	35,610,000	0.750	0.350	0.00064	0.00030 N	b/ten	Water Suppression	50.03. 	30.56	5.59	1,15 .80.9	2.64
						1.0		n Coal/Petcoke Loadou Coal/Petcoke Emission		65.4 1246.2	227.4	.40.9 589.4	54) 1074)
Salt f	tandling Finissio	ия Г	1	(	1	1	1	r	(	1	r		
ric (Fro SP 1 (Salt)	3,500	30,660,000	0.730	0.350	0.00064	0.00030	byten.	None	2.23	53,17	9,76	25.29	1.62

#### PROCESS UNITS POTENTIAL TO EMILICAT CLEATIONS.

DISCRIPTION		UM MAFERIAL D'ING RAFE <sup>7</sup>		PARTICLESIZE MULTIPLIER <sup>7</sup> FMISSION FACTORS <sup>7</sup>			CONTROL		PALEMISSION RATE		PAL <sub>P</sub> FAUSSION RAIT		
	ton/hr	ton/yr	PM	$PM_{36}$	PM	$PM_{10}$	axiis	1 YPF	marc.	lb⁄day	ton/yr	lb⁄day	ton/yr
<ul> <li>Section Transfer</li> <li>Points</li> </ul>	2,500	21.900.000	0.740	0.550	0.00064	0.000220	lb/ton	Nene	0.0%	o11.11	111.84	289.04	62./6
					•			ions Erom Salt Handlin		titi-1.ti	121.4		57.4
Soil Cria	hing/Screening I'm	tissions											
RPCS (Crushing)	140	1.226.400			0.0055	0.00101	lb/ton	Water Suppression	- 60.0N	1.14	1.01	1.73	2.21
RPCS (Screening)	110	1.226,400			0.00067	0.000034	ll/ton	Water Suppression	60.0N	1.12	0.21	2.87	2.13
						Euri	ssions From	Soil Crushing/Screenin	g: Total>>	6.7	1.2	2.3	0.4
								hacil	ity Total>>	1917.4	,149,9	906.0	165.3

. The nounly rate is based on \$,760 hours/year of operation.

2. Aeredonamic Particulate Size Mining in (k) per AP-12 Section 15.2, 1.5, Aggregate Handling and Storage Prios, 11700

Prinssion factor for material handling onlissions calculated per Equation 1 of AP 12 Section (3.2.4.3).

Aggregate Handling and Storage Piles.

4. mtp://www.nedchoaa.gov/ca/elmato/online/ecc/avgwind.htm

The coal and percede that are recoived at the facility nave non-moust ways or being conveyed through the facility. To be conservative in calculating the emissions, the pertable conveyors were chosen as the main method or moving the materials from the receiving areas.

Tacility has a water suppression system to control particulate matter emissions.

Coal and perceived at the Facility have an average measure content or 18.3% and 10.0% respectively. Emissions were calculated based on 2021 Emotyleput of perceive as exemations

#### Assumptions: BACKOROUND DATA

Coal/PerCoke moisture content tweighted average): 10.0% Operating Schedule = 24 twens/day Operating Schedule = 565 days/coar Operating Schedule = 8,500 hears/coar Maar wrig speet = 10.5 mph

### 1 ABET 2

DESCRIPTION	MANIMUM MATERIA UANDI ING RATE <sup>1</sup>			PARTICLESIZE MULTIPLUR <sup>7</sup>		SSION FAC	TORS	CONTRO	II.	PM IMISSION RATI.		PAL <sub>10</sub> FAUSSION R VIE	
	ton/hr	ton/yr	PM	$-PM_{40}$	PM	$PM_{10}$	UNTIS	түрт	EFTIC.	1b/day	ton/yr	1b/day	ton/yr
Storage Pile 1	Emissions			-			•						
ch na 17	N/A	N/A	1,300	d.pdd	4997.6	2479.8	lb/acro	Water Suppression	75,0%	176.55	24.74	\$7.77	12.W
CL: 27	NZA	NZA	.000	0.500	4947.0	3473.8	lb/acre	Water Suppression	75.0%	35.55	34,74	н7.77	3.37
CL 143 (	N/A	N/A	1.000	d.pdd	4942.6	2479.8	l lb/acro	Water Suppression	75.0%	176.55	24.74	57.77	12.37
ciusa /	N/A	N/A	.000	0.500	4947.0	3473.8	liny as no	Water Suppression	75.0%	35.35	34.74	57.77	2.37
CT 045 (	N/A	N/A	1.300	d.pdd	4947.0	2479.8	lb/acro	Water Suppression	75.0%	176.55	24.74	\$7.77	12.W
CL26 <sup>7</sup>	N/A	N/A	.200	0.500	4947.0	P <b>≟7</b> 7.8	liny as no	Water Suppression	75.0%	35.35	24.74	n7.77	2.37
CL 047 (	N/A	N/A	1.300	d.pdd	4962.6	2479.8	lb/acro	Water Suppression	75,0%	176.55	24.74	s7.77	12.W
CL187	NZA	N/A	.200	0.500	4947.0	3473.8	liny as no	Water Suppression	75.0%	35.55	34.74	<del>5</del> 7.77	2.37
(1 h-9 f	N/A	873	1.300	d.pdd	4942.6	2479.8	lo/acro	Water Suppression	V9.0%	176.55	24.74	67.77	12.3V
C1.19107	NZA	N/A	.300	0.500	4947.0	3473.8	lb/acre	Water Suppression	75.0%	35.55	34,74	<del>5</del> 7.77	2.37
crimu i k	N/A	N/A	1.300	0.500	494206	2479.8	lo/acro	Water Suppression	75,0%	176.55	24.74	67.77	12.W
CLF 12 <sup>7</sup>	NZA	N/A	.200	0.500	4947.0	3473.8	lb/acre	Water Suppression	75.0%	35.55	34.74	<del>5</del> 7.77	2.37
ci n4 37	N/A	N/A	1.000	d.pdd	4942.6	2479.8	lb/acro	Water Su <del>ppr</del> ession	75.0%	176.55	24.74	s7.77	12.3V
cius 147	N/A	N/A	.000	0.500	4947.0	3473.8	lin/ as no	Water Suppression	75.0%	35.35	34.74	57.77	2.37
CL D4 (5 /	N/A	N/A	1,300	d.pdd	4942.6	2479.8	lb/acre	Water Su <del>ppr</del> ession	75.0%	176.55	24.24	<del>6</del> 7.77	12.W
(17)-	NZA	N/A	.000	0.500	4947.0	2473.8	liny as no	Water Suppression	75.0%	35.35	24.74	57.77	2.37
Ch.F.2	N/A	N/A	1.300	t.ptt	4942.6	242/9.8	lb/acro	Water Su <del>ppr</del> ession	75.0%	176.55	24.74	67.77	12.W
CI72-3	N/A	N/A	.000	0.500	4947.0	2473.8	liny as no	Water Suppression	75.0%	35.35	24.74	57.77	2.37
CILE4	N/A	N/A	1.000	d.pdd	4942.6	242/9.8	lb/acro	Water Suppression	VB.0%	176.55	24.74	s7.77	12.37
CFP-5	N/A	N/A	.300	0.500	4947.0	2477.8	ley as re	Water Suppression	75.0%	35.55	34.74	h7.77	2.37
Clure	N/A	N/A	1.300	d.pdd	4942.6	2479.8	lo/acro	Water Suppression	75,0%	176.55	24.74	57.77	12.W
c1/047	N/A	N/A	.300	0.500	4947.6	2473.8	ley as re	Water Suppression	75.0%	35.55	34,74	h7.77	2.37
	N/A	N/A	1.300	d.add	4942.6	2479.8	lb/acro	Water Suppression	75.0%	33.89	5.18	15.94	9.09
		l	1	I	1	I	1	torage Pile Unission	ls: Total>>	3016.0	550.4	1508.0	275.2

DESCRIPTION		MAIAITRIAL LING RAITE <sup>T</sup>	PARTIC MULTI		i ARS	istox Laci	IORS	CONTRO	t)	PALIMISS	ION RAIT	$= \frac{PM_{10}}{R^3} \frac{F\Lambda}{R^3}$	
	ton/lir	ton/yr	PM	$-PM_{25}$	PM	$-PM_{25}$	UNTIS	T Y P4	EFFIC.	lb/day	ton/yr	lb/day	ton/yr
Reclaim Belt Loadin	ig Emissions		•		•		•				•		
ike – loaded by Dozen/Thid Leader T	3,000	8,780,000	0.240	0.750	0.00061	0.00030	lb/ton	Water Suppression	p0.0%	22.92	1.39	10.81	Clas
Ku 2 Libaded by Dozen/Tina Loader 4	3,000	8,750,000	0.740	0.350	0.00064	0.00030	lb/ter	Water Suppression	50.0%	22,92	1.36	10.84	0.mm
iku oʻribaded <del>iyy</del> Dozer/find floader V	3,000	8,750,000	0.740	0.350	0.00064	0.00030	'b/ter	Water Suppression	50.0%	22.92	1,79	10.84	0.nn
iku -= i loaded by Dozen/Tind Leader	3.000	8.750,000	0,240	0.750	0.00061	0.00030	.b/ton	Water Suppression	p0.0%	22.92	1.39	10.81	il.aa
Front End Loader" Readway Emissions	N/A	N/A	4,900	1.500	8.5	2.2	ISZANI.	Water Suppression	75.0%	25 Leb	40.47	55,59	11.99
Front and Loader <sup>2</sup> Koadway limissions	XZA -	N/A	4.900	1.500	8.5	2.2	167AN	Water Suppression	75.0%	254.65	40.47	55.5°	.44
KC billioadod by Dozor <sup>4</sup>	2,000	8,750,000	0.740	0.350	6,600,64	0.00020	'by ter	Water Suppression	50.0%	15.28	1.79	7.23	0.nn
KC 6 Hoadod by Dozen <sup>a</sup>	1.000	8.750,000	0,240	0.750	0.00061	0.00030	.b/ton	Water Suppression	p0.0%	7. <del>04</del>	1.39	3.61	il.aa
RC-7 Headed by Dezer <sup>1</sup>	1.000	8.780,000	0.240	0.350	0.00061	0.00030	.b/ton	Water Suppression	p0.0%	7. <b>0</b> 4	1.99	3.61	0.55
•	•		•	•	•		Reclaim B	di Coading Unission	is: 'Intal>>	631.5	102.7	189.2	28.6
Truck Loading F	missions												
Salt Toaded by find Leader <sup>4</sup>	bbt	4.818.000	3.740	0.750	0.00064	0.00030	.b/ton	None	0.3%	8.40	1.53	7,97	0.2/3
Ceal Leaded by Net Toatler <sup>1</sup>	475	4.161.000	::.740	0.350	0.00061	0.00030	.b/ton	Water Suppression	p0.0%	3.63	0.85	1.72	0.91
	<b>`</b>		•	•	•		Tru	ck-t-oading Unission	is: Total>>	12.0	2.2	5.7	1.0
Roadway I m	issions				,		,	1			,		•
Inhound Coal Truck	N/A	N/A	4,900	Lott	0.0	1.2	ISZANI.	l ugitive Dust Management Plan	VB.(0%)	0,00		0,00	
Outbound Ceal Thus k Thaths	N/A	N/A	4.900	Lotti	0.0	1.2	ISZANI.	- Eugiliya Dust Management Plan	75.0%	1074.83	196.12	277.23	o().59
Outbound Salt Truck Traffic <sup>®</sup>	NJA	NZA	4,900	1.500	0.0	1.7	157VV <sup>m</sup>	l ugitvə Dust Vəragement Plan	75.0%	244.2	227.09	391.00	.56.56
I			1	1	1	1	1	Roadway Emission	is: Total>>	2318.9	423.2	598,2	109.2
									ity Lotal>>	5978.5	1078.5	2301.1	+14.0

1. The neurly rate is based on 4,200 neurs/year of operation.

2. Accordynamic ParticulateSize Multiplier (k) per AP40 Section (3.3.4.9, Aggregate Hardling and Storage Priss, 11/00

3. Xlean Wind Speed (U) (estimate).

4. Emission factor for material bandling emissions ratio lated per Equation - of AP-42 Section 13.2.4.3,

Aggregate Handling and Storage files.

5. Emission factor for unpaved read emissions calculated per Equation AP42 Section (3.3.2, Unpaved Reads,

b. From National Weather Service (estimate).

Z. Frem: An Polluton Engineering Manual and References Section 9.3. (http://www.winapanteng/forums/ulej/full/contant/CD9-Storage\_Print WindB20Ensenr. ResDapul) .59 (fb/veet/acrossurface) = 1.7(s/1.5)(3e5)3e5 p]/23o)(5/15)

Couland percoke received at the Bachty have an average moisture content of 182% and 10.2% respectively. Emissions were adjulated based on 102% throughput of percoke as a worst-case scanario.

#### Assumptions:

COAL BACKGROUND DATA Coal/Fel Coke moisture content (weighted average) : 10.0% But content of coal = 15.0% TND FOADER/DOZER OPERATIONS Frent Find Toaders/Dezer (Storage Price) = 24 hears/day eront line Loaders/Dozer (Reclaim) = 24 nours/ day Operating Schedule = 124 hours/ day Operating Schedule = 1955 days/year Operating Schedule = -8,750 hears/ year From and a order/ Dozen sheed = 15.0 mph -XVI of Front Frid Loader/Dozer (Storage Piles) = -1200 miles/day VMT of Front End Loader/Dezer (Reclaim) = -1200 miles/day Front End Leader/Dezer Average Weight (Cat 980.) = 139 term STORAGE PILE INFORMATION Burface area of storage rules (Coal) = 140.0 acres Surface area of storage piles (Coke) = 140.0 acres Surface area of storage p iss(Salt) = -10.0 acres Days in storage pile = 366 days Number of days<sup>6</sup> with ram > 0.01 min = 117 days Meen wind speed<sup>4</sup> = 10.3 mpl: Persent of time? winds  $\geq 10$  mph = [41, 126]

#### INBOUND COAL TRUCK BACKGROUND DATA

Dolivery truck fare weight - 15 tons Maximum full truck weight - 29 toris-Average track weight= 22 Ions. Maximum facility input= 25,046,000 ton/year Maximum truck loadoar = 4,161,000 ton/ year Number of coactifices = 29/1214 trueles/year Miles portrip= 0.8 miles Alles per day = c5 of miles/day Miles per voer- 23/5/91 miles/year-OUTBOUND COAFTRUCK BACKGROUND DATA Delivery truck tare weight= 15 tons Maximum full truck weight= 29 tens Average track weight = 22 tons Maximum facility output - 35.040,000 ton/ year Maximum truck dolwerv= [4,15],6001cm/year. Number of coal trucks= 297,214 trucks/ year Miles per trip = 0.8 miles Miles per day= 001.4 miles/day Viles per veer- 227,771 miles/year-SALT HAULING TRUCK BACKGROUND DATA Delivery truck tare weight - 15 tons Maximum full truck weight - 29 tons. Average truck weight= 22 Ions. Maximum facility output= 4,8, \$,660 ten/year Maximum truck loading = 4,818,000 ton/year Number of coastrucks - 344143 trucks/year Allos por trip= 0.8 miles Miles per day = 754.3 miles/day Miles per voer= 2/5.314 miles/year-

# Page 1 of 2

## TABLE 3

## POTENTIAL TO EMIT CALCULATIONS DIESEL GENERATORS

				E	mission Fac	tor (lb/hp-hi	<i>י</i> )					
Unit	Unit ID		$NOx^{d}$	$CO^{d}$	$-SO_2^{-h}$	$PM^{y}$	$-PM_{16}^{\mu}$	VOM"				
Description		Prime Power	0.015	0.00815	34 Xi	0.0005	0.0005	0.00033				
		(hp)	Emissions (lh/ar)									
Diesel Generator 1	DG-1	118	1.77	0.96	0.021	0.06	0.06	0.04				
Diesel Generator 2	DG-2	118	1.77	0.96	0.021	0.06	0.06	0.04				
Diesel Generator 3	DG-3	118	1.77	0.96	0.021	0.06	0.06	0.04				
		Totals (lb/hr)	5.31	2.89	0.06	0.18	0.18	0.12				
		Totals (ton/yr) <sup>°</sup>	23.26	12.64	0.28	0.78	0.78	0.51				

			-	E	mission Fac	tor (lb/hp-hi	9	
Unit	Unit ID		$NOx^{d}$	$CO^{d}$	$SO_2^{-b}$	$PM^{y}$	$PM_{16}^{-d}$	VOM"
Description	unit	Prime Power	0.015	0.00573	**	0.0003	0.0003	0.00033
		(hp)			Emission	ıs (lb/hr)		
Diesel Generator 4	DG-4	500	7.50	2.86	0.043	0.15	0.15	0.17
Diesel Generator 5	DG-5	500	7.50	2.86	0.043	0.15	0.15	0.17
Diesel Generator 6	DG 6	500	7.50	2.86	0.043	0.15	0.15	0.17
Diesel Generator 7	DG-7	500	7.50	2.86	0.043	0.15	0.15	0.17
		lotals (lb/hr)	30.00	11.45	0.17	0.60	().6()	0.66
		Totals (ton/yr) <sup>c</sup>	131.40	50.17	0.75	2.63	2.63	2.89

				E	mission Fac	tor (lb/hp-h	r)				
Unit	Unit ID		$NOx^{d}$	$CO^{d}$	$-SO_2^{-h}$	$PM^{u}$	$PM_{10}^{d}$	VOM <sup>™</sup>			
Description		Prime Power	0.015	0.00815	34-35	0.0005	0.0005	0.00033			
		(hp)	Emissions (lb/hr)								
Air Compressor	AC-1	100	1.50	0.82	0.02	0.05	0.05	0.03			
		Totals (lb/hr)	1.50	0.82	0.02	0.05	0.05	0.03			
		Totals (ton/yr) <sup>c</sup>	6.57	3.57	0.09	().22	0.22	0.14			

## POTENTIAL TO EMIT CALCULATIONS DIESEL GENERATORS

				E	mission Fac	tor (Ib/hp-hi	r)						
Unit	Unit ID		$NOx^{d}$	$CO^{d}$	$-SO_2^{-h}$	$PM^{y}$	$PM_{10}^{d}$	VOM <sup>™</sup>					
Description		Prime Power	0.015	0.00903	**	0.001	0.001	0.00033					
		(hp)	Emissions (lb/ar)										
Light Standard	1.5-1	15	0.23	0.14	0.01	0.02	0.02	0.005					
Light Standard	LS 2	15	0.23	0.14	0.01	0.02	0.02	0.005					
Light Standard	1.5-3	15	0.23	0.14	0.01	0.02	0.02	0.005					
Light Standard	LS-4	15	0.23	0.14	0.01	0.02	0.02	0.005					
Light Standard	1.5-5	15	0.23	0.14	0.01	0.02	0.02	0.005					
		Totals (lb/hr)	1.13	0.68	0.05	0.08	0.08	0.02					
		Totals (ton/yr) °	4.93	2.97	0.23	0.33	0.33	0.11					

		Emission Factor (lb/hp-hr)										
		$NOx^{d}$	$CO^{d}$	$SO_2^{b}$	$PM^{g}$	$PM_{16}^{-d}$	$VOM^{d}$					
unitID	Prime Power	0.015	0.01079	**	0.0013	0.0013	0.00033					
	(lip)	Emissions (lb/hr)										
DWP 1	20	0.30	0.22	0.01	0.03	0.03	0.01					
	□ otals (lb/hr)	0.30	0.22	0.01	0.03	0.03	0.01					
	fotals (ton/yr) <sup>c</sup>	0.08	0.05	0.003	0.01	0.01	0.002					
Facility En	ussions (ton/vr)	166.23	69.39	1.36	3.96	3.96	3.66					
		Prime Power       (hp)       DWP 1     20       Totals (lb/hr)       Totals (ton/yr)*	Unit ID         Prime Power         0.015           Prime Power         0.015           Opp         0.015           Opp         0.30           Totals (lb/hr)         0.30	Unit ID $NOx^{d}$ $CO^{d}$ Prime Power $0.015$ $0.010/9$ DWP 1         20 $0.30$ $0.22$ Totals (lb/hr) $0.30$ $0.22$ Totals (ton/yr) $0.08$ $0.05$	NOx* $CO^*$ $SO_2^{b}$ Prime Power $0.015$ $0.010/9$ **           (hp) $0.30$ $0.22$ $0.01$ DWP 1         20 $0.30$ $0.22$ $0.01$ Totals (lb/hr) $0.30$ $0.22$ $0.01$ Totals (ton/yr)* $0.08$ $0.05$ $0.003$	$NOx^{a}$ $CO^{a}$ $SO_{2}^{b}$ $PM^{a}$ Prime Power $0.015$ $0.010/9$ ** $0.0013$ (hp) $Imission(lb/hr)$ $Imission(lb/hr)$ $Imission(lb/hr)$ DWP 1         20 $0.30$ $0.22$ $0.01$ $0.03$ Totals (lb/hr) $0.30$ $0.22$ $0.01$ $0.03$ Totals (lb/hr) $0.08$ $0.05$ $0.003$ $0.01$	$NOx^{d}$ $CO^{d}$ $SO_2^{b}$ $PM^{d}$ $PM_{46}^{d}$ Prime Power (hp)         0.015         0.010/9         **         0.0013         0.0013           DWP 1         20         0.30         0.22         0.01         0.03         0.03           Totals (lb/hr)         0.30         0.22         0.01         0.03         0.03           Totals (ton/yr)         0.08         0.05         0.003         0.01         0.01					

PTF Emissions Assumptions:

Calculated using NSPS emission factors for stationary combustion sources (40 CFR Part 89, Section 112). VOM emission \* factor from Permit #07050082 issued on May 21, 2009.

." Calculated using low sulfur diesel fuel and formula used in Permit #07050082 issued on May 21, 2009 with revised diesel fuel consumption data as follows:

500 HP Engine	20 gal/hr
100 & 118 HP Engines	10 gal/hr
15 & 20 HP Engines	3 gal/hr
* Hours of operation	8,760 hr/yr
	500 hr/yr

(For emergency diesel water pump only.)

 $^{-2}$  It is assumed that PM  $_{\rm B}$  emissions are equal to PM.

### Example Calculation

500 HP Diesel Engine  $NO_X$  Emissions –

565 horsepsacer x 0.515 lb NO  $_\odot$  per horsepsacer hour x 8,760 hr/yr / 2,005 lb/ton - 32.85 ton/yr NO  $_\odot$ 

## Conversion of NSPS Emission Factors

 $NO_X = 9.2 \text{ g/kW-hr}$  or 6.9 g/HP-hr 6.9 g/HP-hr /454 g per pound = 0.015 lb/hp-hr

## TABLE 3A

			Diesel Engines	
CAS No.	Pollutant	Emission Factor <sup>a</sup> (Ib/hp-hr)	Emission Rate <sup>b</sup> (Ib/Iır)	Emission Rate <sup>c</sup> (ton/yr)
71-43-2	Benzene	6.56E-06	1.67E-02	7.32E-02
108-88-3	Toluene	2.88E-06	7.33E-03	3.21E-02
1330207	Xylene	2.00E-06	5.11E-03	2.24E-02
106-99-0	1,3-Butadiene	2.75E-07	7.01E-04	3.07E-03
50-00-0	Formaldehyde	8.29E-06	2.11E-02	9.26E-02
75070	Acetaldehyde	5.39E-06	1.37E-02	6.02E-02
107028	Acrolein	6.50E-07	1.66E-03	7.26E-0?
91-20-3	Naphthalene	5.96E-07	1.52E-03	6.66E-0?
		HAP Totals:	6.79E-02	2.97E-01

# POTENTIAL TO EMIT HAP CALCULATIONS DIESEL GENERATORS

<sup>a</sup> AP-42, Fifth Edition, Volume I, Section 3.3, Gasoline and Industrial Engines (October 1996)
 <sup>b</sup> Diesel Fuel-Fired Engines maximum heat input
 <sup>c</sup> Diesel Fuel-Fired Engines maximum hours of operation
 8760 hr/yr
 Emission Factor Conversion Factor
 0.007

Calculated by dividing the emission factor for Nox (lb/hp-hr) into the NO<sub>X</sub> emission factor (lb/MMBtu). This provides a conversion factor for use with HAP emission calculation.

0.031 lb/hp-hr / 4.41 lb/MMBtu = 0.007

CRA 652450 01a 13A

## PTE EMISSIONS SUMMARY

	Emissions (ton/yr)											
Emission Point	NOx	со	<b>SO</b> <sub>2</sub>	РМ	PM 10	VOM						
Process				349.93	165.35							
Generator	166.23	69.39	1.36	3.96	3.96	3.66						
Total	166.23	69.39	1.36	353.89	169.30	3.66						

### MAXIMUM PROCESS UNITS EMISSION CALCULATIONS.

DESCRIPTION		UM MATERI M DI ING RATE <sup>T</sup>	PARTIC MULTI		EMIS	SIONTACT	ORS <sup>1</sup>	CONTROL		PMLMISS	HON RALL		JISSION ATE
	ton/la	ton/yr	PM	$PM_{B}$	PM	$PM_{Ab}$	UNTES	TYPL	LITIC.	lb/day	ton/yr	lly/day	ton/yr
Coul/Pet	coke Unloading En	rissions	·										
BU-1 to C (1-6) (Coal/Petcoke)	266	1,117,200	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	1.02	0.18	0.48	0.08
RU/TU-1 to C-(1-6) (Coal/Petcoke)	266	1,117,200	0.740	0.350	0.00064	0.00030	lhs/ton	Water Suppression	50.0%	1.02	0.18	0.48	0.08
RU/TU-L to C (L 6) (Coal/Petcoke)	266	1,117,200	0.740	0.350	0.00064	0.00030	lbs/ton	Baghouse	90.0%	0.20	0.04	0.10	0.02
RU-2 to C-7 (Coal/Petcoke)	2,000	8,400,000	0.740	0.350	0.00064	0.00030	lhs/tan	Water Suppression	50.0%	7.64	1.34	3.61	0.63
RU-3 to C-8 (Coal/Petcoke)	2,000	8,400,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	7.64	1.34	3.61	0.63
	·	·	-	·	·	Emis	dons From (	`oal/Petcoke Unloadin	g : Fotal>>	17.5	3.1	8.3	13
Coal/Petcoke (*	onveyo <del>r</del> Transfer P	oint Emissions											
C-1 to C-2	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lhs/ton	Water Suppression	50.0%	9.55	1.67	4.52	0.79
C 2 to S 1	4,000	11,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	15.28	1.75	7.23	0.83
C-3 to C-2	4,000	11,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	15.28	1.75	7.23	0.83
С 6 to S 3	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	9.55	1.67	4.52	0.79
C-1 to C-4	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lbs/tan	Water Suppression	50.0%	9.55	1.67	4.52	0.79
C4 to C⊃	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	9.55	1.67	4.52	0.79
C-5 to S-2	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lbs/tan	Water Suppression	50.0%	9.55	1.67	4.52	0.79
RC 1-ю-С 3	3,000	11,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	11.46	1.75	5.42	0.83
RC-2 to C-3	3,000	11,000,000	0.740	0.350	0.00064	0.00030	lbs/tan	Water Suppression	50.0%	11.46	1.75	5.42	0.83
RC 3 to C 3	3,000	11,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	11.46	1.75	5.42	0.83
RC-4 to C-3	3,000	11,000,000	0.740	0.350	0.00064	0.00030	lbs/tan	Water Suppression	50.0%	11.46	1.75	5.42	0.83
C 7 to C 9	2,000	8,400,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	7.64	1.34	3.61	0.63
C-8 ta C-10	2,000	8,400,000	0.740	0.350	0.00064	0.00030	lbs/tan	Water Suppression	50.0%	7.64	1.34	3.61	0.63
C 9 to C 11	2,000	8,400,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	7.64	1.34	3.61	0.63
C-10 to C-11	2,000	8,400,000	0.740	0.350	0.00064	0.00030	lhs/tan	Water Suppression	50.0%	7.64	1.34	3.61	0.63
C 11 to []? 1	2,000	8,400,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	7.64	1.34	3.61	0.63
TP-1 to C-12	2,000	8,400,000	0.740	0.350	0.00064	0.00030	lhs/tan	Water Suppression	50.0%	7.64	1.34	3.61	0.63
C 12 to SPTP 1	2,000	8,400,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	7.64	1.34	3.61	0.63

### MAXIMUM PROCESS UNITS EMISSION CALCULATIONS.

DESCRIPTION		UM MATERI M DI ING RATE <sup>T</sup>		PARTICI ESIZE MULTIPI IER <sup>3</sup>		SION EVER	ORS <sup>1</sup>	CONTROL		PMEMISS	GON RALL		IISSION ITE
	ton/la	ton/yr	PM	$PM_{\rm ff}$	PM	$PM_{15}$	UNITS	TYPL	LITIC.	lb/day	ton/yr	lb/day	ton/yr
SETP-1 to S-4	2,000	8,400,000	0.740	0.350	0.00064	0.00030	lb5/ton	Water Suppression	50.0%	7.64	1.34	3.61	0.63
DSH 1 to C 3	2,000	8,400,000	0.740	0.350	0.00064	0.00030	lbs/tan	Water Suppression	50.0%	7.64	1.34	3.61	0.63
RC-5 to C-3	1,000	4,200,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	3.82	0.67	1.81	0.32
RC 6 to C 3	1,000	4,200,000	0.740	0.350	0.00064	0.00030	lbs/tan	Water Suppression	50.0%	3.82	0.67	1.81	0.32
RC-7 to C-3	1,000	4,200,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	3.82	0.67	1.81	0.32
Contractor	Portable Conveyo	a Doubeed con-				Divissions	From Coul/	Petcoke Transfer Poin	s: Total>>	204.3	32.9	96.0	15.6
PC-1 Drap Point	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	9.55	1.67	4.52	0.79
PC 2 Drop Point	2,500	10,300,000	0.740	0.350	0.00064	0.00030	lhs/tan	Water Suppression	50.0%	9.55	1.67	4.52	0.79
PC-3 Drop Point	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	9.55	1.67	4.52	0.79
PC 4 Drop Point	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lbs/tan	Water Suppression	50.0%	9.55	1.67	4.52	0.79
PC-5 Drap Point	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	9.55	1.67	4.52	0.79
PC 6 Drop Point	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lhs/tan	Water Suppression	50.0%	9.55	1.67	4.52	0.79
PC-7 Drap Point	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	9.55	1.67	4.52	0.79
PC 8 Drop Point	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lhs/tan	Water Suppression	50.0%	9.55	1.67	4.52	0.79
PC-9 Drap Point	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lb5/ton	Water Suppression	50.0%	9.55	1.67	4.52	0.79
PC-10 Drop Point	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lbs/tan	Water Suppression	50.0%	9.55	1.67	4.52	0.79
PC-11 Drop Point	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	9.55	1.67	4.52	0.79
PC 12 Drop Point	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lhs/tan	Water Suppression	50.0%	9.55	1.67	4.52	0.79
PFH-1 to PC-(1-12)	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	9.55	1.67	4.52	0.79
PF-1 to PC (1-12)	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lhs/tan	Water Suppression	50.0%	9.55	1.67	4.52	0.79
RPCS-1 to PC-(1-12)	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	9.55	1.67	4.52	0.79
	1	1		Lunis.	i sions From (	loul/Petcoke	Portable Co	i incegor Fransfer Poin	s: Total>>	143.2	25.7	67.7	11.9

### MAXIMUM PROCESS UNITS EMISSION CALCULATIONS.

DESCRIPTION		UM MATERI M DI ING RATE <sup>7</sup>	1	PARTICLESIZE MULTIPLIER <sup>7</sup>		SION FACT	ORS <sup>1</sup>	CONTROL		PMEMISSION RATE			JISSION ME
	ton/la	ton/yr	PM	$PM_{4k}$	PM	$PM_{15}$	UNITS	TYPL	LITIC.	lb/day	ton/yr	Ry/day	ton/yr
Coul/P	etcoke Stacker Lini	ssions T			······					γ	· ·		······
S-1 to CLP-5	4,000	11,000,000	0.740	0.350	0.00064	0.00030	lbs/tan	Water Suppression	50.0 <i>%</i>	15.28	1.75	7.23	0.83
5-1- to CLP 4	4,000	11,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	15.28	1.75	7.23	0.83
S-2 to CLP-2	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lhs/tan	Water Suppression	50.0%	9.55	1.67	4.32	0.79
5-2 to CLP 3	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	9.55	1.67	4.52	0.79
S-3 to CEP-1	2,500	10,300,000	0.740	0.350	0.00064	0.00030	lbs/tan	Water Suppression	50.0%	9.55	1.67	4.52	0.79
5-3- to CLP 4	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	9.55	1.67	4.52	0.79
S-1 to CLP-6	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lhs/tan	Water Suppression	50.0%	9.55	1.67	4.52	0.79
5-1- to CLP 7	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	9.55	1.67	4.52	0.79
S-1 to CI P-8	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lhs/tan	Water Suppression	50.0%	9.55	1.67	4.52	0.79
5-1-to-CLP 9	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	9.55	1.67	4.52	0.79
S-1 to CTP-10	2,500	10,300,000	0.740	0.350	0.00064	0.00030	lbs/tan	Water Suppression	50.0%	9.55	1.67	4.52	0.79
5-1-to-CLP-11	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	9.55	1.67	4.52	0.79
S-1 to CLP-12	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lhs/ton	Water Suppression	50.0%	9.55	1.67	4.52	0.79
5-1-to-CLP-13	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	9.55	1.67	4.52	0.79
S-1 to CLP-14	2,500	10,300,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	9.55	1.67	4.52	0.79
5-1-to-CLP-15	2,500	10,500,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	9.55	1.67	4.52	0.79
S-4 to CFP-1	2,000	8,400,000	0.740	0.350	0.00064	0.00030	lbs/tan	Water Suppression	50.0%	7.64	1.34	3.61	0.63
5-4 to CEP 2	2,000	8,400,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	7.64	1.34	3.61	0.63
S-4 to CFP-3	2,000	8,400,000	0.740	0.350	0.00064	0.00030	lbs/tan	Water Suppression	50.0%	7.64	1.34	3.61	0.63
5-4 to CEP 4	2,000	8,400,000	0.740	0.350	0.00064	0.00030	lb5/ton	Water Suppression	50.0%	7.64	1.34	3.61	0.63
S-4 to CFP-5	2,000	8,400,000	0.740	0.350	0.00064	0.00030	lbs/tan	Water Suppression	50.0%	7.64	1.34	3.61	0.63
5-4 to CEP 6	2,000	8,400,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	7.64	1.34	3.61	0.63
S-4 to CFP-7	2,000	8,400,000	0.740	0.350	0.00064	0.00030	lbs/tan	Water Suppression	50.0%	7.64	1.34	3.61	0.63
5-4 to D5FL 1	2,000	8,400,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	7.64	1.34	3.61	0.63
	•	•	•	•	•	Lin	nissions Fro	m Coal/Petcoke Stacki	m Total>>	225.3	37.6	106.6	17.8

#### MAXIMUM PROCESS UNITS EMISSION CALCULATIONS

DESCRIPTION	MANIMUM MATERI M HANDLING RATE <sup>1</sup>			PARTICLESIZE MULTIPLIER <sup>7</sup>		MISSION FACTORS <sup>1</sup>		CONTROL		PM1MISSION RAIL		PM <sub>B</sub> EMISSION RAIT	
	ton/la	ton/yr	PM	$PM_{(6)}$	1244	$PM_{16}$	UNITS	TYPL	LITIC.	lb/day	ton/yr	Ry/day	ton/yr
Coul/Petcoke t	oudout Emission	s Emissions											
Coal Loadout to S-1	4,000	11,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	15.28	1.75	7.23	0.83
Coal/Pet Coke Loadout to 11, 2	550	2,310,000	0.740	0.350	0.00064	0.00030	lbs/tan	Water Suppression	50.0%	2.10	0.37	0.99	0.17
Petcoke Loadout to 5-1	4,000	11,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	15.28	1.75	7.23	0.83
			•		•	Em	issions Fron	i Coal/Petcoke Loadou	it: Fotal>>	.32.7	3.9	154	1.8
							(	'oul/Petcoke Emission	is: Fotal>>	623.7	102.5	294.7	48.5
Salt f	tandling Emissio	ns	_		_	_							
BU-1 to SP-1 (Salt)	3,500	250,000	0.740	0.350	0.00064	0.00030	lbs/ton	None	0.0%	26.74	0.08	12.65	0.04
16 Various Transfer Points	2,500	250,000	0.740	0.350	0.00064	0.00030	lbs/ton	None	0.0∿	305.56	1.27	144.52	0.60
		•	•		•	•	Timissi	ons From Salt Handlin	g: Total>>	332.3	1.4	157.2	0.6
Soil Crush	ing/Screening Lin	issions											
RPCS 1 (Crushing)	140	306,600			0.0033	0.00101	lbs/ton	Water Suppression	50.0%	2.77	0.25	0.85	0.08
RPCS 1 (Screening)	140	306,600			0.00067	0.00034	lbs/ton	Water Suppression	50.0%	0.56	0.05	0.29	0.03
						Emis	sions From	Soil Crushing/Screenin	g: Total>>	3.3	θ.3	I.7	0.1
								Facil	ity Total>>	958.7	104.1	453.0	49.2

1. The hourly rate is based on 4,200 hours/year of operation.

2. Aerodynamic Particulate Size Multiplier (k) per AP 42 Section 13.2.4.3, Aggregate Handling and Storage Piles, 11/06

3. Emission factor for material handling emissions calculated per Equation 1 of AP 42 Section 13.2.4.3,

Aggregate Handling and Storage Piles.

4. http://www.nedc.noaa.gov/oa/climate/online/ccd/avgwind.html

The coal and petcoke that are received at the facility have numerous ways of being conveyed through the facility. To be conservative in calculating the emissions, the portable conveyors were chosen as the main method of moving the materials from the receiving areas.

Facility has a water suppression system to control particulate matter emissions.

Coal and pet coke received at the Facility have an average moisture content of 18.3% and 10.0% respectively. Emissions were calculated based on 100% throughput of pet coke as a worst case scenario.

### Assumptions:

#### BACKGROUND DATA

Coal/Pet Coke moisture content (weighted average): 10.0%

- Operating Schedule = 12 hours/day
- Operating Schedule = 350 days/year
- Operating Schedule = -4,200 hours/year
- Mean wind speed 10.3 mph

### MAXIMUM FUCITIVE EMISSIONS CALCULATIONS

DESCRIPTION		M MATERIAL 'ING RATE <sup>T</sup>		PARTICLE SIZE MULTIPLIER <sup>®</sup>		SION FAC	IORS	CONTI	OL.	R	AISSION AIT:	R/	MISSION ATE
	ton/lir	ton <b>y</b> yr	РМ	$PM_{B}$	PM	$-PM_{B_{1}}$	UNITS	TYPE	- EHTIC,	lb/day	ton/yr	lb/day	ton∳yr
Storage Pile En								Water					
CLP-1 <sup>2</sup>	N/A	N/A	1.000	0.500	4744.2	2372.1	lbs/acre	Suppression	75.0 <sup>n</sup> /a	129.98	23.72	64.99	11.86
CLP-2 <sup>17</sup>	N/A	N/A	1.000	0.500	4744.2	2372.1	lbs/acre	Water Suppression	75.0 <sup>n</sup> /a	129.98	23.72	64.99	11.86
CLP-3 <sup>17</sup>	N/A	N/A	1.000	0.500	4744.2	2372.1	lbs/acre	Water Suppression	75.0 <sup>%</sup>	129.98	23.72	64.99	11.86
$\text{CLP-4}^{\text{S}}$	N/A	N/A	1.000	0.500	4744.2	2372.1	lbs/acre	Water Suppression	75.0 <sup>n</sup> /a	129.98	23.72	64.99	11.86
CLP-5 <sup>17</sup>	N/A	N/A	1.000	0.500	4744.2	2372.1	lbs/acre	Water Suppression	75.0%	129.98	23.72	64.99	11.86
CLP-6 <sup>17</sup>	N/A	N/A	1.000	0.500	4744.2	2372.1	lbs/acre	Water Suppression	75.0%	129.98	23.72	64.99	11.86
CLP-7 <sup>17</sup>	N/A	N/A	1.000	0.500	4744.2	2372.1	lbs/acre	Water Suppression	7.5.0 <sup>%</sup>	129.98	23.72	64.99	11.86
CLP-8 <sup>17</sup>	N/A	N/A	1.000	0.500	4744.2	2372.1	lbs/acre	Water Suppression	$75.0^{n}_{20}$	129.98	23.72	64.99	11.86
CLP-9 <sup>17</sup>	N/A	N/A	1.000	0.500	4744.2	2372.1	lbs/acre	Water Suppression	$75.0_{20}^{n}$	129.98	23.72	64.99	11.86
CLP-10 <sup>17</sup>	N/A	N/A	1.000	0.500	4744.2	2372.1	lbs/acre	Water Suppression	75.0%	129.98	23.72	64.99	11.86
CLP-11 <sup>17</sup>	N/A	N/A	1.000	0.500	4744.2	2372.1	lbs/acre	Water Suppression	75.0%	129.98	23.72	64.99	11.86
CLP-12 <sup>17</sup>	N/A	N/A	1.000	0.500	4744.2	2372.1	lbs/acre	Water Suppression	75.0%	129.98	23.72	64.99	11.86
CLP-13 <sup>17</sup>	N/A	N/A	1.000	0.500	4744.2	2372.1	lbs/acre	Water Suppression	75.0%	129.98	23.72	64.99	11.86
CLP-14 <sup>11</sup>	N/A	N/A	1.000	0.500	4744.2	2372.1	lbs/acre	Water Suppression	75.0%	129.98	23.72	64.99	11.86
CLP-15 <sup>17</sup>	N/A	N/A	1.000	0.500	4744.2	2372.1	lbs/acre	Water Suppression	75.0%	129.98	23.72	64.99	11.86
СТР I	N/A	N/A	1.000	0.500	4744.2	2372.1	lbs/acre	Water Suppression	75.0%	129.98	23.72	64.99	11.86
CFP-2	N/A	N/A	1.000	0.500	4744.2	2372.1	lbs/acre	Water Suppression	75.0 <sup>n</sup> /2	129.98	23.72	64.99	11.86
CFP 3	N/A	N/A	1.000	0.500	4744.2	2372.1	lbs/acre	Water Suppression	75.0 <sup>n</sup> /2	129.98	23.72	64.99	11.86
CEP 4	N/A	N/A	1.000	0.500	4744.2	2372.1	lbs/acre	Water Suppression	75.0 <sup>n</sup> /2	129.98	23.72	64.99	11.86
CEP 5	N/A	N/A	1.000	0.500	4744.2	2372.1	lbs/acre	Water Suppression	75.0 <sup>n</sup> /a	129.98	23.72	64.99	11.86

KM00000440

	MAXIMU	IM MATERIAL PARTICLE SIZE		1.1415	I MISSION FACTORS			CONTROL		PM EMISSION			
DESCRIPTION	HAND	LING RATE	MULTI	PETER <sup>2</sup>	1.003		CAC5	CONTR	. <i>CH</i> .	R.	AIT:	R/	ATE
	tons/hr	tons/year	PM	$PM_{16}$	PM	$PM_{16}$	UNHS	TYPE	ETTC.	lb/day	lpy	lb/day	tрy
FP 6	N/A	N/A	1.000	0.500	4744.2	2372.1	lbs/acre	Water Suppression	75.0 <sup>a</sup>	129.98	23.72	64.99	11.86
'FP 7	N/A	N/A	1.000	0.500	4744.2	2372.1	lbs/acre	Water Suppression	75.0%	129.98	23.72	64.99	11.86
5P-1	N/A	N/A	1.000	0.500	4744.2	2372.1	lbs/acre	Water Suppression	75.0 <sup>n</sup> ,a	32.49	5.93	16.25	2.97
							Stori	ge Pile Emission	is: Total>>	2892.0	527 <b>.8</b>	1446.0	263.9
-Reclaim Belt Loadin	g Emissions			•	•		•	•					
&C.1. Loaded by Dozer/End Loader <sup>1</sup>	3,000	2,750,000	0.740	0,350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	11.46	0.44	5.42	0.21
RC 2: Loaded by Dozer/End Loader <sup>1</sup>	3,000	2,750,000	0.740	0,350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	11.46	0.44	5.42	0.21
RC 3: Loaded by Dozer/End Loader <sup>1</sup>	3,000	2,750,000	0.740	0,350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	11.46	0.44	5.42	0.21
RC 4: Loaded by Dozer/Find Loader <sup>1</sup>	3,000	2,750,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	11.46	0.44	5.42	0.21
front End Loader Roadway Emissions	N/A	N/A	4.900	1,500	8.5	2.2	lbs/VMT	Water Suppression	75.0%	127.32	22.28	32,85	5.75
front End Loader Roadway Emissions	N/A	N/A	4.900	1,500	8.5	2.2	lbs/VMT	Water Suppression	75.0%	127.32	22.28	32,85	5.75
RC 5   Loaded by Dozer <sup>4</sup>	2,000	2,750,000	0.740	0,350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	7.64	0.44	3.61	0.21
€C 6 - Loaded by Dozer <sup>4</sup>	1,000	2,750,000	0.740	0,350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	3.82	0.44	1.81	0.21
RC 7 - Loaded by Dozer <sup>4</sup>	1,000	2,750,000	0.740	0,350	0,00064	0.00030	lbs/ton	Water Suppression	50.0%	3.82	0.44	1.81	0 <b>.</b> 21
						Re	claim Belt I.	oading Emission	is: Total>>	315.8	47.6	94.6	12.9
Fruck Loading Fr	nissions												
alt Loaded by End oader <sup>1</sup>	550	250,000	0.740	0,350	0.00064	0.00030	lbs/ton	None	0.0%	4.20	0.08	1.99	0.04
loat Loaded by End oader <sup>4</sup>	475	1,995,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	1.81	0.32	0.86	0.15
•			•	•	•		Truck I.	ouding Emission	is: Total>>	6.0	0.4	2.8	0.2
Roadway I mis	sions												
nbound Coal Truck Taffic <sup>5</sup>	N/A	N/A	4.900	1.500	6.6	1.7	lbs/VMT	Fugitive Dust Management Plan	75.0 <sup>m</sup>	296.27	51.85	76.43	13.37
Dutbound Coal Truck Traffic <sup>5</sup>	N/A	N/A	4.900	1.500	6.6	1.7	lbs/VMT	Fugitive Dust Management Plan	75.0%	296.27	51.85	76.43	13.37
Dutbound Salt Truck Traffic <sup>5</sup>	N/A	N/A	4.900	1,500	6.6	1.7	lbs/VMT	Fugitive Dust Management Plan	75.0%	67.33	11.78	17.37	3.04
1			•		1		Ro	adreay Emission	is: Total>>	659.9	115.5	170.2	29,8
								Faci	lity Total>>	3873.7	691.3	1713.7	306.8

2. Aerodynamic Particulate Size Multiplier (k) per AP-42 Section 13.2.4.3, Aggregate Handling and Storage Piles, 11/06

3. Mean Wind Speed (U) (estimate).

4. Emission factor for material handling emissions calculated per Equation 1 of AP-42 Section 13.2.4.3,

Aggregate Handling and Storage Piles.

5. Emission factor for unpaved road emissions calculated per Equation AP-42 Section 13.2.2, Unpaved Roads.

6. From National Weather Service (estimate).

7. From Air Pollution Engineering Manual and References Section 9.3. (http://www.wrapair.org/forums/dejf/fdh/content/Ch9-Storage\_Pile\_Wind%20Erosion\_Rev06.pdf) TSP (lb/year/acrea surface) = 1.7(s/1.3)(365]363-p]/235)(f/15)

Coal and pet coke received at the Facility have an average moisture content of 18.3% and 10.0% respectively. Emissions were calculated based on 100% throughput of pet coke as a worst-case scenario.

### Assumptions:

COAL BACKGROUND DATA Coal/Pet Coke moisture content (weighted average): 10.0% Silt content of coal - 5.0% END LOADER/DOZER OPERATIONS Front End Loaders/Dozer (Storage Piles) - 12 hours/day Front End Loaders/Dozer (Reclaim) - 12 hours/day Operating Schedule - 12 hours/day Operating Schedule - 350 days/year Operating Schedule - 4,200 hours/year Front End Loader/Dozer speed - 5.0 mph VMT of Front End Loader/Dozer (Storage Piles) = -60.0 miles/day VMT of Front End Loader/Dozer (Reclaim) - 60.0 miles/day Front End Loader/Dozer Average Weight (Cat 980) - 39 tons STORAGE PILE INFORMATION Surface area of storage piles (Coal) - 40.0 acres Surface area of storage piles (Coke) - 40.0 acres Surface area of storage piles (Salt) - 10.0 acres Days in storage pile - 350 days Number of days<sup>5</sup> with rain > 0.01 inch = 117 days Mean wind speed = 10.3 mph Percent of time<sup>7</sup> winds > 12 mph = 34,0% INBOUND COAL TRUCK BACKGROUND DATA Delivery truck tare weight= 15 tons Maximum full truck weight= 29 tons Average truck weight- 22 tons Maximum facility input- 11,000,000 tons/year Maximum truck loadout= 1,100,000 tons/year Number of coal trucks= 78,571 trucks/year Miles per trip- 0.8 miles Miles per day- 179.6 miles/day Miles per year= 62,857 miles/year

### OUTBOUND COAL TRUCK BACKGROUND DATA

Delivery truck fare weight- 15 tons Maximum full truck weight- 29 tons Average truck weight= 22 tons Maximum facility output- 11,000,000 ton/year Maximum truck delivery- 1,100,000 ton/year Number of coal trucks- 78,571 trucks/year Miles per trip- 0.8 miles Miles per day- 179.6 miles/day Miles per year- 62,857 miles/year SALT HAULING TRUCK BACKGROUND DATA Delivery truck tare weight- 15 tons Maximum full truck weight- 29 tons Average truck weight= 22 tons Maximum facility output- 250,000 ton/year Maximum truck loading- 250,000 ton/year Number of coal trucks- 17,857 trucks/year Miles per trip- 0.8 miles Miles per day- 40.8 miles/day Miles per year- 14,286 miles/year

## MAXIMUM EMISSION CALCULATIONS DIESEL GENERATORS

				E	mission Fac	tor (lb/hp-hi	9					
Unit	Unit ID		$NOx^{d}$	CO''	$SO_2^{(6)}$	$PM^{u}$	$PM_{19}^{-d}$	-VOM''				
Description		Prime Power	0.015	0.00815	si; 55	0.0005	0,0005	0.00033				
		(hp)	tunissions (lb/hr)									
Diesel Generator 1	DG 1	118	1.77	0,96	0.021	0,06	0.06	0.04				
Diesel Generator 2	DG 2	118	1.77	0.96	0.021	0.06	0.06	0.04				
Diesel Generator 3	DG 3	118	1.77	0.96	0.021	0.06	0.06	0.04				
		Totals (lb/hr)	5.31	2.89	0.06	0.18	0.18	0.12				
		Totals (ton/yr) $^{\circ}$	11.15	6.06	0.13	0.37	0.37	0.25				

				E	mission Fac	tor (lb/hp-hi	)						
Unit	Unit ID		$NOx^{d}$	CO''	$SO_2^{(6)}$	PM''	$-PM_{19}^{-d}$	VOM"					
Description	ann D	Prime Power	0.015	0.00573	34-35	0.0003	0.0003	0.00033					
		(hp)	Emissions (lb/ur)										
Diesel Generator 4	DG-4	500	7.50	2.86	0.043	0.15	0.15	0.17					
Diesel Generator 5	DG-5	500	7.50	2.86	0.043	0.15	0.15	0.17					
Diesel Generator 6	DG-6	500	7.50	2.86	0.043	0.15	0.15	0.17					
Diesel Generator 7	DG-7	500	7.50	2.86	0.043	0.15	0.15	0.17					
		Totals (lb/hr)	30.00	11.45	0.17	0,60	0.60	0.66					
		Totals (ton/yr) <sup>c</sup>	63.00	24.05	0.36	1.26	1.26	1.39					

			Emission Factor (lb/hp-hr)									
Unit	Unit ID		$NOx^{d}$	CO''	$SO_2^{(6)}$	PM''	$-PM_{19}^{-d}$	$VOM^{*}$				
Description		Prime Power	0.015	0.00815	**	0.0005	0.0005	0.00033				
		(hp)		Emissions (lb/hr)								
Air Compressor	AC-1	100	1.50	0.82	0.02	0.05	0.05	0.03				
		lotals (lb/hr)	1.50	0.82	0.02	0.05	0.05	0.03				
		Totals (ton/yr) <sup>c</sup>	3.15	1.71	0.04	0.11	0.11	0.07				

## MAXIMUM EMISSION CALCULATIONS DIESEL GENERATORS

				E	mission Fac	tor (lb/hp-hi	)	
Unit	Unit ID		$NOx^{d}$	CO''	$SO_2^{(6)}$	$PM^{u}$	$-PM_{19}^{-d}$	VOM''
Description		Prime Power	0.015	0.00903	si; 55	0.001	0.001	0.00033
		(hp)			Emission	is (lb/hr)		
Light Standard	1.5-1	15	0.23	0.14	0.01	0.02	0.02	0.005
Light Standard	1.5-2	15	0.23	0.14	0.01	0.02	0.02	0.005
Light Standard	1.5-3	15	0.23	0.14	0.01	0.02	0.02	0.005
Light Standard	1.5-4	15	0.23	0.14	0.01	0.02	0.02	0.005
Light Standard	L5-5	15	0.23	0.14	0.01	0.02	0.02	0.005
		lotals (lb/hr)	1.13	0.68	0.05	0.08	0.08	0.02
		Totals (ton/yr) `	2.36	1.42	0.11	0.16	0.16	0.05

			Emission Factor (lb/hp-hr)									
Unit	Unit ID		$NOx^{d}$	CO"	$SO_2^{(6)}$	PM''	$-PM_{(0)}^{-d}$	VOM''				
Description	Gant II)	Prime Power	0.015	0.01079	**	0.0013	0.0013	0.00033				
		(hp)	Emissions (lb/ur)									
Diesel Water Pump	DWP 1	20	0,30	0.22	0.01	0.03	0.03	0.01				
		Totals (lb/hr)	0.30	0.22	0.01	0.03	0.03	0.01				
		Totals (ton/yr) <sup>c</sup>	0.08	0.05	0.003	0.01	0.01	0.002				
	Facility En	nissions (ton/yr)	79.74	33.30	0.65	1.90	1.90	1.75				

Maximum Emissions Assumptions:

<sup>a</sup> Calculated using NSPS emission factors for stationary combustion sources (40 CER Part 89, Section 112). VOM emission factor from Permit #07050082 issued on May 21, 2009.

E Calculated using low sulfur diesel fuel and formula used in Permit #07050082 issued on May 21, 2009 with revised diesel fuel consumption data as follows:

500 HP Engine	20 gal/hr
100 & 118 HP Engines	10 gal/hr
15 & 20 HP Engines	5 gal/hr
* Hours of operation	4,200 hr/yr
	500 hr/yr

 $^3$  It is assumed that  $PM_{\rm cl}$  emissions are equal to  $PM_{\rm cl}$ 

(For emergency diesel water pump only.)

### Example Calculation

500 HP Diesel Engine NO<sub>X</sub> Emissions

509 harseptaver  $\pm$  0.015 lb NO  $^{-}$  per barseptaver haur  $\pm$  4,296 hr yr  $^{-}$  2,909 lb ton - 15.75 ton yr NO  $^{-}$ 

Conversion of NSPS Emission Factors

 $NO_X = 9.2 \text{ g/kW-hr}$  or 6.9 g/HP-hr

 $6.9~g/\,\mathrm{HP}$  hr /454 g per pound - 0.015 lb/hp hr

# FESOP REQUESTED LIMITATION AND FEE ALLOWABLE EMISSIONS SUMMARY

			Emission	s (ton/yr)		
Emission Point	NOx	со	<b>SO</b> 2	PM	$PM_{30}$	VOM
Process				104.14	49.22	
Generator	79.74	33.30	0.65	1.90	1.90	1.75
Total	79.74	33.30	0.65	106.04	51.12	1.75

Based on limiting operations to 4,200 hours per year.

### TYPICAL PROCESS UNITS EMISSION CALCULATIONS.

DESCRIPTION		M MAITRIAI ING RAIE <sup>T</sup>	РАКТІС МИГТІ		FMIS	SION FACT	ORS <sup>4</sup>	CONTROL		PM FMISS	ION RAIF	PM <sub>19</sub> EMISSION RATE	
	ton/la	ton/yr	PM	$PM_{16}$	PM	PM 16	UNITS	TYPE	EFFIC.	lb/day	ton∕yr	lb/day	ton/y <del>r</del>
Coal/P	etcoke Unloading Emis	sions											
BL=1 to C (1.6) (Coal/Petroke)	266	829,920	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	1.02	0.13	0.48	0.06
RU/TU-1 to C-(1-6) (Coal/Petcoke)	266	829,920	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	1.02	0.13	0.48	0.06
RU/TU-1_to C-(1-6) (Coal/Petcoke)	266	829,920	0.740	0.350	0.00064	0.00030	lbs/ton	Baghouse	90.0%	0.20	0.03	0.10	0.01
RU 2 to C 2 (Coal/Petroke)	2,000	6,240,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	7.64	0.99	3.61	0.47
RU 3 to C 8 (Coal/Petroke)	2,000	6,240,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	2.64	0.99	3.61	0.42
						En	dissions From	n Coal/Petcoke Unloadii	ng : Total>>	17.5	2.3	8.3	1.1
Coal/Petcoke	Conveyor Fransfer Poi: T								1	1			
C-L to C-2	2,500	7,800,000	0.240	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	9.55	1'4	4.52	(159
C 2 to 9 1	-4,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	15.28	0.32	7.23	0.15
C-3 to C-2	4,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	1.5.28	0.32	2.23	0.1.5
C.6. to 9.3	2,500	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	9.55	0.32	4.52	0.15
C-L to C-4	2,500	2,000,000	0.740	0.3.50	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	9.ob	0.39	4.52	0.1.5
C 4 to C 5	2,500	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0∜	9.55	0.32	-4.52	0.15
C-5 to S-2	2,500	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	9.55	0.39	4.52	0.15
RC L to C 3	3,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0∜	11.46	0.32	5.42	0.15
RC-2 to C-3	3,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	11.46	0.39	5.4?	0.1.5
RC 3 to C 3	3,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0℃	11.46	0.32	5.42	0.15
RC-4 to C-3	3,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	11.46	0.39	5.42	0.15
C Z ta C 9	2,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0℃	7.64	0.32	3.61	0.15
C-8 to C-10	2,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	7.64	0.39	3.61	0.15
C 9 to C 11	2,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0∜	7.64	0.32	3.61	0.15
C-10 to C-11	2,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	7.64	0.39	3.61	0.15
C 11 to 112 1	2,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	7.64	0.32	3.61	0.15
TP-1 to C-12	2,000	2,000,000	0.240	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	2.64	0.39	3.61	0.1.5
C 12 to SETP 1	2,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0∜	7.64	0.32	3.61	0.15
SFTP-1 to S-4	2,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	2.64	0.39	3.61	0.1.5

CORVICIALIZED CHANTABER R

### TYPICAL PROCESS UNITS EMISSION CALCULATIONS.

DESCRIPTION	MAXIMUM MAITRIA) HANDLING RAIT <sup>1</sup>		PARTICLESTZE MULTIPLER <sup>2</sup>		FMISSION FACTORS <sup>4</sup>			CONIROI		PM EMISSION RATE		PM <sub>19</sub> EMISSION RATE	
	ton/hr	(on/yr	PM	$PM_{P_{1}}$	PM	$PM_{P_{1}}$	UNITS	TYPE	EFTIC.	lb/day	ton∕yr	lb/day	ton/y <del>r</del>
DSH 1 to C 3	2,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0 <i>%</i>	7.64	0.32	3.61	0.15
RC-5 to C-3	2,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	7.64	0.32	3.61	0.1.5
RC 6 to C 3	1,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0 <i>%</i>	3.82	0.32	1.81	0.15
RC-7 to C-3	1,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	3.82	0.32	1.81	0.1.5
	Emissions From Coal/Petcoke Transfer Points: Total>> 2								208.2	8.2	98.5	3.0	
Coal/Petcol	ke Portable Conveyor.	Emissions											<del></del>
PC-L Drap Paint	2,500	3,900,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	9.55	0.62	4.52	0.29
PC-2 Drop Point	2,500	3,900,000	0.240	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	9.55	0.62	4.5?	(),29
PC 3 Drap Paint	2,500	3,900,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	<i>5</i> 0.0 <i>™</i>	9.55	0.62	4.52	0.29
PC-4 Drop Point	2,500	3,900,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	9 <del></del>	0.62	4.5?	0.29
PC 5 Drap Paint	2,500	3,900,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0 <i>%</i>	9.55	0.62	4.52	0.29
PC-6 Drop Point	2,500	3,900,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	9.55	0.62	4.52	0.29
PC 7 Drap Paint	2,500	3,900,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0 <i>%</i>	9.55	0.62	4.52	0.29
PC-8 Drop Point	2,500	3,900,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0 <i>%</i>	9.55	0.62	4.52	0.29
PC-9 Drop Point	2,500	3,900,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	9.55	0.62	4.52	0.29
PC 10 Drop Point	2,500	3,900,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	9əb	0.62	4.5?	0.29
PC 11 Drap Point	2,500	3,900,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	9.55	0.62	4.52	0.29
PC-12 Drop Point	2,500	3,900,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	9.ob	0.62	4.52	0.29
PEH 1 to PC (1.12)	2,500	3,900,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	9.55	0.62	4.52	0.29
PF-1 to PC-(1-12)	2,500	3,900,000	0.240	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	9 <del>5</del>	0.62	4.5?	0.29
RPCS I to PC (L12)	2,500	3,900,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0 <i>™</i>	9.55	0.62	4.52	0.29
	1	1	1	En.	i lissions Fron	n Coal/Petri	ske Portable	Conveyor Fransfer Poin	ts: Total>>	743.2	9.3	67.7	4.4

KM00000447

### TYPICAL PROCESS UNITS EMISSION CALCULATIONS.

DESCRIPTION	MAXIMU HANDI.	PARTICLE SIZE MULTIPLIER <sup>2</sup>		FMISSION FACTORS <sup>4</sup>			CONIROI		PM FMISSION RATE		PM <sub>19</sub> EMISSION RATE		
	ton/la	ton/yr	PM	$-PM_{P_{0}}$	PM	$PM_{P_{0}}$	UNITS	TYPE	EFTIC.	lb/day	ton/yr	lb/day	ton/yr
Coul	Petcoke Stacker Emiss	lons				, ,							
S 1 to CEP 5	4,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0∜	15.28	0.32	7.23	0.15
S-1 CLP-4	4,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	1.5.28	0.39	7.23	0.1.5
5-2-to CEP 2	2,500	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0∜	9.55	0.32	4.52	0.15
8-2 to CLP-3	2,500	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	9.ob	0.39	4.52	0.1.5
5-3 to CEP 1	2,500	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0∜	9.55	0.32	4.52	0.15
S-3 to CLP-4	2,500	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	. <del>5</del> 0.0%	9.55	0.32	4.52	0.1.5
5-1 to CEP 6	2,500	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0∜	9.55	0.32	4.52	0.15
S-1 to CLP-7	2,500	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	. <del>5</del> 0.0%	9.55	0.32	4.52	0.1.5
5-1 to CLP 8	2,500	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0∜	9.55	0.32	4.52	0.15
5-1 to CLP-9	2,500	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	. <del>5</del> 0.0%	9.55	0.32	4.52	0.1.5
5-1 to CEP-10	2,500	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0∜	9.55	0.32	4.52	0.15
S-1 to CLP-11	2,500	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	. <del>5</del> 0.0%	9.55	0.32	4.52	0.1.5
5-1 to CEP-12	2,500	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0∜	9.55	0.32	4.52	0.15
S-1 to CLP-13	2,500	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	. <del>5</del> ().()%	9.55	0.39	4.52	0.15
5-1 to CEP-14	2,500	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0∜	9.55	0.32	4.52	0.15
S-1 to CLP-15	2,500	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	9.55	0.39	4.52	0.15
S 4 to CEP 1	2,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0∜	7.64	0.32	3.61	0.15
S-4 to CEP-2	2,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	. <del>5</del> ().()%	7.64	0.32	3.61	0.15
5.4 to CLP 3	2,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0%	7.61	0.32	3.61	0.15
5-4 to CEP-4	2,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	. <del>5</del> ().()%	7.64	0.39	3.61	0.1.5
5.4 to CFP 5	2,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0∜	7.64	0.32	3.61	0.15
S-4 to CEP-6	2,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	. <del>5</del> ().()%	7.64	0.39	3.61	0.1.5
s 4 to CFP Z	2,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0∜	7.64	0.32	3.61	0.15
s-4 to DSH-1	2,000	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	7.64	0.39	3.61	0.1.5
	1	•				•	Emissions I	rom Coal/Petcoke Stack	er: Total>>	225.3	7.6	106.6	3.6

CIRA CARAGO CILA TANGGER

#### TYPICAL PROCESS UNITS EMISSION CALCULATIONS.

DISCRIPTION	MAXIMU HANDI		PARTICLE SIZE MULTIPLIER <sup>2</sup>		SION FACT	ORS <sup>4</sup>	CONIROI		PM EMISSION RATE		PM <sub>19</sub> EMISSION RATE		
	ton/la	to <b>n/</b> yr	PM	$PM_{16}$	PM	$-PM_{P_{0}}$	UNITS	TYPE	ETTC.	lb/day	ton∕yr	lb/day	ton/y <del>r</del>
Coal/Petcoke	Loadout Emissions	Emissions											
Coal Loadout to S 1	-1,000	1,300,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0 %	15.28	0.21	7.23	0.10
Coal/Pet Coke Loadout to TL-2	550	200,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	50.0∜	2.10	0.03	0.99	0.02
Pet Coke Loadout to S-t	4,000	1,300,000	0.740	0.350	0.00064	0.00030	lbs/ton	Water Suppression	.50.0%	15.28	0.21	7.23	0.10
	Emissions From Coul/Petcoke Eoadout: Total>>										0.4	15.4	0.2
								Coul/Petcoke Emission	us: Total>>	626.9	27.9	296.5	13.2
Salt	Handling Emission	5	_	_	_	-							_
BL_1 to SP-1 (Salt)	3,500	125,000	0.740	0.350	0.00064	0.00030	lbs/ton	None	0.0%	26.74	0.06	12.65	0.03
16 Various Transfer Points	2,500	2,000,000	0.740	0.350	0.00064	0.00030	lbs/ton	None	0.0%	19.10	0.64	9.03	0.30
							Emi	ssions From Salt Handlii	ig: Total>>	45.8	0.7	21.7	0.3
Soil Crusi	hing/Screening Emi	ssions											
RPCF-1 (Crushing)	140	218,400			0.0033	0.00101	lbs/ton	Water Suppression	.50.0%	2.77	0.18	0.85	0.06
RPCE 1 (Screening)	140	218,400			0.00067	0.00034	lbs/ton	Water Suppression	50.0 <i>™</i>	0.56	0.04	0.29	0.02
						Ē	nissions Fro	m Soil Crushing/Screenii	ig: Total>>	3.3	0.2	1.1	0.1
								Laci	lity Total>>	676.1	28.8	319.3	13.6

1. The hourly rate is based on 3,120 hours/year of operation.

2. Aerodynamic Particulate Size Multiplier (k) per AP-42 Section 13.2.4.3, Aggregate Handling and Storage Piles, 11/06

3. Emission factor for material handling emissions calculated per Equation 1 of AP 42 Section 13.2.4.3,

Aggregate Handling and Storage Piles.

4. http://www.ncdc.noaa.gov/oa/climate/online/ccd/avgwind.html

The coal and petcoke that are received at the facility have numerous ways of being conveyed through the facility. To be conservartive in calculating the emissions, the portable conveyors were chosen as the main method of moving the materials from the receiving areas.

Facility has a water suppression system to control particulate matter emissions.

Coal and pet coke received at the Facility have an average moisture content of 18.3% and 10.0% respectively. Emissions were calculated based on 100% throughput of pet coke as a worst-case scenario.

### Assumptions:

### BACKGROUND DATA

Coal/Pet Coke moisture content (weighted average) : 10.0%

Operating Schedule = 12 hours/day

 $Operating Schedule + \left\lceil 260 | days / year \right\rceil$ 

- $Operating Schedule = (3.120 \ hours/year)$
- Mean wind speed<sup>4</sup> 10.3 mph

### TYPICAL FUGITIVE EMISSIONS CALCULATIONS

DESCRIPTION		M M VIERIAL ING RAFI <sup>T</sup>	PARTIC AMD 17	TT STZE PUTER <sup>2</sup>	FAUS	STON FAC	(ORS	COATE	ю	PMTAIRS	SON RAIT	PM <sub>10</sub> FMIS	SSION RAIT
	ton/lir	ton/yr	PM	$-PM_{00}$	PM	$PM_{25}$	UNTIS	ויזייו	- FFFRC.	lb/day	ton/yr	lb/day	ton/yr
Storage Pile I CLP 17	smissions N/A	N/A	1.000	0.500	4947.5	2473.8	'bs/acre	Water Suppression	75.0%	35.35	34.74	n7.77	12.37
anga	N/A	N/A	1.000	0.500	4947.5	2473.8	.bs/acre	Water Suppression	75.0%	176.55	24.54	87.77	12.37
curs?	N/A	N/A	1.000	0.500	49477.6	2473.8	.bs/acro	Water Suppression	75.0%	175.55	24.74	67.77	12.37
CLP 4 <sup>2</sup>	X/A	NYA	1.000	0.500	49 <b>47</b> .5	2473.8	"bs/acre	Water Suppression	75.0%	35.35	34.74	87.77	12.37
CIUP 5 1	N/A	NZA	1.000	0.500	4947.5	2473.8	'bs/acre	Water Suppression	75.0%	35.55	34.74	<del>57.77</del>	12.37
CLP-s 1	N/A	N/A	1.330	0.500	4947.5	2473.8	.bs/acre	Water Suppression	75.0%	176.55	21.74	87.77	12.37
CH 1947 <sup>9</sup>	N/A	N/A	1.000	0.500	49472.6	2473.8	.bs/acro	Water Suppression	75.0%	176.55	24.54	67.77	12.37
C117.8 <sup>2</sup>	N/A	NZA	1.000	0.500	4947.5	2473.8	'bs/acre	Water Suppression	75.0%	35.35	34.74	57.77	12.37
CU15 A.	N/A	NYA	1.000	0.500	4947.5	2473.8	'bs/acre	Water Suppression	75.0%	35.35	34.74	57.77	12.37
CEP-101	N/A	N/A	1.000	0.500	4947.6	2473.8	.bs/acre	Water Suppression	75.0%	176.55	24.54	87.77	12.37
CEP-11.2	N/A	N/A	1.000	0.500	4947.6	2479.8	lbs/acro	Waler Suppression	75.0%	175.55	24.74	87.77	12.37
CLP 12 <sup>2</sup>	N/A	NYA	1.000	0.500	4947.5	2473.8	'bs/acre	Walter Suppression	75.0%	35.35	34.74	57.77	12.37
CI 121 131	N/A	N/A	1.000	0.500	4947.5	2473.8	'bs/acre	Water Suppression	75.0%	35.35	34.74	57.77	12.37
ch pula r	N/A	N/A	1.330	0.500	4947.6	2473.8	.bs/acro	Water Suppression	75.0%	176.55	24.74	87.77	12.37
CLD-15 <sup>9</sup>	N/A	N/A	1.000	0.500	4947.6	2473.8	.bs/acro	Water Suppression	75.0%	176.55	24.74	87.77	12.37
CIPP-I	N/A	N/ A	1.000	0.500	4947.8	2473.8	'bs/acre	Water Suppression	75.0%	35.35	34,74	57.77	12.37
CIPD-2	N/A	NZA	1.000	0.500	4947.5	2473.8	"bs/acre	Water Suppression	75.0%	35.55	34.74	87.77	12.37
CHP 3	N/A	N/A	1.000	0.500	49477.8	2473.8	lbs/acro	Water Suppression	75.0%	175.55	24.74	67.77	12.37
CEPH	N/A	N/A	1.000	0.500	4947.5	2473.8	.bs/acro	Water Suppression	75.0%	175.55	24.74	67.77	12.37
CIPD-5	N/A	NZA	1.000	0.500	1947. <del>5</del>	2473.8	"bs/acre	Water Suppression	75.0%	35.55	34,74	n7.77	12.37
CIED-5	N/A	N/A	1.000	0.500	-947. <del>5</del>	2473.8	"bs/acre	Water Suppression	75.0%	35.35	34.74	87.77	12.37
CHP 7	N/A	N/A	1.000	0.500	4947.5	2473.8	lbs/acre	Water Suppression	75.0%	175.55	24.74	67.77	12.37
sp_ /	N/A	N/A	1.000	0.500	4947.5	2473.8	.bs/acro	Walter Suppression	75.0%	33,89	o.18	18.94	3,39
							Store	age Pile Emission	us: Total>>	3076.0	550.4	1508.0	275.2

DESCRIPTION		M M WERTAL 'ING RATE		VESIZI PLIER <sup>2</sup>	I'MI:	SION LAC	ORS	CONTROL		PM IMISSION RATE.		PM 10 FMISSION R.	
	tons/lir	tons/year	PAL	PM <sub>10</sub>	PM	$PM_{10}$	UNITS	TYPI.	EFTIC.	1b/day	tpy	PM - a FMHS8 Ib/day 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.42 5.	tpy
Reclaim Belt Loadi	ng Emissions										1.2		1.7
RC 1. Loaded by Dozer/Tind Loader <sup>4</sup>	3,000	500,000	0.740	0.350	0.00064	0.00070	les/ten	Water Suppression	50.0%	11.4o	0.08	5.43	0.0 <del>2</del>
RC 2. Loaded by Dozer/Fiel Toader <sup>4</sup>	3,000	500,000	0.740	0.350	0.00064	0.00070	lbs/ten	Water Suppression	50.0%	11.4o	0.08	5.40	0.04
RC-3. Leaded by Dozer/Find Loader <sup>4</sup>	3,000	500,000	0.740	0.350	0.00064	0.00090	lles/ton	Water Suppression	50.0%	112lø	0.08	o.42	
RC-4. Leaded by Dozen/sind Loader <sup>4</sup>	3,000	500,000	0.740	0.350	0.00064	0.00090	lbs/ton	Water Suppression	50.0%	112lø	0.08	p.42	
Front line Loader <sup>®</sup> Roadway Emissions	NZA	N/A	4.900	.500	ð.5	2.2	"bs/AN""	Water Suppression	75.0%	37.32	n.55	32.85	4.27
Front line Loader <sup>9</sup> Roadway Emissions	NZA	N/A	4,900	.500	ð.5	2.2	"bs/AN""	Water Superession	75.0%	37.32	n.55	32.85	≐.27
RCB Loaded by Dozer <sup>4</sup>	2,000	500,000	0.740	0.350	0.00064	0.00030	lfrs/ton	Water Suppression	50.0%	2.64	0.08	3.61	
RC-n Toaded by Dezer	1.000	500,000	0.740	0.350	0.00064	0.00030	lfes/ten	Water Suppression	50.0%	3.82	0.08	1.81	
RC-7 Toaded by Dozer <sup>1</sup>	1,000	500,000	0.740	0.350	0.00064	0.00070	lbs/ten	Water Suppression	50.0%	3.82	0.08	.ö	002
			•		•	Re	claim Belt t	oading Unission	is: 'Total>>	315.8	33.7	94.6	8.5
Truck Loading 1	Emissions												
Salt Toordoo By Find Toordon <sup>4</sup>	550	1,716,300	0.240	0.350	0.00064	0.00030	lles/ten	Nene	(),()%;	4.20	0.55	1.99	0.26
Coal Toacted by First Loader <sup>4</sup>	475	1,482,000	0.740	0.350	0.00064	0.00030	lfrs/ten	Water Suppression	50.0%	.ö	0.24	Ú.áo	0.1
		•	•	•			Fruck t	oading l'mission	is: '1 otal>>	6.0	0.8	2.8	0.4
Roadway En	lissions												
Inbound Coal Truck Traffic (	N/A	N/A	4.900	1.500	0.5	1.7	.bs/AAL	Lugitva Dust Management Plan	75.0%	72.51	9,43	18.21	2,43
Outbound Coal Truck Tractic	N/A	N/A	4.900	1.500	0.5	1.7	.bs/AXL	Tugitva Dust Managament Plan	75.0%	72.51	9,43	18.21	2,43
Outbound Satt Fruck Traffic 1	N/A	N/A	4.900	1.500	0.5	1.2	.bs/AXL	Tugitva Dust Management Plan	75.0%	cl- <i>Ca</i>	8.25	18.37	2.13
		·		·	·		Ri	adway Emission	is: Total>>	208.5	.27.1	53.8	7.0
								I aci.	lity I otal>>	3546.2	612.0	1659.2	291.4

. The hourly rate is based on 3, 20 hours/year of operation.

2. Aerodynamic Jasticulate Size Multiplies (k) per AP 42 Section 13.27LX Aggregate Handling and Storage Files, 11/06

3. Moan Wind Spood (c) (estimate).

- 4. Emission factor for material handling emissions calculated per Equation 1 of AP-42 Section (2.2.4.3).
- Aggregate mandling and Storage Piles.

b. Immission factor for unnaved road emissions calculated per houation A.742 Section 13.2.2. Unpaved Roads.

b. From National Weather Service (estimate).

7. From Air Pellutier Ungineering Manual and References Sectors 9.3. (http://www.wrapain.org/forums/dejt/fulh/content/Ch98Sterage\_Pile\_Wind920Flesien\_Rev0o.pdf)

TSP (lb/ycan/actea surface) = 1.7(s/1.5)(365[365-p]/235)(1/15)

Coal and peticoke received at the facility have an average morsture content of 18.5% and 10.0% respectively. Emissions were calculated based on 10.0% throughput of peticoke as a worst-case science.

#### Assumptions:

COAL BACKGROUND DATA Coal/Pet Coke moisture contact (weighted average) = 0.0% Silt center: et ceal = 15.0% IND LOADER/DOZER OPERATIONS eront line Loaders/Dozer (Storage Files) = 12 hours/day Front Find Toaders/Dezer (Recibirn) = 12 hours/day Operating Schedule = 1.2 hours/day Operating Schedule = 1260 days/year Operating Schedule = 13/120 hours/year Front Find Leader/Dezenspeed = 15.0 mph. VML of eront and Loader/ Dozer (Storage Piles) = 100.0 miles/day AMT of Front Ind Loader/Dozer (Reclam) = 100.0 miles/day Tront and Loader/Dozer Average Weight (Cat 980) = 139 tons STORAGE PILE INFORMATION Surface area of sterage piles (Coal) = -40.0 acres Surface area of storage piles (Coke) = -40.0 acres Surface area of storage piles (Salt) = 10.0 acres Davis mistorage prie = 1365 davis. Number of days' with rain > 0.01 inch = --7 days Near wind speed<sup>3</sup> = 10.3 mp.a. . Forcent of time' winds > 12 mph = 34.0%

#### INBOUND COAF-FRUCK BACKGROUND DATA

Delivery truck tare weight= 15 lons. Waximum full truck weight= 29 tons. Average truck weight= 22 tors Maximum facility input= 2,000,000 ton/year Maximum truck/badeut= (200,000 ten/year Number of coal trucks= 14,265 trucks/year Miles per trip= 0.8 miles Miles per day= 44.0 miles/ day Alles pervear= 1,429 miles/year OUTBOUND COAL TRUCK BACKGROUND DATA Delivery truck tare weight= 1p tors. Maximum full truck weight= 29 tors Average truck weight- 22 tens. Maximum facility output= 2,000,000 tons/year Maximum truck dolivory= 200.000 tons/year Number of coal trucks+ 14,286 trucks/year Miles per trip= 0.8 miles. Viles per day = 44.0 miles/day Miles per year= 11.429 miles/year SAFE HAULING FRUCK BACKGROUND DATA Delivery truck tare weight= 15 tors. Maximum full truck weight= 29 toos. Average truck weight= 22 tons. Maximum facility output= 195,000 ton/yr Maximum truck loading= - 75,000 ten/vir Number of coal trucks= 12,500 trucks/year Miles per trip= 0.8 miles Milles per day= 38.0 miles/day Allies perivear= 10,000 miles/year

			DILJEL GI	MERATOR	3			
				L	mission Fac	tor (Ib/hp-h	r)	
Unit	Unit ID		$NOx^{d}$	CO <sup>3</sup>	$SO_2^{-h}$	PM "	$PM_{19}^{d}$	VOM*
Description	unii 1D	Prime Power	0.015	0.00815	**	0.0005	0.0005	0.00033
		<i>(hp)</i>		•	Emission	is (lb/hr)	•	•
Diesel Generator 1	DG-1	118	1.77	0.96	0.021	0.06	0.06	0.04
Diesel Generator 2	DG 2	118	1.77	0.96	0.021	0.06	0.06	0.04
Diesel Generator 3	DG-3	118	1.77	0.96	0.021	0.06	0.06	0.04
		Totals (Ib/ hr)	5.31	2.89	0.06	0.18	0.18	0.12
		Totals (ton/yr) $^\circ$	8.28	4.50	0.10	0.28	0.28	0.18

#### TYPICAL EMISSION CALCULATIONS DIESEL GENERATORS

				E	mission Fac	tor (Ib/hp-h	r)	
Unit	Unit ID		$NOx^{d}$	$CO^{(\ell)}$	$SO_2^{(b)}$	$PM^{d}$	$-PM_{(19)}^{-d}$	VOM"
Description	unn 1D	Prime Power	0.015	0.00573	X-3-	0.0003	0.0003	0.00033
		(hp)			Emission	ts (lb/hr)		
Diesel Generator 4	DG 4	500	7.50	2.86	0.043	0.15	0.15	0.17
Diesel Generator 5	DG-5	500	7.50	2.86	0.043	0.15	0.15	0.17
Diesel Generator 6	DG-6	500	7.50	2.86	0.043	0.15	0.15	0.17
Diesel Generator 7	DG 7	500	7.50	2.86	0.043	0.15	0.15	0.17
		Totals (lb/hr)	30.00	11.45	0.17	0.60	0.60	0.66
		Totals (ton/yr) <sup>c</sup>	46.80	17.87	0.27	0.94	0.94	1.03

				E	mission Fac	tor (Ib/hp-h	r)	
Unit	Unit ID		$NOx^{d}$	CO "	$SO_2^{-h}$	PM''	$-PM_{19}^{d}$	VOM *
Description	umuno	Prime Power	0.015	0.00815	**	0.0005	0.0005	0.00033
		(hp)			Emission	is (lb/hr)		
Air Compressor	AC 1	100	1.50	0.82	0.02	0.05	0.05	0.03
		-Totals (lb/hr)	1.50	0.82	0.02	0.05	0.05	0.03
		Totals (ton/yr) <sup>c</sup>	2.34	1.27	0.03	0.08	0.08	0.05

				E	mission Fac	tor (Ib/hp-h	r)	
Unit	Unit ID		$NOx^{d}$	CO "	$SO_2^{-b}$	PM "	$PM_{19}^{d}$	VOM*
Description	umin	Prime Power	0.015	0.00903	***	0.001	0.001	0.00033
		<i>(hp)</i>			Emission	is (lb/hr)		
Light Standard	I.S 1	15	0.23	0.14	0.01	0.02	0.02	0.005
Light Standard	I.S 2	15	0.23	0.14	0.01	0.02	0.02	0.005
Light Standard	LS-3	15	0.23	0.14	0.01	0.02	0.02	0.005
Light Standard	LS-1	15	0.23	0.14	0.01	0.02	0.02	0.005
Light Standard	LS 5	15	0.23	0.14	0.01	0.02	0.02	0.005
		Totals (lb/hr)	1.13	0.68	0.05	0.08	0.08	0.02
		Totals (ton/yr) <sup>c</sup>	1.76	1.06	0.08	0.12	0.12	0.04

#### TYPICAL EMISSION CALCULATIONS DIESEL GENERATORS

				E	mission Fac	tor (Ib/hp-hi	<i>'</i> )	
Unit	Unit ID		$NOx^{d}$	CO "	$SO_2^{-h}$	$PM^{*}$	$PM_{19}^{d}$	VOM "
Description	unun	Prime Power	0.015	0.01079	373F	0.0013	0.0013	0.00033
		(hp)			Emission	is (lb/hr)		
Diesel Water Pump	DWP 1	20	0.30	0.22	0.01	0.03	0.03	0.01
		- Totals (Ib/hr)	0.30	0.22	0.01	0.03	0.03	0.01
		Totals (ton/yr) <sup>c</sup>	0.04	0.03	0.001	0.003	0.003	0.001
	Facility En	uissions (ton/yr)	59.22	24.72	0.48	1.41	1.41	1.30

Maximum Emissions Assumptions:

Calculated using N515 emission factors for stationary combustion sources (40 CFR Part 89, Section 112). VOM emission \* factor from Permit #07050082 issued on May 21, 2009.

Calculated using low sulfur diesel fuel and formula used in Permit #07050082 issued on May 21, 2009 with revised diesel.
 <sup>b</sup> fuel consumption data as follows:

500 HP Engine	20 gal/hr
100 & 118 HP Engines	10 gal/hr
15 & 20 HP Engines	5 gal/hr
<sup>e</sup> Hours of operation	3,120 hr/yr
	250 hr/yr

(For emergency diesel water pump only.)

 $^{\rm d}$  It is assumed that  $\rm PM_{10}$  emissions are equal to PM.

Example Calculation

500 HP Diesel Engine NO<sub>X</sub>Emissions

500 horseptater x 6.015 lb NO  $_\odot$  per horseptater hour x 3,126 hr/gr / 2,650 lb/but = 11 / ton/gr NO  $_\odot$ 

 $\label{eq:conversion} \frac{Conversion of NSPS Emission Factors}{NO_x = 9.2~g/kW~hr~or~6.9~g/HP~hr}$  6.9~g/HP-hr/454~g~per~pound = 0.015~lb/hp-hr

CRA 052450 01A TABLE 11

#### TYPICAL EMISSIONS SUMMARY

			Emission	s (ton/yr)		
Emission Point	NOx	со	<b>SO</b> <sub>2</sub>	РМ	PM 10	VOM
Process				28.82	13.60	
Generator	59.22	24.72	0.48	1.41	1,41	1.30
Total	59.22	24,72	0.48	30,23	15.01	1.30

#### LISTING OF EMISSION UNITS

Process Equipment	Unit Designation	Submittal	Permit #
Unloading Operations			
Barge Unloader	BU-1	Existing	
Rail/Truck Unloader	RU/TU-1	Existing	
Rail Unloader 2	RU-2	Existing	7050082
Rail Unloader 3	RU-3	Existing	7050082
Conveyor Operations			
Conveyor 1	C-1	Existing	
Conveyor 2	C-2	Existing	
Conveyor 3	C-3	Existing	
Conveyor 4	C-1	Existing	
Conveyor 5	C-5	Existing	
Conveyor 6	C-6	Existing	
Conveyor 7	C-7	Existing	7050082
Conveyor 8	C-8	Existing	7050082
Conveyor 9	C-9	Existing	7050082
Conveyor 10	C-10	Existing	7050082
Conveyor 11	C-11	Existing	7050082
Conveyor 12	C-12	Existing	7050082
Reclaim Conveyor 1	RC-1	Existing	
Reclaim Conveyor 2	RC-2	Existing	
Reclaim Conveyor 3	RC-3	Existing	
Reclaim Conveyor 4	RC-1	Existing	
Reclaim Conveyor 5	RC-5	Existing	7050082
Reclaim Conveyor 6	RC-6	Existing	7050082
Reclaim Conveyor 7	RC-7	Existing	7050082
Portable Conveyor 1	PC-1	Existing	7050082
Portable Conveyor 2	PC-2	Existing	7050082
Portable Conveyor 3	PC-3	Existing	7050082
Portable Conveyor 4	PC-1	Existing	7050082
Portable Conveyor 5	PC-5	Existing	7050082
Portable Conveyor 6	PC-6	Existing	7050082
Portable Conveyor 7	PC-7	Existing	7050082
Portable Conveyor 8	PC-8	Existing	7050082
Portable Conveyor 9	PC-9	Proposed	
Portable Conveyor 10	PC-10	Proposed	
Portable Conveyor 11	PC-11	Proposed	
Portable Conveyor 12	PC-12	Proposed	
Transfer Hopper Operations	- <u>-</u>		
Direct Ship Hopper 1	DSH-1	Existing	7050082
Portable Feed Hopper	PFII-1	Existing	7050082
Portable Feeder	PF-1	Existing	7050082
Rental Portable Crusher/Screen	RPCS-1	Existing	7050082
Transfer Point 1	T P-1	Existing	7050082
Stacker Feed Transfer Point	SFIP-1	Existing	7050082

#### LISTING OF EMISSION UNITS

Process Equipment	Unit Designation	Submittal	Permit #
Stacker Operations			
Stacker 1/Barge & Rail Loadout	S-1	Existing	
Stacker 2	5-2	Existing	
Stacker 3	5-3	Existing	
Stacker 4	5-1	Existing	7050082
Storage Pile Operations			
Coal Pile 1	CLP-1	Existing	
Coal Pile 2	CLP 2	Existing	
Coal Pile 3	CLP 3	Existing	
Coal Pile I	CLP 4	Existing	
Coal Pile 5	CLP 5	Existing	
Coal Pile 6	CLP 6	Proposed	
Coal Pile 7	CLP 7	Proposed	
Coal Pile 8	CLP 8	Proposed	
Coal Pile 9	CLP 9	Proposed	
Coal Pile 10	CLP 10	Proposed	
Coal Pile 11	CLP 11	Proposed	
Coal Pile 12	CLP 12	Proposed	
Coal Pile 13	CLP 13	Proposed	
Coal Pile 14	CLP 14	Proposed	
Coal Pile 15	CLP 15	Proposed	
Salt Pile 1	SP-1	Existing	7050082
Coke Pile 1	CEP 1	Existing	7050082
Coke Pile 2	CEP 2	Existing	7050082
Coke Pile 3	CEP 3	Existing	7050082
Coke Pile 4	CEP 4	Proposed	
Coke Pile 5	CEP 5	Proposed	
Coke Pile 6	CEP 6	Proposed	
Coke Pile 7	CEP 7	Proposed	
<u>Diesel Generators</u>			
Diesel Generator - 118 HP (1)	DG-1	Existing	7050082
Diesel Generator - 118 HP (2)	DG-2	Existing	7050082
Diesel Generator - 118 HP (3)	DG-3	Existing	7050082
Diesel Generator - 500 HP (4)	DG-4	Existing	7050082
Diesel Generator - 500 HP (5)	DG-5	Existing	7050082
Diesel Generator - 500 HP (6)	DG-6	Existing	7050082
Diesel Generator - 500 HP (7)	DG-7	Existing	7050082
Air Compressor - 100 IIP	AC-1	Proposed	4
Light Standard - 15 HP	LS-1	Proposed	4
Light Standard - 15 HP	LS-2	Proposed	4
Light Standard - 15 HP	LS-3	Proposed	
Light Standard - 15 HP	LS-4	Proposed	_ <b>_</b>
Light Standard - 15 HP	LS-5	Proposed	
Diesel Water Pump - 20 HP	DWP-1	Existing	7050082

## Exhibit P



Hogan Lovells US LLP Columbia Square 555 Thirteenth Street, NW Washington, DC 20004 T +1 202 637 5600 F +1 202 637 5910 www.hoganlovells.com

January 31, 2014

#### By FedEx and Electronic Mail

Attn: Compliance Tracker, AE-17J Air Enforcement and Compliance Assurance Branch U.S. Environmental Protection Agency Region 5 77 W. Jackson Boulevard Chicago, IL 60604

Nicole Cantello Bonnie Bush U.S. Environmental Protection Agency 77 West Jackson Boulevard Chicago, Illinois 60647 Cantello.Nicole@epa.gov Bush.Bonnie@epa.gov

## Re: Koch Mineral Services – Response to EPA Information Request Dated December 30, 2013

Dear Ms. Cantello and Ms. Bush:

This letter and its attachments are hereby submitted as a response to the above-referenced December 30, 2013 request for information, issued by the United States Environmental Protection Agency ("EPA") to Koch Mineral Services, LLC pursuant to Section 114(a) of the Clean Air Act, 42 U.S.C. § 7414(a). We note that Koch Mineral Services, LLC is a holding company that does not itself conduct any activities relevant to this information request, and are instead offering this response on behalf of Koch Minerals, LLC (a direct subsidiary of Koch Mineral Services, LLC) and its affiliates KCBX Terminals Company and The C. Reiss Coal Company (collectively for purposes of responding to EPA's requests, "Koch Minerals").

In your electronic message of January 14, 2014, EPA agreed to certain modifications and clarifications of the original information request. Koch Minerals' understanding of the requests as modified is indicated with respect to each request below.

Koch Minerals has engaged in considerable effort to ensure that its submissions are complete, responsive, and useful to the Agency. Koch Minerals makes the following general qualifications and objections to EPA's request:

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- Koch Minerals objects to the request insofar as it seeks privileged information, including any and all communications and documents that are protected from disclosure by either the attorney-client communication privilege or attorney work-product doctrine.
- Koch Minerals objects to the request to the extent it improperly seeks information beyond the scope of EPA's authority under Section 114(a) of the Clean Air Act, 42 U.S.C. § 7414(a), and therefore is not a proper exercise of EPA's information-gathering authority.
- Koch Minerals objects to the request to the extent it is vague, ambiguous, overbroad, or unduly burdensome.
- Koch Minerals reserves the right to supplement and revise its response, and reserves the right to assert additional objections as it continues to evaluate its response.
- Koch Minerals requests confidential treatment for the documents and information designated as "confidential business information" ("CBI") to the extent information in the files and documents is designated confidential.

Accordingly, notwithstanding the foregoing, and without waiving any of the foregoing qualifications and objections, below Koch Minerals has included the relevant numbered request followed by Koch Minerals' response.<sup>1</sup> The numbers of the responses below correspond to the numbers of the specific request included in Appendix B of the December 30, 2013 request.

#### Request No. 1:

Provide a list of all locations in Region 5 that Koch owned or operated for storage of petroleum coke from 2004 through the present. For each location, identify the following:

- a. The owner or operator of the petroleum coke storage or handling during the entire period you owned or handled petroleum coke at that site;
- b. The dates Koch first and last stored or handled petroleum coke at the site and all intervening dates when shipments were accepted at the site and when shipments were transported off the site;
- c. The dates and amounts (in tons) of each shipment from 2009 to the present; and
- d. Detailed descriptions of any measures taken to prevent fugitive emissions from each pile.

#### Response to Request No. 1:

As reflected in EPA's January 14th electronic message, Koch Minerals understands this Request to require it to identify, as to sites that Koch Minerals owned or operated in Region 5:

a. The owner(s) or operator(s) of such sites at which Koch Minerals staged or handled petroleum coke since January 1, 2004;

<sup>&</sup>lt;sup>1</sup> For all attached electronic files, KCBX has scanned the files for viruses using Symantec Endpoint Protection in accordance with the instructions in Appendix A of the information request.

- b. For the sites identified in (a) above, the first and last date petroleum coke was staged or handled there;
- c. For the sites identified in (a) above for the period 2009 to the present, the monthly throughput expressed in tons of petroleum coke; and
- d. For the sites identified in (a) above, descriptions of the measures taken to prevent fugitive emissions from piles.

Koch Minerals notes that subsection (a) appears to inadvertently omit the word "site" from "the owner or operator of the petroleum coke storage or handling [site] during the entire period you owned or handled petroleum coke at that site," and interprets that portion of the request accordingly.

Koch Minerals objects to this Request to the extent it implies that Koch Minerals "stores" or accepts for "storage" any petroleum coke. For purposes of identifying responsive information, Koch Minerals interprets these terms to refer to staging, rather than storage, of petroleum coke.

Koch Minerals owned or operated the following sites within Region 5 from January 1, 2004 until the present where petroleum coke was staged or handled.

- 1. KCBX North (3259 E. 100<sup>th</sup> St., Chicago, Illinois) Owned and operated by KCBX Terminals Company. Koch Minerals presently stages and handles petroleum coke at this facility. Upon information and belief, Koch Minerals has staged and handled petroleum coke at this site since January 1, 2004. Therefore, for purposes of this request, the date petroleum coke was first staged or handled at this facility is January 1, 2004. Further, please note that Koch Minerals purchased and began to operate the facility in 1990. Koch Minerals would have staged and handled petroleum coke at this facility from time to time between the date of purchase and December 31, 2003. However, Koch Minerals is unable to identify with precision or certainty when it might have received the first shipment of petroleum coke at the facility because Koch Minerals, in accordance with its record retention policy, has not retained the records sufficient to definitively state an exact date. Total monthly throughput of petroleum coke from January 2009 through December 2013 is set forth in the spreadsheet designated "KM00000001\_Native\_Format" (with a duplicate provided in bates-numbered pdf format), attached hereto on Disc 1 in an electronic file folder labeled Response #1c. A detailed description of the measures taken to prevent fugitive emissions from piles at the site is contained in a document designated "KM00000017," attached hereto on Disc 1 in an electronic file folder labeled Response #1d.
- KCBX South (10730 S. Burley Ave., Chicago, Illinois) Owned by KM Railways, LLC and operated by KCBX Terminals Company. Koch Minerals presently stages and handles petroleum coke at this facility. Koch Minerals acquired the facility on December 20, 2012. It has staged and handled petroleum coke at the facility from that date. The first shipment of petroleum coke from this facility was on or about December 21, 2012. Total monthly throughput of petroleum coke from December 2012 through December 2013 is

set forth in the spreadsheet designated "KM00000001\_Native\_Format" (with a duplicate provided in bates-numbered pdf format), attached hereto on Disc 1 in an electronic file folder labeled Response #1c. A detailed description of the measures taken to prevent fugitive emissions from piles at the site is contained in the document designated "KM00000031," attached hereto on Disc 1 in an electronic file folder labeled Response #1d.

- 3. Duluth (50th Avenue West & LeSure, Duluth, Minnesota) Owned and operated by The C. Reiss Coal Company. Koch Minerals presently stages and handles petroleum coke at this facility. Koch Minerals has staged and handled petroleum coke at this site since January 1, 2004. Therefore, for purposes of this request, the date petroleum coke was first staged or handled at this facility is January 1, 2004. Further, please note that Koch Minerals purchased and began to operate the facility in December 1986. Koch Minerals would have staged and handled petroleum coke at this facility from time to time between the date of purchase and December 31, 2003. However, Koch Minerals is unable to identify with precision or certainty when it might have received the first shipment because Koch Minerals, in accordance with its record retention policy, has not retained the records sufficient to definitively state an exact date. Total monthly throughput of petroleum coke from January 2009 through December 2013 is set forth in the spreadsheet designated "KM00000001 Native Format" (with a duplicate provided in bates-numbered pdf format), attached hereto on Disc 1 in an electronic file folder labeled Response #1c. A detailed description of the measures taken to prevent fugitive emissions from piles at the site is contained in the document designated "KM00000003," attached hereto on Disc 1 in an electronic file folder labeled Response #1d.
- 4. Green Bay (111 W. Mason St., Green Bay, Wisconsin) Owned and operated by The C. Reiss Coal Company. Koch Minerals presently stages and handles petroleum coke at this facility. Koch Minerals has staged and handled petroleum coke at this site since January 1, 2004. Therefore, for purposes of this request, the date petroleum coke was first staged or handled at this facility is January 1, 2004. Further, please note that Koch Minerals purchased and began to operate the facility in 1986. Koch Minerals would have staged and handled petroleum coke at this facility from time to time between the date of purchase and December 31, 2003. However, Koch Minerals is unable to identify with precision or certainty when it might have received the first shipment of petroleum coke at the facility because Koch Minerals, in accordance with its record retention policy, has not retained the records sufficient to definitively state an exact date. Total monthly throughput of petroleum coke from January 2009 through December 2013 is set forth in the spreadsheet designated "KM00000001\_Native\_Format" (with a duplicate provided in bates-numbered pdf format), attached hereto on Disc 1 in an electronic file folder labeled Response #1c. A detailed description of the measures taken to prevent fugitive emissions from piles at the site is contained in the document designated "KM00000008," attached hereto on Disc 1 in an electronic file folder labeled Response #1d.

Scott Lebbin (Vice-President of Operations – Koch Minerals, LLC), William Reiss (President – The C. Reiss Coal Company), Robert Valley (Dock Superintendent – The C. Reiss Coal Company), Richard Schlies (Manager of Transportation – Koch Minerals, LLC), Kathy Meese (Administrative Assistant – The C. Reiss Coal Company), Roberta Peterson (Administrative Clerk – KCBX Terminals Company), Christian Zuidmulder (Operations Supervisor – The C. Reiss Coal Company), Pete Rotundo (Distribution Manager – KCBX Terminals Company), Mark Cummings (Manager of Bulk Sales & Dev. – The C. Reiss Coal Company), Terry Steinert (Environmental Compliance Manager – Koch Minerals, LLC), John Hydock (Controller – Koch Minerals, LLC), Tom Kramer (General Manager – KCBX Terminals Company), Kermit Altendorfer (General Manager North American Marketing – Koch Carbon, LLC), Dave Emmerich (Operations Manager – The C. Reiss Coal Company) and Michelle Joki (Office Supervisor – The C. Reiss Coal Company) were consulted in preparation of this response and the appendices attached hereto.

#### Request No. 2:

Identify all locations owned or operated by Koch currently used for petroleum coke storage or handling in Region 5.

#### **Response to Request No. 2:**

Koch Minerals objects to this Request to the extent it implies that Koch Minerals "stores" or accepts for "storage" any petroleum coke. For purposes of identifying responsive information, Koch Minerals interprets these terms to refer to staging, rather than storage, of petroleum coke. The following facilities are currently used for petroleum coke staging and handling:

KCBX North (Chicago, Illinois) KCBX South (Chicago, Illinois) Duluth (Duluth, Minnesota) Green Bay (Green Bay, Wisconsin)

Scott Lebbin (Vice-President of Operations – Koch Minerals, LLC), William Reiss (President – The C. Reiss Coal Company), Robert Valley (Dock Superintendent – The C. Reiss Coal Company) and Richard Schlies (Manager of Transportation – Koch Minerals, LLC) were consulted in preparation of this response.

#### Request No. 3:

Identify all locations owned or operated by Koch where future petroleum coke storage or handling is planned, permitted, or zoned in Region 5. Continue to identify and notify EPA of such sites through December 31, 2015. For each location, identify the date Koch plans to use the location and the date when operations commence. Provide an explanation for how and why the location was chosen.

#### **Response to Request No. 3:**

Koch Minerals objects to this Request as improperly issued under Clean Air Act Section 114(a), 42 U.S.C. § 7414(a), because the information sought is not necessary to serve any of the purposes outlined in Section 114(a)(i), (ii), or (iii). Any future petroleum coke staging or handling by Koch Minerals is not currently subject to regulation under the Clean Air Act and therefore is not within the scope of EPA's authority under Section 114(a). Koch Minerals further objects to the request insofar as EPA seeks to require Koch Minerals to "[c]ontinue to identify and notify EPA of such sites through December 31, 2015," as beyond the scope of EPA's Clean Air Act Section 114(a) authority. Furthermore, information regarding "how and why" any location for petroleum coke staging or handling "was chosen" is not relevant to Clean Air Act compliance and therefore is also outside EPA's Section 114(a) authority.

In its January 14<sup>th</sup> electronic message, EPA modified this request to require Koch Minerals to submit documents regarding "locations where there is a current permit application, current permit or current permit that does not prohibit the storage of petcoke." It is Koch Minerals' understanding that air permits issued by state and federal authorities do not typically "prohibit" the handling of a bulk material. Nonetheless, Koch Minerals responds that, in addition to the four sites identified in its response to Request 1, it owns and operates four additional facilities within Region 5 that could at least potentially stage or handle petroleum coke at some point in the future.

Ashland (601 ½ Lake Shore Drive, Ashland, WI) Escanaba Dock 1 (Power Plant Road, Escanaba, MI) Escanaba Dock 2 (1010 3<sup>rd</sup> Avenue North, Escanaba, MI) Manitowoc (937 S. Fifth St., Manitowoc, WI)

Relevant permitting documents and/or applications for each respective facility are attached hereto on Disc 1 in an electronic file folder labeled Response #3 (KM0000044-KM00000478).

In addition to the sites identified above, Koch Minerals or its affiliates own the following industrial sites within Region 5 that do not involve the handling of petroleum coke:

Benton Facility, 5182 State Highway 37, Benton, IL 62812 (Magnetite Handling Facility)

Clarkson Dock, end of 11<sup>th</sup> Ave. East, Ashland, Wisconsin 54806 (Koch Minerals is not presently operating this site and has not since at least January 1, 2004) Superior-Berwind Dock, Adjacent to 3200 Winter Street, Superior, Wisconsin 54880 (Koch Minerals has not operated this site since the early 1980s)

Sault Ste. Marie Dock, South Street, Sault Ste. Marie, MI 49783 (Koch Minerals has not operated this site since the 1990s)

Koch Minerals or its affiliates also own real estate located at 2400 Winter Street, Superior, WI 54880, which it leases to a third party. That third party has informed Koch Minerals that it has not handled petroleum coke at the property at any time since January 1, 2004. Koch Minerals does not have specific information as to whether the facility has permits to handle petroleum coke. Scott Lebbin (Vice-President of Operations – Koch Minerals, LLC), William Reiss (President – The C. Reiss Coal Company), Robert Valley (Dock Superintendent – The C. Reiss Coal Company) and Richard Schlies (Manager of Transportation – Koch Minerals, LLC) were consulted in preparation of this response and the appendices attached hereto.

Koch Minerals welcomes further discussion with EPA regarding the purpose and scope of this Request.

#### Request No. 4:

For all petroleum coke Koch owns or owned that was stored or handled by Detroit Bulk Storage at 115 Rosa Parks Boulevard, Detroit, Michigan, identify each location to which that petroleum coke has been transported. Provide the name of the entity that owns each location with the complete address along with copies of all supporting documentation.

#### **Response to Request No. 4:**

In its January 14th electronic message, EPA modified this request to require Koch Minerals to submit "information regarding the users or end users in Region 5 only." Further, EPA clarified that Koch Minerals should submit "just locations" of users, and that EPA "do[es] not require all back up information."

Koch Minerals responds that it does not own and has never owned any petroleum coke that was stored or handled by Detroit Bulk Storage at 115 Rosa Parks Boulevard, Detroit, Michigan.

David Stout (General Manager West Coast Pet Coke – Koch Carbon, LLC), Kathy Jordan (Carbon Process Improvement Manager – Koch Carbon, LLC, Michael Albrecht (Manager, North American Pet Coke Marketing – Koch Carbon, LLC) were consulted in preparation of this response.

#### Request No. 5:

For all petroleum coke Koch owns or owned that was stored or handled by Detroit Bulk Storage in River Rouge, Michigan, identify each location to which that petroleum coke has been transported. Provide the name of the entity that owns each location with the complete address along with copies of all supporting documentation.

#### **Response to Request No. 5:**

In its January 14th electronic message, EPA modified this request to require Koch Minerals to submit "information regarding the users or end users in Region 5 only." Further, EPA clarified that KCBX should submit "just locations" of users, and that EPA "do[es] not require all back up information."

Koch Minerals responds that it does not own and has never owned any petroleum coke

that was stored or handled by Detroit Bulk Storage in River Rouge, Michigan.

David Stout (General Manager West Coast Pet Coke - Koch Carbon, LLC), Kathy Jordan (Carbon Process Improvement Manager - Koch Carbon, LLC, and Michael Albrecht (Manager, North American Pet Coke Marketing - Koch Carbon, LLC) were consulted in preparation of this response.

The certification requested in the December 30, 2013 information request is attached hereto.

Koch Minerals stands willing to discuss the foregoing responses and the attached appendices with EPA at a mutually convenient time.

Sincerely.

Adam M. Kushner

Partner adam.kushner@hoganlovells.com (202) 637-5724

Enclosures

#### Koch Minerals Certification of January 31, 2014

#### **Response To**

#### EPA's December 30, 2013 Clean Air Act Section 114(a) Information Request

I certify under penalty of law that I have examined and am famillar with the information in the enclosed documents, including all attachments. Based on my inquiry of those individuals with primary responsibility for obtaining the information, I certify that the statements and information are, to the best of my knowledge and belief, true and complete. I am aware that there are significant penalties for knowingly submitting false statements and information, including the possibility of fines or imprisonment pursuant to Section 113(c)(2) of the Clean Alr Act and 18 U.S.C. §§ 1001 and 1341.

Mast J.M.

Scott Lebbin Vice President of Operations Koch Minerals, LLC

	KCBX N	KCBX N	Green Bay	Green Bay	Duluth	Duluth			KCBX N	KCBX N	Green Bay	Green Bay	Duluth	Duluth			KCBX N	KCBX N	Green Bay	Green Bay	Duluth	Duluth
2009	IN	OUT	IN	OUT	IN	OUT		2010	IN	OUT	IN	OUT	IN	OUT		2011	IN	OUT	IN	OUT	IN	OUT
Jan	74768	3039	29211	13461	2901	3007		Jan	26886	0	788	11683	3378	2637		Jan	50267	9899	0	13018	4957	1596
Feb	65265	3486	28839	12603	1521	1417		Feb	16795	0	814	14915	2756	2089		Feb	29205	2731	0	8722	1331	804
Mar	100071	61699	6480	14249	0	1952		Mar	20460	8047	3163	14518	4335	2698		Mar	64508	27328	6816	13449	3490	404
Apr	135371	108189	10080	12714	25	1897		Apr	22232	50151	15098	15295	630	1193		Apr	71942	82925	7844	3605	0	586
May	83543	105611	15930	7058	0	0		May	59248	80420	5596	10464	2967	2266		May	109385	99013	7008	2998	25	1122
Jun	74900	156503	0	18203	0	1784		Jun	64875	132197	11970	16449	2775	2814		Jun	68118	163913	12480	6385	0	0
Jul	83451	77846	20272	16419	278	2893		Jul	57626	61985	10890	11656	705	2292		Jul	102558	65800	25754	13494	0	0
Aug	71757	90320	9	16329	3174	2407		Aug	85909	59379	24519	14219	374	681		Aug	105455	102741	7008	17695	0	790
Sep	55724	40215	15763	13909	2696	1739		Sep	72593	90898	12600	16352	402	0		Sep	100077	136912	0	16137	0	813
Oct	48550	75041	28537	12020	2055	1851		Oct	83568	116145	6570	7485	452	0		Oct	118582	60268	6528	9339	0	678
Nov	34424	90756	29665	13397	2033	1739		Nov	73172	71369	35606	14014	1597	2604		Nov	126033	151946	18685	14446	0	490
Dec	45696	2049	4575	15554	0	3337		Dec	73905	48760	18995	14333	3361	2160		Dec	73532	82326	19391	11181	0	543
TOTAL	873,520	814,754	189,361	165,916	14,683	24,023		TOTAL	657,269	719,351	146,609	161,383	23,732	21,434		TOTAL	1,019,662	985,802	111,514	130,469	9,803	7,826
	KCBX N	KCBX N	KCBX S	KCBX S	Green Bay	Green Bay	Duluth	Duluth			KCBX N	KCBX N	ксвх s	ксвх s	Green Bay	Green Bay	Duluth	Duluth				
2012		OUT	IN	OUT	IN	OUT		OUT		2013		OUT	IN	OUT	,	OUT		OUT				
Jan	IN 68316	37061	0	0	0	12336	IN 2450	746		Jan	IN 63322	24817	18093	0	IN O	16981	IN 0	248				
Feb	34483	0	0	0	0	5774	2430	600		Feb	49628	0	0	0	0	11503	0	248				
Mar	42750	80348	0	0	20352	11601	0	499		Mar	20980	56530	0	136	7844	15576	0	243				
Apr	63471	44894	0	0	13632	11710	0	455		Apr	80498	86047	0	3241	15199	11128	0	381				
May	43064	70783	0	0	20297	12024	0	331		Мау	108659	87731	0	3649	14112	11120	0	295				
Jun	59160	63293	0	0	22792	11431	0	283		Jun	95696	112636	12588	2623	29589	11292	0	297				
Jul	98543	134066	0	0	14180	15228	1301	280		Jul	80916	69860	35077	0	14650	16993	0	315				
Aug	109769	76470	0	0	15688	17612	0	247		Aug	140795	150245	15769	52409	16465	16084	0 0	228				
Sep	69462	29313	0	0	15476	13183	0	255		Sep	104834	59955	13403	40631	20279	10587	0 0	334				
Oct	90940	117583	0	0	31376	10658	0	239		Oct	122115	173618	24843	21327	12560	17422	0	86				
Nov	67672	92037	0	0	7632	15268	0	332		Nov	57321	40402	32248	40276	32248	13588	0 0	0				
	0.0.2	52007	v	•		10100	•	001			0.011		522.0		522.0	10000	-	•				
Dec	42698	70011	13766	0	0	14349	0	396		Dec	76187	138227	78525	66190	0	15488	0	0				
Dec TOTAL	42698 <b>790,328</b>	70011 <b>815,859</b>	13766 <b>13,766</b>	0	0 <b>161,425</b>	14349 <b>151,174</b>	0 <b>5,839</b>	396 <b>4,679</b>		Dec TOTAL	76187 <b>1,000,951</b>	138227 <b>1,000,068</b>	78525 <b>230,546</b>	66190 <b>230,482</b>	0 <b>162,946</b>	15488 <b>168,199</b>	0	0 <b>2,723</b>				

# Exhibit Q

	▼   World > No	rth America > United	d States > Illinois > (	Chicago				
Ĉ	AccuWea	in partnership with		nicago, IL				English (US), °F ▾ Login ▾
	United States WEATHER	Chicago, LOCAL WEATH	FR /	RAINE				
	Now Wee	ekend Ext	ended Mon	th Radar	MinuteCas	t™		
	< November 2013	3 View:		December 🔻	<b>2013</b> ‡		January 2014 >	
	Sunday	Monday	Tuesday	Wednesday	Thursday	Friday	Saturday	
	Dec 1	2	3	4	5	6	7	
	Actual Temp <b>44°</b> Lo 30°	Actual Temp <b>43°</b> Lo 33°	Actual Temp <b>51°</b> Lo 37°	Actual Temp <b>57°</b> Lo 42°	Actual Temp 42° Lo 22°	Actual Temp <b>22°</b> Lo 14°	Actual Temp <b>21°</b> Lo 9°	
	Hist. Avg. 40° Lo 28°	Hist. Avg. 40° Lo 27°	Hist. Avg. 40° Lo 27°	Hist. Avg. <b>39° Lo 26</b> °	Hist. Avg. <b>39° Lo 26</b> °	Hist. Avg. 38° Lo 26°	Hist. Avg. 38° Lo 25°	
	8	9	10 10	11	12	13	14	
	Actual Temp							
	25° Lo 16°	26° Lo 3°	22° Lo 1°	21° Lo 2°	20° Lo -3°	<b>31°</b> Lo 15°	<b>30°</b> Lo 23°	
	Hist. Avg. <b>37°</b> Lo 25°	Hist. Avg. <b>37° Lo 24°</b>	Hist. Avg. <b>37° Lo 24</b> °	Hist.Avg. 36° Lo 24°	Hist.Avg. 36°Lo 24°	Hist. Avg. <b>36° Lo 23°</b>	Hist.Avg. 35°Lo 23°	
	15	16	17	18	19	20	21	
	Actual Temp <b>24°</b> Lo 12°	Actual Temp	Actual Temp <b>33°</b> Lo 16°	Actual Temp <b>34°</b> Lo 16°	Actual Temp <b>43°</b> Lo 34°	Actual Temp <b>37°</b> Lo 34°	Actual Temp <b>36°</b> Lo 32°	
	Hist. Avg. 35° Lo 23°	Hist. Avg. 35° Lo 22°	Hist. Avg. <b>34° Lo 22</b> °	Hist. Avg. <b>34°</b> Lo 22°	Hist. Avg. <b>34° Lo 22°</b>	Hist. Avg. <b>34° Lo 21°</b>	Hist. Avg. <b>34°</b> Lo 21°	
	22	23	24	25	26	27	28	
	Actual Temp	Actual Temp	A ctual Temp	Actual Temp	Actual Temp	Actual Temp	Actual Temp	
	35° Lo 26°	27° LO 0°	<b>19°</b> Lo -1°	27° Lo 19°	<b>36°</b> Lo 15°	<b>44°</b> Lo 26°	51° Lo 34°	
	Hist. Avg. 33° Lo 21°	Hist. Avg. 33° Lo 21°	Hist. Avg. 33° Lo 20°	Hist. Avg. 32° Lo 20°				
	29	30	31	Jan 1	2	3	4	
	Actual Temp							
	<b>39°</b> Lo 12°	15° Lo 3°	<b>14°</b> Lo 4°	<b>24°</b> Lo 14°	22° Lo 5°	20° Lo -2°	<b>33°</b> Lo 20°	
	Hist. Avg. 32° Lo 20°	Hist. Avg. <b>32° Lo 19°</b>	Hist. Avg. <b>32° Lo 19°</b>	Hist.Avg. 32°Lo 19°	Hist.Avg. 32°Lo 19°	Hist. Avg. 32° Lo 19°	Hist. Avg. 32° Lo 19°	

< November 2013

| January 2014 >

**Temperature Graph December 2013** 

#### Company

About Us Advertise With Us Self-Serve Advertising Careers Press

▼ World > No			Chicago				
AccuWea	ather.com		nicago, IL			E	English (US), °F 🔫
United States	Chicago,		FEATURA				
WEATHER	LOCAL WEATH	FR	RAINE				
Now We	ekend Ext	ended Mon	th Radar	MinuteCas	st™		
< December 201	3 View:		January 🔻	2014 ≑		February 2014 >	
Sunday	Monday	Tuesday	Wednesday	Thursday	Friday	Saturday	
Dec 29	30	31	Jan 1	2	3	4	
Actual Temp <b>39°</b> Lo 12°	Actual Temp <b>15°</b> Lo 3°	Actual Temp <b>14°</b> Lo 4°	Actual Temp <b>24°</b> Lo 14°	Actual Temp <b>22°</b> Lo 5°	Actual Temp <b>20°</b> Lo -2°	Actual Temp <b>33°</b> Lo 20°	
Hist. Avg.	Hist. Avg.	Hist. Avg.	Hist. Avg.	Hist. Avg.	Hist. Avg.	Hist. Avg.	
32° Lo 20° 5	32° Lo 19° 6	32° Lo 19° 7	32° Lo 19° 8	32° Lo 19° 9	32° Lo 19° <b>10</b>	32° Lo 19° <b>11</b>	
Actual Temp <b>31°</b> Lo -1°	Actual Temp -1° Lo -15°	Actual Temp <b>5°</b> Lo -11°	Actual Temp <b>15°</b> Lo -2°	Actual Temp <b>29°</b> Lo 2°	Actual Temp 42° Lo 29°	Actual Temp <b>41°</b> Lo 31°	
Hist. Avg.	Hist. Avg.	Hist. Avg.	Hist. Avg.	Hist. Avg.	Hist. Avg.	Hist. Avg.	
32° Lo 19° 12	32° Lo 18° 13	32° Lo 18° <b>14</b>	32° Lo 18° <b>15</b>	31° Lo 18° <b>16</b>	31° Lo 18° <b>17</b>	31° Lo 18° <b>18</b>	
Actual Temp	Actual Temp	Actual Temp	Actual Temp	Actual Temp	Actual Temp	Actual Temp	
<b>44°</b> <sub>Lo</sub> 29° Hist. Avg.	47° Lo 28° Hist. Avg.	35° Lo 22° Hist. Avg.	22° Lo 16°	<b>35°</b> Lo 20° Hist. Avg.	21° Lo 13° Hist. Avg.	<b>21°</b> Lo 11° Hist. Avg.	
31° Lo 18° 19	31° Lo 18°	31° Lo 18° <b>21</b>	31° Lo 18°	31° Lo 18° 23	31° Lo 18°	31° Lo 18° 25	
19	20	21		23	24	23	
Actual Temp	Actual Temp	Actual Temp	Actual Temp	Actual Temp	Actual Temp	Actual Temp	
<b>39°</b> Lo 11°	37° Lo 20°	20° Lo 1°	15° Lo 1°	11° Lo -3°	28° Lo -6°	33° Lo 7°	
Hist. Avg. 31° Lo 18°	Hist. Avg. 31° Lo 18°	Hist. Avg. 31° Lo 18°	Hist. Avg. 31° Lo 18°	Hist. Avg. 31° Lo 18°	Hist. Avg. 31° Lo 18°	Hist. Avg. 32° Lo 18°	
26	27	28	29	30	31	Feb 1	
Actual Temp	Actual Temp	Actual Temp	Actual Temp	Actual Temp	Actual Temp	Actual Temp	
32° LO 6°	6° Lo -7°	<b>4°</b> Lo -11°	22° Lo 1°	33° Lo 19°	<b>28°</b> Lo 19°	<b>32°</b> Lo 23°	
Hist. Avg. <b>32° Lo 18°</b>	Hist. Avg. <b>32° Lo 18°</b>	Hist. Avg. <b>32° Lo 18°</b>	Hist. Avg. 32° Lo 18°	Hist.Avg. 32° Lo 18°	Hist. Avg. 32° Lo 18°	Hist. Avg. 32° Lo 19°	

< December 2013

| February 2014 >

**Temperature Graph January 2014** 

#### Company

About Us Advertise With Us Self-Serve Advertising Careers Press

World >	North America > Unite		Chicago										
🔅 AccuWe	eather.com		nicago, IL				English (US), °F 👻 Login 🤜						
United States WEATHER Chicago, IL LOCAL WEATHER MIGRAINE													
Now W	eekend Ext	ended Mon	th Radar	MinuteCas	t™								
< January 2014	View:		February 🔹 💈	2014 ≑		March 2014 >							
Sunday	Monday	Tuesday	Wednesday	Thursday	Friday	Saturday							
Jan 26	27	28	29	30	31	Feb 1							
Actual Temp <b>32°</b> Lo 6°		Actual Temp <b>4°</b> Lo -11°	Actual Temp <b>22°</b> Lo 1°	Actual Temp <b>33°</b> Lo 19°	Actual Temp <b>28°</b> Lo 19°	Actual Temp <b>32°</b> Lo 23°							
Hist. Avg. 32° Lo 18°	Hist. Avg. <b>32° Lo 18°</b>	Hist. Avg. <b>32° Lo 18°</b>	Hist. Avg. <b>32° Lo 18°</b>	Hist. Avg. <b>32° Lo 18°</b>	Hist. Avg. <b>32° Lo 18°</b>	Hist. Avg. 32° Lo 19°							
2	3	4	5	6	7	8							
Actual Temp 23° Lo 7° Hist. Avg. 32° Lo 19°	Actual Temp 22° Lo 1° Hist. Avg. 33° Lo 19°	Actual Temp <b>25°</b> Lo 10° Hist. Avg. <b>33°</b> Lo 19°	Actual Temp <b>25°</b> Lo 9° Hist. Avg. <b>33°</b> Lo 19°	Actual Temp <b>12°</b> Lo -1° Hist. Avg. <b>33°</b> Lo 20°	Actual Temp <b>11°</b> Lo -3° Hist. Avg. <b>33°</b> Lo 20°	Actual Temp <b>17°</b> Lo 6° Hist. Avg. <b>34°</b> Lo 20°							
9	10	11	12	13	14	15							
Actual Temp 20° Lo 7° Hist. Avg. 34° Lo 20°	Actual Temp <b>13°</b> Lo -2° Hist. Avg. <b>34°</b> Lo 20°	Actual Temp <b>15°</b> Lo -4° Hist. Avg. <b>34°</b> Lo 21°	Actual Temp 23° Lo 2° Hist. Avg. 35° Lo 21°	Actual Temp <b>34°</b> Lo 15° Hist. Avg. <b>35°</b> Lo 21°	Actual Temp 22° Lo 13° Hist. Avg. 35° Lo 21°	Actual Temp <b>24°</b> Lo 6° Hist. Avg. <b>36°</b> Lo 22°							
16	17	18	19	20	21	22							
Actual Temp 28° Lo 18° Hist. Avg. 36° Lo 22°	Actual Temp 29° Lo 22° Hist. Avg. 36° Lo 22°	Actual Temp 45° Lo 23° Hist. Avg. 37° Lo 22°	Actual Temp 45° Lo 32° Hist. Avg. 37° Lo 23°	Actual Temp <b>51°</b> Lo 35° Hist. Avg. <b>37°</b> Lo 23°	Actual Temp <b>37°</b> Lo 28° Hist. Avg. <b>38°</b> Lo 23°	Actual Temp <b>35°</b> Lo 23° Hist. Avg. <b>38°</b> Lo 24°							
23		25	26	27	28	Mar 1							
Actual Temp 29° Lo 16° Hist. Avg. 38° Lo 24°	Actual Temp 25° Lo 13° Hist. Avg. 39° Lo 24°	Actual Temp <b>24°</b> Lo 7° Hist. Avg. <b>39°</b> Lo 25°	Actual Temp <b>19°</b> Lo 1° Hist. Avg. <b>40°</b> Lo 25°	Actual Temp <b>19°</b> Lo 6° Hist. Avg. <b>40°</b> Lo 25°	Actual Temp <b>32°</b> Lo 6° Hist. Avg. <b>40°</b> Lo 26°	Actual Temp <b>32°</b> Lo 12° Hist. Avg. <b>41°</b> Lo 26°							

< January 2014

March 2014 >

#### Temperature Graph February 2014

About Us Advertise With Us Self-Serve Advertising Careers Press

		d States > Illinois > C	Chicago				
AccuWea	ather.com		nicago, IL			E	English (US), °F 👻
ite d Chetter	China na		FEAD				
WEATHER	Chicago, LOCAL WEATH		AINE				
ow Wee	ekend Ext	ended Mon	th Radar	MinuteCas	t™		
ebruary 2014	View:		March <b>v</b> 20	14 ÷		April 2014 >	
			Wednesday	Thursday	Friday		
Sunday Feb 23	Monday 24	Tuesday	26	27	Friday 28	Saturday Mar 1	
red 25	24	25	20	27	20	Mari	
Actual Temp	Actual Temp	Actual Temp	Actual Temp	Actual Temp	Actual Temp	Actual Temp	
29° Lo 16°	25° Lo 13°			19° Lo 6°	32° Lo 6°	32° Lo 12°	
Hist. Avg.	Hist. Avg.	Hist. Avg.	Hist. Avg.	Hist. Avg.	JZ Lo 6° Hist. Avg.	JZ Lo IZ° Hist. Avg.	
38° Lo 24°	<b>39°</b> Lo 24°	<b>39°</b> Lo 25°	40° Lo 25°	40° Lo 25°	40° Lo 26°	41° Lo 26°	
2	3	4	5	6	7	8	
Actual Temp	Actual Temp	Actual Temp	Actual Temp	Actual Temp	Actual Temp	Actual Temp	
16° Lo 5°	20° Lo 1°	<b>27°</b> Lo 12°	<b>24°</b> Lo 20°	32° Lo 16°	46° Lo 20°	<b>39°</b> Lo 23°	
Hist. Avg. <b>41° Lo 26°</b>	Hist. Avg. <b>42° Lo 27°</b>	Hist. Avg. <b>42°</b> Lo 27°	Hist. Avg. <b>42° Lo 27°</b>	Hist. Avg. 43° Lo 28°	Hist. Avg. 43° Lo 28°	Hist. Avg. <b>44° Lo 28°</b>	
9	10	11	12 10 27	13 13	14	15	
Actual Temp	Actual Temp	Actual Temp	Actual Temp	Actual Temp	Actual Temp	Actual Temp	
<b>12°</b> Lo 21°	<b>54°</b> Lo 41°	51° Lo 33°	<b>34°</b> Lo 18°	<b>39°</b> Lo 14°	54° Lo 38°	40° Lo 28°	
Hist. Avg.	Hist. Avg.	Hist. Avg.	Hist. Avg.	Hist. Avg.	Hist. Avg.	Hist. Avg.	
44° Lo 28°	44° Lo 29° 17	45° Lo 29° 18	45° Lo 30° 19	46° Lo 30° 20	46° Lo 30°	46° Lo 30°	
16	17	18	19	20	21	22	
Actual Temp 29° Lo 19°	Actual Temp <b>39°</b> Lo 20°	Actual Temp	Actual Temp <b>47°</b> Lo 35°	Actual Temp <b>48°</b> Lo 31°	Actual Temp <b>58°</b> Lo 33°	Actual Temp <b>42°</b> Lo 29°	
	JJ Lo 20°	<b>JL</b> Lo 30°					
Hist. Avg. 47° Lo 31°	Hist. Avg. <b>47° Lo 31°</b>	Hist. Avg. 48° Lo 32°	Hist. Avg. 48° Lo 32°	Hist. Avg. 48° Lo 32°	Hist. Avg. <b>49° Lo 32°</b>	Hist. Avg. <b>49° Lo 33°</b>	
23	24	25	26	27	28	29	
Actual Temp	Actual Temp	A ctual Temp	Actual Temp	Actual Temp	Actual Temp	Actual Temp	
30° Lo 21°	<b>37°</b> Lo 20°	31° Lo 21°	<b>39°</b> Lo 17°	<b>54°</b> Lo 35°	<b>55°</b> Lo 34°	41° Lo 28°	
Hist. Avg. 50° Lo 33°	Hist. Avg. 50° Lo 34°	Hist. Avg. 50° Lo 34°	Hist. Avg. 51° Lo 34°	Hist. Avg. 51° Lo 35°	Hist. Avg. 52° Lo 35°	Hist. Avg. <b>52°</b> Lo 35°	
30	31	Apr 1	2	3	4	5	
Actual Temp	Actual Temp	Actual Temp	Actual Temp	Actual Temp	Actual Temp	Actual Temp	
5 <b>7°</b> Lo 25°	<b>68°</b> Lo 44°	<b>57°</b> Lo 34°	45° Lo 36°	42° Lo 37°	46° Lo 35°	<b>49°</b> Lo 33°	
Hist. Avg.	Hist. Avg.	Hist. Avg.	Hist. Avg.	Hist. Avg.	Hist. Avg.	Hist. Avg.	
52° Lo 36°	53° Lo 36°	53° Lo 36°	54° Lo 37°	54° Lo 37°	54° Lo 38°	55° Lo 38°	
ebruary 2014	1					April 2014 >	

### **Temperature Graph March 2014**

#### < February 2014

Company

#### http://www.accuweather.com/en/us/chicagoil/60608/month/348308?monyr=3/01/2014