## Traffic Impact Study 3900 South Normal Avenue



Prepared For:

## 3900 S. Normal TMG, LLC

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## I. Executive Summary

This report summarizes the results of a traffic impact study conducted by Kenig, Lindgren, O'Hara, Aboona, Inc. (KLOA, Inc.) for a proposed industrial building to be located at 3900 South Normal Avenue in Chicago, Illinois. The objectives of the traffic study are as follows:

- Determine the existing vehicular, pedestrian, bicycle, and public transportation conditions in the study area to establish a base condition.
- Assess the impact that the proposed development will have on transportation conditions in the area.
- Determine any street, access, bicycle, and pedestrian modifications and/or improvements that will be necessary to effectively accommodate and mitigate future conditions.

Vehicle, pedestrian, and bicycle counts were conducted during the weekday morning and weekday evening peak periods at the intersections of Perishing Road with Wallace Street and Normal Avenue and Root Street with Wallace Street and Normal Avenue in order to determine the general peak hour of traffic activity during these time periods.

As proposed, the site will be developed with an approximately 170,493 square-foot industrial building divided to serve up to four separate tenants. The development will provide a total of 179 parking spaces for employees, 26 spaces for trailer storage, and 16 truck loading bays. Access to the development is proposed to be provided via a full movement access drive on Wallace Street and a full movement access drive on Normal Avenue located approximately 250 feet south of Pershing Road.

Based on the preceding analyses and recommendations, the following conclusions have been made:

- The truck traffic generated by the development is anticipated to have a limited impact on the street system as the majority of truck traffic is expected to arrive and depart the site outside of peak hours.
- Area intersections have sufficient reserve capacity to accommodate the traffic estimated to be generated by the proposed development and no roadway improvements or traffic control modifications are required.
- The proposed access system will be adequate in accommodating the traffic estimated to be generated by the development.


## 1. Introduction

This report summarizes the methodologies, results, and findings of a traffic impact study conducted by Kenig, Lindgren, O'Hara, Aboona, Inc. (KLOA, Inc.) for a proposed industrial building to be located at 3900 South Normal Avenue in Chicago, Illinois. The site, which is currently vacant, is located on the south side of Pershing Road between Normal Avenue and Wallace Street. As proposed, the site will be developed with a multi-tenant industrial building with approximately 170,493 square feet of space. Access to the site is proposed to be provided via a full movement access drive off Wallace Street and a full movement access drive off Normal Avenue.

The purpose of this study was to examine existing traffic conditions, assess the impact that the proposed development will have on traffic conditions in the area, and determine if any determine if any improvements to the transportation system are required to accommodate the proposed development. Figure 1 shows the location of the site in relation to the area street system. Figure 2 shows an aerial view of the site.

The sections of this report present the following:

- Existing street conditions
- A description of the proposed development
- Directional distribution of the development traffic
- Vehicle trip generation for the development
- Future traffic conditions including access to the development
- Traffic analyses for the weekday morning and weekday evening peak hours
- Evaluation and recommendations with respect to adequacy of the site access, on-site circulation, and adjacent street system.

Traffic capacity analyses were conducted for the weekday morning and weekday evening peak hours for the following conditions:

1. Year 2021 Base Conditions - Analyzes the capacity of the existing roadway system using peak hour traffic volumes conducted in 2021 and adjusted to represent pre-pandemic conditions.
2. Year 2027 Total Projected Conditions - Analyzes the capacity of the future roadway system using the projected traffic volumes that include the Year 2021 base traffic volumes, ambient area growth not attributable to any particular development, and the additional traffic estimated to be generated by the proposed development.


Site Location
Figure 1


## 2. Existing Conditions

Existing transportation conditions in the vicinity of the site were documented based on field visits conducted by KLOA, Inc. in order to obtain a database for projecting future conditions. The following provides a description of the geographical location of the site, physical characteristics of the area street system including lane usage and traffic control devices, and existing peak hour traffic volumes.

## Site Location

The site is generally bounded by Pershing Avenue to the north, Normal Avenue to the east, Wallace Street to the west, and the Norfolk Southern Railway (NSR) railroad tracks to the south. The area offers a mixture of residential, industrial, and commercial uses. A U-Haul self-storage facility is located in the southeast quadrant of the intersection of Pershing Road with Normal Avenue and a car wash is located in the southwest quadrant of the intersection of Pershing Road with Wallace Street

## Existing Street System Characteristics

The characteristics of the existing streets near the development are described below and illustrated in Figure 3. All streets are under the jurisdiction of the Chicago Department of Transportation (CDOT) unless otherwise noted.

Pershing Road is an east-west, principal arterial street that provides two lanes in each direction. At its signalized intersection with Wallace Street, Pershing Road provides an exclusive left-turn lane, a through lane, and a shared through/right-turn lane on both approaches. All legs of this intersection provide high visibility crosswalks with pedestrian countdown signals. At its signalized intersection with Normal Avenue, Pershing Road provides one through lane and a shared through/right-turn lane on the eastbound approach and an exclusive left-turn lane and two through lanes on the westbound approach. All legs of this intersection provide high visibility crosswalks with pedestrian countdown signals. Parking is prohibited on both sides of the street between 7:00 A.M. and 9:00 A.M and between 4:00 P.M. and 6:00 P.M. Monday through Friday. Pershing Road is under the jurisdiction of the Illinois Department of Transportation (IDOT), is designated as a Strategic Regional Arterial (SRA) route and carries and Annual Average Daily Traffic of 14,500 vehicles (IDOT 2018).

Root Street is an east-west, minor collector street that provides one lane in each direction. At its all-way stop sign controlled intersection with Wallace Street, Root Street provides a shared left-turn/through/right-turn lane on both approaches. All legs of this intersection provide high visibility crosswalks. At its all-way stop sign controlled intersection with Normal Avenue, Root Street provides a shared left-turn/through/right-turn lane on both approaches. All legs of this intersection provide high visibility crosswalks. Within the vicinity of the site, bike lanes are provided on both sides of Root Street and parking is generally permitted on both sides of the street. Root Street carries an AADT of 1,750 vehicles (IDOT 2018).


Wallace Street is a north-south, local street that provides one lane in each direction. At its signalized intersection with Pershing Road, Wallace Street provides a shared left-turn/through/right-turn lane on both approaches. All legs of this intersection provide high visibility crosswalks and pedestrian countdown timers. At its all-way stop sign controlled intersection with Root Street, Wallace Street provides a shared left-turn/through/right-turn lane on both approaches. All legs of this intersection provide high visibility crosswalks. Within the vicinity of the site parking is generally permitted on both sides of the street. Wallace Street has a viaduct with the NSR railroad tracks and, as such, is not impacted by train activity. Wallace Street carries an AADT of 3,300 vehicles (IDOT 2018).

Normal Avenue is a north-south local street that provides one lane in each direction. At its signalized intersection with Pershing Road, Normal Avenue provides a shared left-turn/right-turn lane on the northbound approach. It should be noted that access between Pershing Road and the north leg of Normal Avenue is prohibited. All legs of this intersection provide high visibility crosswalks and pedestrian countdown timers. At its all-way stop sign controlled intersection with Root Street, Normal Avenue provides a shared left-turn/through/right-turn lane on both approaches. All legs of this intersection provide high visibility crosswalks. Within the vicinity of the site parking is generally permitted on both sides of the street. Normal Avenue has a viaduct with the NSR railroad and, as such, is not impacted by train activity. Normal Avenue carries an AADT of 825 vehicles (IDOT 2018).

## Alternative Modes of Transportation

Accessibility to and from the area is enhanced by the various alternative modes of transportation serving the area as summarized below.

Public Transportation. The area is served by the Chicago Transit Authority (CTA) rapid transit via the Sox-35th Red Line station located approximately 3,500 feet northwest of the site. The CTA Red Line operates 24 hours a day, seven days a week between Howard Street and the $95^{\text {th }} /$ Dan Ryan station located along the Dan Ryan Expressway at $95^{\text {th }}$ Street. Additional service is provided via the Green Line tracks between the Cermak-McCormick Place station and the Ashland/63 ${ }^{\text {rd }}$ station during rush periods only.

In addition, the following bus routes serve the immediate area and have stops near the facility:
Route 39 (Pershing) generally runs along Pershing Road between the Lake Park Avenue and St. Louis Avenue. It operates daily, including holidays, from approximately 5:00 A.M. to 10:00 P.M. on weekdays and from approximately 7:30 A.M. to 5:15 P.M. on Saturdays.

Route 43 (43rd) generally runs along $43^{\text {rd }}$ Street and Root Street between the Oakenwald Avenue and Halsted Avenue. It operates daily, including holidays, from approximately 5:00 A.M. to 8:10 P.M. on weekdays and from approximately 6:40 A.M. to 6:50 P.M. on Saturdays.

Route 44 (Wallace-Racine) generally runs along Wallace and Racine between the Halsted Orange Line Station and $87^{\text {th }}$ Street. It operates daily, including holidays, from approximately 4:30 A.M. to 11:00 P.M. on weekdays and from approximately 8:00 A.M. to 7:30 P.M. on Saturdays.

Pedestrian Accommodations. Sidewalks and high-visibility crosswalks are generally provided on the majority of the streets within the study area.

Bike Facilities. Root Street provides dedicated bike lanes in both directions.

## Year 2021 Base Traffic Volumes

In order to determine current traffic conditions in the vicinity of the site, KLOA, Inc. conducted peak period traffic counts using Miovision Scout Video Collection Units on Tuesday, February 27, 2021 during the weekday morning (6:00 A.M. to 9:00 A.M.) and weekday evening (3:00 P.M. to 6:00 P.M.) peak periods at the following intersections:

- Pershing Road with Wallace Street
- Pershing Road with Normal Avenue
- Root Street with Wallace Street
- Root Street with Normal Avenue

The results of the traffic counts indicated that the weekday morning peak hour of traffic occurs from 7:15 A.M. to 8:15 A.M. and the weekday evening peak hour of traffic occurs from 3:15 P.M. to 4:15 P.M. Copies of the traffic count summary sheets are included in the Appendix. In order to accurately represent Year 2021 conditions due to the ongoing pandemic, the traffic volumes were compared with hourly counts previously conducted by IDOT on Pershing Road east of the site in 2018. Based on the 2018 counts, the 2021 traffic counts were increased by 25 percent during the weekday morning peak hour and 10 percent during the weekday evening peak hour.

Figure 4 illustrates the Year 2021 base peak hour vehicle traffic volumes, inclusive of heavy vehicles. Figure 5 illustrates the Year 2021 base heavy vehicle peak hour traffic volumes. Figure 6 illustrates the existing pedestrian and bicycle volumes, showing direction of travel.




## 3. Traffic Characteristics of the Proposed Development

In order to properly evaluate future traffic conditions in the surrounding area, it was necessary to determine the traffic characteristics of the proposed development, including the directional distribution and volumes of traffic that it will generate.

## Proposed Development Plan

As proposed, the site will be developed with an approximately 170,493 square-foot industrial building divided to serve up to four separate tenants. The development will provide a total of 179 employee parking spaces. 16 truck loading bays will be provided on the east side of the building and 26 trailer storage spaces will be provided on the east side of the site. Access to the development is proposed to be provided as follows:

- A full movement access drive on the east side of Wallace Street located approximately 300 feet south of Pershing Road and will serve the employee parking lot. This access drive will provide one inbound lane and one outbound lane with outbound movements under stop sign control.
- A full movement access drive on the west side of Normal Avenue located approximately 250 feet south of Pershing Road and will primarily serve the truck loading bays and will provide a connection to the employee parking lot south of the building and the parking lot in the northeast corner of the site. This access drive will provide one inbound lane and one outbound lane with outbound movements under stop sign control.

It should be noted that the proposed development will replace an existing curb cut on Wallace Street and an existing curb cut on Normal Avenue serving the site. A copy of the preliminary site plan is included in the appendix.

## Directional Distribution

The directions from which traffic will approach and depart the site was estimated based on existing travel patterns, as determined from the traffic counts and the proposed access system of the development. Figure 7 illustrates the directional distribution of traffic.


## Peak Hour Traffic Volumes

The number of peak hour trips estimated to be generated by the proposed development was based on trip generation rates published by the Institute of Transportation Engineers (ITE) in Trip Generation Manual, $10^{\text {th }}$ Edition. The "General Light Industrial" (Land-Use Code 110) was used for the development. It is important to note that ITE rates indicate that general light industrial developments typically generate minimal truck trips during the peak hours. However, in order to provide a conservative analysis, it was assumed that 10 percent of traffic generated by the development during the peak hours was truck traffic. Table 1 summarizes the trips projected to be generated by the development.

Table 1
ESTIMATED SITE GENERATED TRAFFIC

| ITE LandUse Code | Type/Size | Weekday Morning Peak Hour |  |  | Weekday Evening Peak Hour |  |  | Daily TwoWay Trips |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | In | Out | Total | In | Out | Total |  |
| 110 | General Light Industrial (170,493 s.f.) | 105 | 14 | 119 | 14 | 93 | 107 | 844 |
|  | Passenger Vehicles (90\%) | 94 | 13 | 107 | 13 | 83 | 96 | 760 |
| Trucks (10\%) |  | 11 | 1 | 12 | 1 | 10 | 11 | 84 |

## 4. Projected Traffic Conditions

The total projected traffic volumes include the existing traffic volumes, increase in background traffic due to growth, and the traffic estimated to be generated by the proposed subject development.

## Development Traffic Assignment

The estimated weekday morning and weekday evening peak hour traffic volumes that will be generated by the proposed development were assigned to the street system in accordance with the previously described directional distribution (Figure 7). Figure 8 illustrates the traffic assignment of the new passenger vehicle trips for the development. Figure 9 illustrates the traffic assignment of the new truck trips for the development.

## Ambient Traffic Growth

To account for any additional increase in traffic due to other factors or developments not previously discussed, an ambient growth factor of 0.5 percent per year was also applied to the study area over a six-year period to represent Year 2027 no-build conditions. Furthermore, in order to account for the increase in population in the study area, bicycle and pedestrian volumes were increased by 10 percent at each intersection. Figure 10 illustrates the Year 2027 No Build Volumes.

## Total Projected Traffic Volumes

The Year 2021 base traffic volumes increased by the ambient growth in the area, were combined with the new peak hour traffic volumes generated by the subject development to determine the Year 2027 total traffic volumes, shown in Figure 11.





## 5. Traffic Analysis and Recommendations

The following provides an evaluation conducted for the weekday morning and weekday evening peak hours. The analysis includes conducting capacity analyses to determine how well the street system and access drives are projected to operate and whether any street improvements or modifications are required.

## Traffic Analyses

Intersection analyses were performed for the weekday morning and weekday evening peak hours for the Year 2021 base and Year 2027 total projected traffic volumes.

The traffic analyses were performed using the methodologies outlined in the Transportation Research Board's Highway Capacity Manual (HCM), $6^{\text {th }}$ Edition and analyzed using Synchro/SimTraffic 11 software. The analysis for the signalized intersections were conducted utilizing actual cycle lengths, phasings, and offsets.

The analyses for the unsignalized intersections determine the average control delay to vehicles at an intersection. Control delay is the elapsed time from a vehicle joining the queue at a stop sign (includes the time required to decelerate to a stop) until its departure from the stop sign and resumption of free flow speed. The methodology analyzes each intersection approach controlled by a stop sign and considers traffic volumes on all approaches and lane characteristics.

The ability of an intersection to accommodate traffic flow is expressed in terms of level of service, which is assigned a letter from A to F based on the average control delay experienced by vehicles passing through the intersection. The Highway Capacity Manual definitions for levels of service and the corresponding control delay for signalized intersections and unsignalized intersections are included in the Appendix of this report.

Summaries of the traffic analysis results showing the level of service and overall intersection delay (measured in seconds) for the Year 2021 base and Year 2027 total projected conditions are presented in Tables 2 through 5. A discussion of the intersections follows. Summary sheets for the capacity analyses are included in the Appendix.

Table 2
CAPACITY ANALYSIS RESULTS - PERSHING ROAD WITH WALLACE STREET

|  | Peak <br> Hour | Eastbound |  | Westbound |  | Northbound | Southbound | Overall |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | L | T/R | L | T/R | L/T/R | L/T/R |  |
|  | Weekday Morning Peak Hour | $\begin{gathered} \hline \hline \mathrm{A} \\ 8.2 \end{gathered}$ | $\begin{gathered} \hline \mathrm{A} \\ 9.4 \end{gathered}$ | $\begin{gathered} \hline \mathrm{C} \\ 23.2 \end{gathered}$ | $\begin{gathered} \hline \mathrm{C} \\ 24.2 \end{gathered}$ | $\begin{gathered} \text { B } \\ 19.2 \end{gathered}$ | $\begin{gathered} \text { B } \\ 16.6 \end{gathered}$ | $\begin{gathered} \text { B } \\ 17.1 \end{gathered}$ |
|  |  | A - 9.3 |  | C-24.1 |  |  |  |  |
|  | Weekday Evening Peak Hour | $\begin{gathered} \hline \mathrm{A} \\ 9.2 \end{gathered}$ | $\begin{gathered} \hline \mathrm{A} \\ 9.1 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{C} \\ 27.1 \end{gathered}$ | $\begin{gathered} \mathrm{C} \\ 25.5 \end{gathered}$ | $\begin{gathered} \text { B } \\ 17.7 \end{gathered}$ | $\begin{gathered} \text { B } \\ 18.2 \end{gathered}$ | $\begin{gathered} \text { B } \\ 18.0 \end{gathered}$ |
|  |  | A - 9.1 |  | C-25.7 |  |  |  |  |
|  | Weekday Morning Peak Hour | $\begin{gathered} \hline \mathrm{A} \\ 8.4 \end{gathered}$ | $\begin{gathered} \hline \mathrm{A} \\ 9.6 \end{gathered}$ | $\begin{gathered} \hline \mathrm{C} \\ 26.6 \end{gathered}$ | $\begin{gathered} \mathrm{C} \\ 24.4 \end{gathered}$ | $\begin{gathered} \text { B } \\ 19.7 \end{gathered}$ | $\begin{gathered} \text { B } \\ 16.9 \end{gathered}$ | $\begin{gathered} \text { B } \\ 17.4 \end{gathered}$ |
|  |  | A - 9.5 |  | C-24.7 |  |  |  |  |
|  | Weekday Evening | $\begin{gathered} \mathrm{A} \\ 9.5 \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{A} \\ 9.2 \end{gathered}$ | $\begin{gathered} \text { C } \\ 28.4 \end{gathered}$ | $\begin{gathered} \mathrm{C} \\ 25.7 \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{C} \\ 21.4 \end{gathered}$ | B | B |
|  | Peak <br> Hour | A -9.3 |  | C-26.0 |  |  | 18.6 | 18.8 |
| Letter denotes Level of Service Delay is measured in seconds. |  | $\begin{aligned} & \text { L - Left-Turns } \\ & \text { T - Through } \end{aligned}$ |  |  |  |  | R-Right-Turns |  |

Table 3
CAPACITY ANALYSIS RESULTS - PERSHING ROAD WITH NORMAL AVENUE

|  | Peak <br> Hour | Eastbound | Westbound |  | Northbound | Overall |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | T/R | L/T |  | L/R |  |
|  | Weekday <br> Morning Peak Hour | $\begin{gathered} \text { A } \\ 7.8 \end{gathered}$ | $\begin{gathered} \mathrm{A} \\ 9.3 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { B } \\ 11.2 \\ \hline \end{gathered}$ | $\begin{gathered} \text { A } \\ 8.7 \end{gathered}$ | A |
|  |  |  | B - 11.2 |  |  | 9.5 |
|  | Weekday Evening Peak Hour | $\begin{gathered} \mathrm{A} \\ 7.5 \end{gathered}$ | $\begin{gathered} \hline \text { B } \\ 10.9 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { B } \\ 12.8 \\ \hline \end{gathered}$ | A9.9 | $\begin{gathered} \text { B } \\ 10.3 \end{gathered}$ |
|  |  |  | B-12.7 |  |  |  |
|  | Weekday <br> Morning Peak Hour | $\begin{gathered} \text { A } \\ 8.1 \end{gathered}$ | $\begin{gathered} \text { B } \\ 10.4 \\ \hline \end{gathered}$ | $\begin{gathered} \text { B } \\ 11.6 \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{A} \\ 8.7 \end{gathered}$ | $\begin{gathered} \mathrm{A} \\ 9.9 \end{gathered}$ |
|  |  |  | B - 11.6 |  |  |  |
|  | Weekday Evening | $\begin{gathered} \mathrm{A} \\ 8.5 \end{gathered}$ | $\begin{gathered} \hline \text { B } \\ 11.5 \end{gathered}$ | $\begin{gathered} \hline \text { B } \\ 13.1 \end{gathered}$ | A | B |
|  | Peak <br> Hour |  | B - 13.0 |  | 9.0 | 10.9 |
| Letter denotes Level of Service Delay is measured in seconds. |  |  | L - Left-Turns <br> T - Through |  |  | R - Right-Turns |

Table 4
CAPACITY ANALYSIS RESULTS - UNSIGNALIZED - BASE CONDITIONS

| Intersection | Weekday Morning Peak Hour |  | Weekday Evening Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: |
|  | LOS | Delay | LOS | Delay |
| Root Street with Wallace Street ${ }^{1}$ |  |  |  |  |
| - Overall | A | 9.2 | B | 11.2 |
| - Eastbound Approach | A | 9.3 | B | 12.4 |
| - Westbound Approach | A | 9.2 | B | 10.4 |
| - Northbound Approach | A | 9.2 | B | 10.1 |
| - Southbound Approach | A | 8.9 | B | 11.2 |
| Root Street with Normal Avenue ${ }^{1}$ |  |  |  |  |
| - Overall | A | 8.4 | A | 8.9 |
| - Eastbound Approach | A | 8.4 | A | 9.2 |
| - Westbound Approach | A | 8.5 | A | 8.7 |
| - Northbound Approach | A | 7.9 | A | 8.2 |
| - Southbound Approach | A | 8.7 | A | 8.5 |
| 1 - All-Way Stop Sign Control 2 - Two-Way Stop Sign Control | f Service red in sec |  |  |  |

Table 5
CAPACITY ANALYSIS RESULTS - UNSIGNALIZED - TOTAL PROJECTED CONDITIONS

| Intersection | Weekday Morning Peak Hour |  | Weekday Evening Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: |
|  | LOS | Delay | LOS | Delay |
| Root Street with Wallace Street ${ }^{1}$ |  |  |  |  |
| - Overall | A | 9.4 | B | 11.2 |
| - Eastbound Approach | A | 9.6 | B | 12.4 |
| - Westbound Approach | A | 9.5 | B | 10.4 |
| - Northbound Approach | A | 9.4 | B | 10.1 |
| - Southbound Approach | A | 9.1 | B | 11.2 |
| Root Street with Normal Avenue ${ }^{1}$ |  |  |  |  |
| - Overall | A | 8.7 | A | 8.9 |
| - Eastbound Approach | A | 8.9 | A | 9.2 |
| - Westbound Approach | A | 8.7 | A | 8.7 |
| - Northbound Approach | A | 8.0 | A | 8.2 |
| - Southbound Approach | A | 8.8 | A | 8.5 |
| Wallace Street with the Proposed Site Access ${ }^{2}$ |  |  |  |  |
| - Westbound Approach | B | 10.6 | B | 10.7 |
| - Southbound Left Turn | A | 7.9 | A | 7.7 |
| Normal Avenue with the Proposed Site Access ${ }^{2}$ |  |  |  |  |
| - Eastbound Approach | A | 9.5 | A | 9.3 |
| - Northbound Left Turn | A | 7.8 | -- | -- |
| 1- All-Way Stop Sign Control LOS $=$ Level of Service <br> $2-$ Two-Way Stop Sign Control Delay is measured in seconds. |  |  |  |  |

## Discussion and Recommendations

The following summarizes how the intersections are projected to operate and identifies any street and traffic control improvements necessary to accommodate the development-generated traffic.

## Pershing Road with Wallace Street

The results of the capacity analysis indicate that overall, this intersection currently operates at Level of Service (LOS) B during the weekday morning and weekday evening peak hours. Furthermore, all the intersection movements operate at an acceptable LOS C or better during both peak hours.

Under Year 2027 total projected conditions, the overall intersection is projected to continue operating at LOS B during the weekday morning and weekday evening peak hours with increases in delay of less than one second. Furthermore, all of the intersection movements are projected to continue to operate at an acceptable LOS C or better during both peak hours. As such, this intersection has sufficient reserve capacity to accommodate the traffic estimated to be generated by the proposed development and no street improvements or traffic signal modifications will be required.

## Pershing Road with Wallace Street

The results of the capacity analysis indicate that overall, this intersection currently operates at LOS A during the weekday morning peak hour and LOS B during the weekday evening peak hours Furthermore, all the intersection movements operate at a good LOS B or better during both peak hours.

Under Year 2027 total projected conditions, this intersection overall is projected to continue operating at LOS A during the weekday morning peak hour and LOS B during the weekday evening peak hour with increases in delay of less than one second. Furthermore, all the intersection movements are projected to continue to operate at a good LOS B or better during both peak hours. As such, this intersection has sufficient reserve capacity to accommodate the traffic estimated to be generated by the proposed development and no street improvements or traffic signal modifications will be required.

## Root Street with Wallace Street

The results of the capacity analysis indicate that this all-way stop sign control intersection currently operates at an overall LOS A during the weekday morning peak hour and at an LOS B during the weekday evening peak hour. Furthermore, all the intersection approaches operate at a good LOS B or better during both peak hours.

Under Year 2027 total projected conditions, this intersection is projected to continue operating at existing levels of service during the weekday morning and weekday evening peak hours with increases in delay of less than one second. Furthermore, all the intersection approaches are projected to operate at LOS B or better during both peak hours. As such, this intersection has sufficient reserve capacity to accommodate the traffic estimated to be generated by the proposed development and no street improvements or traffic control modifications will be required.

## Root Street with Normal Avenue

The results of the capacity analysis indicate that this all-way stop sign control intersection currently operate at an overall LOS A during the weekday morning and weekday evening peak hours. Furthermore, all the intersection approaches operate at a good LOS A during both peak hours.

Under Year 2027 total projected conditions, this intersection is projected to continue operating at existing levels of service during the weekday morning and weekday evening peak hours with increases in delay of less than one second. Furthermore, all the intersection approaches are projected to operate at LOS A during both peak hours. As such, this intersection has sufficient reserve capacity to accommodate the traffic estimated to be generated by the proposed development and no street improvements or traffic control modifications will be required.

## Wallace Street with the Proposed Site Access Drive

A proposed, a full movement access drive will be provided on Wallace Street located approximately 300 feet south of Pershing Road and will serve the employee parking lot. This access drive will provide one inbound lane and one outbound lane with outbound movements under stop sign control.

The results of the capacity analysis indicate that outbound movements from the access drive to Wallace Street are projected to operate at LOS B during both peak hours. Furthermore, the southbound left-turn movement from Wallace Street to the access drive are projected to operate at LOS A during both peak hours. As such, this access drive will be adequate in accommodating the traffic generated by the development.

## Normal Avenue with the Proposed Site Access Drive

As proposed, a full movement access drive will be provided on Normal Avenue located approximately 250 feet south of Pershing Road and will primarily serve the truck loading bays and will provide a connection to the employee parking lot south of the building and the parking lot in the northeast corner of the site. This access drive will provide one inbound lane and one outbound lane with outbound movements under stop sign control.

The results of the capacity analysis indicate that outbound movements from the access drive to Normal Avenue are projected to operate at LOS A during both peak hours. Furthermore, the northbound left-turn movement from Normal Avenue onto the access drive are projected to operate at LOS A during both peak hours. As such, this access drive will be adequate in accommodating the traffic generated by the development.

## 6. Conclusion

Based on the preceding analyses and recommendations, the following conclusions have been made:

- Access to the development is proposed to be provided as follows:
- A full movement access drive on the east side of Wallace Street located approximately 300 feet south of Pershing Road and will serve the employee parking lot. This access drive will provide one inbound lane and one outbound lane with outbound movements under stop sign control.
- A full movement access drive on the west side of Normal Avenue located approximately 250 feet south of Pershing Road and will primarily serve the truck loading bays and will provide a connection to the employee parking lot south of the building and the parking lot in the northeast corner of the site. This access drive will provide one inbound lane and one outbound lane with outbound movements under stop sign control.
- The truck traffic generated by the development is anticipated to have a limited impact on the street system as the majority of truck traffic is expected to arrive and depart the site outside of peak hours.
- Area intersections have sufficient reserve capacity to accommodate the traffic estimated to be generated by the proposed development and no roadway improvements or traffic control modifications are required.
- The proposed access system will be adequate in accommodating the traffic estimated to be generated by the development.


## Appendix

## Traffic Count Summary Sheets

Preliminary Site Plan
Level of Service Criteria Capacity Analysis Summary Sheets

## Traffic Count Summary Sheets

Count Name: Pershing Road with Normal Avenue
Rosemont, Illinois, United States 60018 (847)518-9990

Site Code:
Start Date: 04/27/2021
Page No: 1

Turning Movement Data

| Start Time | Pershing Road Eastbound |  |  | Turning Movement Data |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | hing R |  |  |  |  | nal Ave |  |  | Int. Total |
|  | Thru | Right | App. Total | U-Turn | Left | Thru | Peds | App. Total | U-Turn | Left | Right | Peds | App. Total |  |
| 6:00 AM | 81 | 1 | 82 | 0 | 2 | 102 | 0 | 104 | 0 | 2 | 4 | 0 | 6 | 192 |
| 6:15 AM | 96 | 0 | 96 | 0 | 3 | 117 | 0 | 120 | 0 | 1 | 4 | 0 | 5 | 221 |
| 6:30 AM | 101 | 2 | 103 | 0 | 2 | 140 | 0 | 142 | 0 | 2 | 3 | 0 | 5 | 250 |
| 6:45 AM | 93 | 0 | 93 | 0 | 6 | 157 | 0 | 163 | 0 | 2 | 4 | 0 | 6 | 262 |
| Hourly Total | 371 | 3 | 374 | 0 | 13 | 516 | 0 | 529 | 0 | 7 | 15 | 0 | 22 | 925 |
| 7:00 AM | 107 | 2 | 109 | 0 | 2 | 110 | 0 | 112 | 0 | 3 | 6 | 0 | 9 | 230 |
| 7:15 AM | 119 | 0 | 119 | 0 | 1 | 135 | 0 | 136 | 0 | 3 | 1 | 0 | 4 | 259 |
| 7:30 AM | 158 | 3 | 161 | 0 | 5 | 110 | 0 | 115 | 0 | 4 | 4 | 0 | 8 | 284 |
| 7:45 AM | 134 | 1 | 135 | 0 | 3 | 129 | 0 | 132 | 0 | 6 | 7 | 0 | 13 | 280 |
| Hourly Total | 518 | 6 | 524 | 0 | 11 | 484 | 0 | 495 | 0 | 16 | 18 | 0 | 34 | 1053 |
| 8:00 AM | 88 | 2 | 90 | 0 | 3 | 128 | 0 | 131 | 0 | 3 | 6 | 0 | 9 | 230 |
| 8:15 AM | 102 | 3 | 105 | 0 | 5 | 109 | 0 | 114 | 0 | 2 | 7 | 0 | 9 | 228 |
| 8:30 AM | 112 | 2 | 114 | 0 | 2 | 118 | 0 | 120 | 0 | 0 | 6 | 0 | 6 | 240 |
| 8:45 AM | 92 | 2 | 94 | 0 | 4 | 122 | 0 | 126 | 0 | 2 | 1 | 0 | 3 | 223 |
| Hourly Total | 394 | 9 | 403 | 0 | 14 | 477 | 0 | 491 | 0 | 7 | 20 | 0 | 27 | 921 |
| *** BREAK *** | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 3:00 PM | 144 | 5 | 149 | 0 | 4 | 134 | 0 | 138 | 0 | 8 | 8 | 0 | 16 | 303 |
| 3:15 PM | 161 | 2 | 163 | 0 | 5 | 158 | 1 | 163 | 0 | 9 | 4 | 0 | 13 | 339 |
| 3:30 PM | 184 | 3 | 187 | 0 | 2 | 187 | 0 | 189 | 0 | 6 | 2 | 0 | 8 | 384 |
| 3:45 PM | 111 | 4 | 115 | 0 | 5 | 182 | 2 | 187 | 0 | 6 | 4 | 0 | 10 | 312 |
| Hourly Total | 600 | 14 | 614 | 0 | 16 | 661 | 3 | 677 | 0 | 29 | 18 | 0 | 47 | 1338 |
| 4:00 PM | 132 | 3 | 135 | 0 | 12 | 169 | 2 | 181 | 0 | 5 | 6 | 0 | 11 | 327 |
| 4:15 PM | 101 | 0 | 101 | 0 | 8 | 183 | 0 | 191 | 0 | 7 | 2 | 0 | 9 | 301 |
| 4:30 PM | 127 | 1 | 128 | 0 | 11 | 169 | 1 | 180 | 0 | 5 | 3 | 2 | 8 | 316 |
| 4:45 PM | 103 | 2 | 105 | 0 | 7 | 191 | 1 | 198 | 0 | 4 | 4 | 0 | 8 | 311 |
| Hourly Total | 463 | 6 | 469 | 0 | 38 | 712 | 4 | 750 | 0 | 21 | 15 | 2 | 36 | 1255 |
| 5:00 PM | 100 | 1 | 101 | 0 | 6 | 183 | 0 | 189 | 0 | 5 | 8 | 0 | 13 | 303 |
| 5:15 PM | 100 | 0 | 100 | 0 | 5 | 170 | 0 | 175 | 0 | 5 | 4 | 0 | 9 | 284 |
| 5:30 PM | 99 | 2 | 101 | 0 | 6 | 180 | 2 | 186 | 0 | 10 | 5 | 0 | 15 | 302 |
| 5:45 PM | 72 | 2 | 74 | 0 | 6 | 182 | 1 | 188 | 0 | 3 | 3 | 0 | 6 | 268 |
| Hourly Total | 371 | 5 | 376 | 0 | 23 | 715 | 3 | 738 | 0 | 23 | 20 | 0 | 43 | 1157 |
| Grand Total | 2717 | 43 | 2760 | 0 | 115 | 3565 | 10 | 3680 | 0 | 103 | 106 | 2 | 209 | 6649 |
| Approach \% | 98.4 | 1.6 | - | 0.0 | 3.1 | 96.9 | - | - | 0.0 | 49.3 | 50.7 | - | - | - |
| Total \% | 40.9 | 0.6 | 41.5 | 0.0 | 1.7 | 53.6 | - | 55.3 | 0.0 | 1.5 | 1.6 | - | 3.1 | - |
| Lights | 2274 | 38 | 2312 | 0 | 82 | 3095 | - | 3177 | 0 | 98 | 86 | - | 184 | 5673 |
| \% Lights | 83.7 | 88.4 | 83.8 | - | 71.3 | 86.8 | - | 86.3 | - | 95.1 | 81.1 | - | 88.0 | 85.3 |


| Buses | 56 | 0 | 56 | 0 | 1 | 60 | - | 61 | 0 | 0 | 1 | - | 1 | 118 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \% Buses | 2.1 | 0.0 | 2.0 | - | 0.9 | 1.7 | - | 1.7 | - | 0.0 | 0.9 | - | 0.5 | 1.8 |
| Single-Unit Trucks | 177 | 2 | 179 | 0 | 17 | 162 | - | 179 |  | 3 | 14 | - | 17 | 375 |
| \% Single-Unit Trucks | 6.5 | 4.7 | 6.5 | - | 14.8 | 4.5 | - | 4.9 | - | 2.9 | 13.2 | - | 8.1 | 5.6 |
| Articulated Trucks | 210 | 3 | 213 | 0 | 13 | 248 | - | 261 | 0 | 1 | 5 | - | 6 | 480 |
| \% Articulated Trucks | 7.7 | 7.0 | 7.7 | - | 11.3 | 7.0 | - | 7.1 | - | 1.0 | 4.7 | - | 2.9 | 7.2 |
| Bicycles on Road | 0 | 0 | 0 | 0 | 2 | 0 | - | 2 | 0 | 1 | 0 | - | 1 | 3 |
| \% Bicycles on Road | 0.0 | 0.0 | 0.0 | - | 1.7 | 0.0 | - | 0.1 | - | 1.0 | 0.0 | - | 0.5 | 0.0 |
| Pedestrians | - | - | - | $\cdots$ | - | - | 10 | - | - | - | - | 2 | - | - |
| \% Pedestrians | - | - | - | - | - | - | 100.0 | - | - | - | - | 100.0 | - | - |

Rosemont, Illinois, United States 60018 (847)518-9990

Count Name: Pershing Road with Normal Avenue
Site Code:
Start Date: 04/27/2021
Page No: 3

| Start Time | Turning Movement Peak Hour Data (7:15 AM) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Pershing Road Eastbound |  |  | Pershing Road |  |  |  |  | Normal Avenue Northbound |  |  |  |  | Int. Total |
|  | Thru | Right | App. Total | U-Turn | Left | Thru | Peds | App. Total | U-Turn | Left | Right | Peds | App. Total |  |
| 7:15 AM | 119 | 0 | 119 | 0 | 1 | 135 | 0 | 136 | 0 | 3 | 1 | 0 | 4 | 259 |
| 7:30 AM | 158 | 3 | 161 | 0 | 5 | 110 | 0 | 115 | 0 | 4 | 4 | 0 | 8 | 284 |
| 7:45 AM | 134 | 1 | 135 | 0 | 3 | 129 | 0 | 132 | 0 | 6 | 7 | 0 | 13 | 280 |
| 8:00 AM | 88 | 2 | 90 | 0 | 3 | 128 | 0 | 131 | 0 | 3 | 6 | 0 | 9 | 230 |
| Total | 499 | 6 | 505 | 0 | 12 | 502 | 0 | 514 | 0 | 16 | 18 | 0 | 34 | 1053 |
| Approach \% | 98.8 | 1.2 | - | 0.0 | 2.3 | 97.7 | - | - | 0.0 | 47.1 | 52.9 | - | - | - |
| Total \% | 47.4 | 0.6 | 48.0 | 0.0 | 1.1 | 47.7 | - | 48.8 | 0.0 | 1.5 | 1.7 | $\checkmark$ | 3.2 | - |
| PHF | 0.790 | 0.500 | 0.784 | 0.000 | 0.600 | 0.930 | - | 0.945 | 0.000 | 0.667 | 0.643 | - | 0.654 | 0.927 |
| Lights | 382 | 5 | 387 | 0 | 8 | 424 | - | 432 | 0 | 16 | 14 | $\checkmark$ | 30 | 849 |
| \% Lights | 76.6 | 83.3 | 76.6 | - | 66.7 | 84.5 | - | 84.0 | - | 100.0 | 77.8 | - | 88.2 | 80.6 |
| Buses | 15 | 0 | 15 | 0 | 0 | 6 | - | 6 | 0 | 0 | 0 | - | 0 | 21 |
| \% Buses | 3.0 | 0.0 | 3.0 | - | 0.0 | 1.2 | - | 1.2 | - | 0.0 | 0.0 | - | 0.0 | 2.0 |
| Single-Unit Trucks | 53 | 0 | 53 | 0 | 2 | 31 | - | 33 | 0 | 0 | 2 | - | 2 | 88 |
| \% Single-Unit Trucks | 10.6 | 0.0 | 10.5 | - | 16.7 | 6.2 | - | 6.4 | - | 0.0 | 11.1 | - | 5.9 | 8.4 |
| Articulated Trucks | 49 | 1 | 50 | 0 | 2 | 41 | - | 43 | 0 | 0 | 2 | - | 2 | 95 |
| \% Articulated Trucks | 9.8 | 16.7 | 9.9 | - | 16.7 | 8.2 | - | 8.4 | - | 0.0 | 11.1 | - | 5.9 | 9.0 |
| Bicycles on Road | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 0 |
| \% Bicycles on Road | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | $\checkmark$ | 0.0 | 0.0 |
| Pedestrians | - | - | - | - | - | - | 0 | - | - | - | - | 0 | - | - |
| \% Pedestrians | - | - | - | - | - | - | - | - | - | - | - | - | - | - |

Rosemont, Illinois, United States 60018 (847)518-9990

Count Name: Pershing Road with Normal Avenue
Site Code:
Start Date: 04/27/2021
Page No: 4

| Start Time | Turning Movement Peak Hour Data (3:15 PM) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Pershing Road Eastbound |  |  | Pershing Road <br> Westbound |  |  |  |  | Normal Avenue <br> Northbound |  |  |  |  | Int. Total |
|  | Thru | Right | App. Total | U-Turn | Left | Thru | Peds | App. Total | U-Turn | Left | Right | Peds | App. Total |  |
| 3:15 PM | 161 | 2 | 163 | 0 | 5 | 158 | 1 | 163 | 0 | 9 | 4 | 0 | 13 | 339 |
| 3:30 PM | 184 | 3 | 187 | 0 | 2 | 187 | 0 | 189 | 0 | 6 | 2 | 0 | 8 | 384 |
| 3:45 PM | 111 | 4 | 115 | 0 | 5 | 182 | 2 | 187 | 0 | 6 | 4 | 0 | 10 | 312 |
| 4:00 PM | 132 | 3 | 135 | 0 | 12 | 169 | 2 | 181 | 0 | 5 | 6 | 0 | 11 | 327 |
| Total | 588 | 12 | 600 | 0 | 24 | 696 | 5 | 720 | 0 | 26 | 16 | 0 | 42 | 1362 |
| Approach \% | 98.0 | 2.0 | - | 0.0 | 3.3 | 96.7 | - | - | 0.0 | 61.9 | 38.1 | - | - | - |
| Total \% | 43.2 | 0.9 | 44.1 | 0.0 | 1.8 | 51.1 | - | 52.9 | 0.0 | 1.9 | 1.2 | - | 3.1 | - |
| PHF | 0.799 | 0.750 | 0.802 | 0.000 | 0.500 | 0.930 | - | 0.952 | 0.000 | 0.722 | 0.667 | - | 0.808 | 0.887 |
| Lights | 543 | 12 | 555 | 0 | 13 | 592 | - | 605 | 0 | 26 | 15 | - | 41 | 1201 |
| \% Lights | 92.3 | 100.0 | 92.5 | - | 54.2 | 85.1 | - | 84.0 | - | 100.0 | 93.8 | - | 97.6 | 88.2 |
| Buses | 6 | 0 | 6 | 0 | 1 | 14 | - | 15 | 0 | 0 | 0 | - | 0 | 21 |
| \% Buses | 1.0 | 0.0 | 1.0 | - | 4.2 | 2.0 | - | 2.1 | - | 0.0 | 0.0 | - | 0.0 | 1.5 |
| Single-Unit Trucks | 16 | 0 | 16 | 0 | 6 | 26 | - | 32 | 0 | 0 | 1 | - | 1 | 49 |
| \% Single-Unit Trucks | 2.7 | 0.0 | 2.7 | - | 25.0 | 3.7 | - | 4.4 | - | 0.0 | 6.3 | - | 2.4 | 3.6 |
| Articulated Trucks | 23 | 0 | 23 | 0 | 3 | 64 | - | 67 | 0 | 0 | 0 | - | 0 | 90 |
| \% Articulated Trucks | 3.9 | 0.0 | 3.8 | - | 12.5 | 9.2 | - | 9.3 | - | 0.0 | 0.0 | - | 0.0 | 6.6 |
| Bicycles on Road | 0 | 0 | 0 | 0 | 1 | 0 | - | 1 | 0 | 0 | 0 | - | 0 | 1 |
| \% Bicycles on Road | 0.0 | 0.0 | 0.0 | - | 4.2 | 0.0 | - | 0.1 | - | 0.0 | 0.0 | - | 0.0 | 0.1 |
| Pedestrians | - | - | - | - | - | - | 5 | - | - | - | - | 0 | - | - |
| \% Pedestrians | - | - | - | - | - | - | 100.0 | - | - | - | - | - | - | - |



| \% Lights | - | 94.0 | 82.2 | 96.9 | - | 84.1 | - | 91.7 | 86.1 | 94.7 | - | 87.0 | - | 94.2 | 93.6 | 92.3 | - | 93.3 | - | 93.7 | 93.7 | 96.0 | - | 94.3 | 87.6 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Buses | 0 | 1 | 46 | 3 | - | 50 | 0 | 9 | 48 | 3 | - | 60 | 0 | 2 | 21 | 9 | - | 32 | 0 | 1 | 22 | 2 | - | 25 | 167 |
| \% Buses | - | 0.7 | 2.0 | 1.3 | - | 1.9 | - | 2.7 | 1.5 | 1.8 | - | 1.6 | - | 1.3 | 3.8 | 3.1 | - | 3.2 | - | 0.9 | 4.2 | 1.0 | - | 3.0 | 2.1 |
| Single-Unit Trucks | 0 | 5 | 157 | 3 | - | 165 | 0 | 9 | 160 | 4 | - | 173 | 0 | 4 | 6 | 4 | - | 14 | 0 | 6 | 3 | 4 | - | 13 | 365 |
| $\begin{gathered} \text { \% Single-Unit } \\ \text { Trucks } \end{gathered}$ | - | 3.4 | 6.8 | 1.3 | - | 6.2 | - | 2.7 | 5.1 | 2.4 | - | 4.7 | - | 2.6 | 1.1 | 1.4 | - | 1.4 | - | 5.4 | 0.6 | 2.0 | - | 1.6 | 4.5 |
| Articulated Trucks | 0 | 3 | 203 | 0 | - | 206 | 0 | 10 | 229 | 2 | - | 241 | 0 | 3 | 0 | 9 | - | 12 | 0 | 0 | 2 | 2 | - | 4 | 463 |
| $\begin{gathered} \hline \text { \% Articulated } \\ \text { Trucks } \\ \hline \end{gathered}$ | - | 2.0 | 8.8 | 0.0 | - | 7.7 | - | 2.9 | 7.3 | 1.2 | - | 6.6 | - | 1.9 | 0.0 | 3.1 | - | 1.2 | - | 0.0 | 0.4 | 1.0 | - | 0.5 | 5.7 |
| Bicycles on Road | 0 | 0 | 2 | 1 | - | 3 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 8 | 0 | - | 8 | 0 | 0 | 6 | 0 | - | 6 | 17 |
| $\begin{gathered} \text { \% Bicycles on } \\ \text { Road } \end{gathered}$ | - | 0.0 | 0.1 | 0.4 | - | 0.1 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 1.5 | 0.0 | - | 0.8 | - | 0.0 | 1.1 | 0.0 | - | 0.7 | 0.2 |
| Pedestrians | - | - | - | - | 13 | - | - | - | - | - | 10 | - | - | - | - | - | 2 | - | - | - | - | - | 4 | - | - |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | 9575 W. Higgins Rd., Suite 400

Rosemont, Illinois, United States 60018 (847)518-9990

Count Name: Pershing Road with Wallace Street Site Code:
Star Date: 04/27/2021
Page No: 3

Turning Movement Peak Hour Data (7:15 AM)

| Start Time | Pershing Road Eastbound |  |  |  |  |  | Pershing Road Westbound |  |  |  |  |  | Wallace Street <br> Northbound |  |  |  |  |  | Wallace Street Southbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | App. | Int. Total |
| 7:15 AM | 0 | 7 | 100 | 10 | 1 | 117 | 0 | 14 | 124 | 7 | 0 | 145 | 0 | 4 | 37 | 8 | 1 | 49 | 0 | 8 | 22 | 7 | 0 | 37 | 348 |
| 7:30 AM | 0 | 8 | 150 | 4 | 0 | 162 | 0 | 10 | 91 | 7 | 0 | 108 | 0 | 6 | 39 | 9 | 0 | 54 | 0 | 5 | 26 | 9 | 0 | 40 | 364 |
| 7:45 AM | 0 | 8 | 117 | 9 | 4 | 134 | 0 | 9 | 124 | 8 | 0 | 141 | 0 | 8 | 17 | 12 | 0 | 37 | 0 | 7 | 24 | 5 | 4 | 36 | 348 |
| 8:00 AM | 0 | 8 | 80 | 11 | 0 | 99 | 0 | 15 | 106 | 5 | 0 | 126 | 0 | 8 | 18 | 10 | 0 | 36 | 0 | 3 | 10 | 7 | 0 | 20 | 281 |
| Total | 0 | 31 | 447 | 34 | 5 | 512 | 0 | 48 | 445 | 27 | 0 | 520 | 0 | 26 | 111 | 39 | 1 | 176 | 0 | 23 | 82 | 28 | 4 | 133 | 1341 |
| Approach \% | 0.0 | 6.1 | 87.3 | 6.6 | - | - | 0.0 | 9.2 | 85.6 | 5.2 | - | - | 0.0 | 14.8 | 63.1 | 22.2 | - | - | 0.0 | 17.3 | 61.7 | 21.1 | - | - | - |
| Total \% | 0.0 | 2.3 | 33.3 | 2.5 | - | 38.2 | 0.0 | 3.6 | 33.2 | 2.0 | - | 38.8 | 0.0 | 1.9 | 8.3 | 2.9 | - | 13.1 | 0.0 | 1.7 | 6.1 | 2.1 | - | 9.9 | - |
| PHF | 0.000 | 0.969 | 0.745 | 0.773 | - | 0.790 | 0.000 | 0.800 | 0.897 | 0.844 | - | 0.897 | 0.000 | 0.813 | 0.712 | 0.813 | - | 0.815 | 0.000 | 0.719 | 0.788 | 0.778 | - | 0.831 | 0.921 |
| Lights | 0 | 27 | 336 | 34 | - | 397 | 0 | 44 | 377 | 26 | - | 447 | 0 | 23 | 106 | 29 | - | 158 | 0 | 23 | 75 | 27 | - | 125 | 1127 |
| \% Lights | - | 87.1 | 75.2 | 100.0 | - | 77.5 | - | 91.7 | 84.7 | 96.3 | - | 86.0 | - | 88.5 | 95.5 | 74.4 | - | 89.8 | - | 100.0 | 91.5 | 96.4 | - | 94.0 | 84.0 |
| Buses | 0 | 0 | 9 | 0 | - | 9 | 0 | 0 | 5 | 1 | - | 6 | 0 | 1 | 3 | 5 | - | 9 | 0 | 0 | 3 | 0 | - | 3 | 27 |
| \% Buses | - | 0.0 | 2.0 | 0.0 | - | 1.8 | - | 0.0 | 1.1 | 3.7 | - | 1.2 | - | 3.8 | 2.7 | 12.8 | - | 5.1 | - | 0.0 | 3.7 | 0.0 | $\checkmark$ | 2.3 | 2.0 |
| Single-Unit Trucks | 0 | 3 | 50 | 0 | - | 53 | 0 | 3 | 28 | 0 | - | 31 | 0 | 1 | 1 | 2 | - | 4 | 0 | 0 | 1 | 1 | - | 2 | 90 |
| \% Single-Unit Trucks | - | 9.7 | 11.2 | 0.0 | - | 10.4 | - | 6.3 | 6.3 | 0.0 | - | 6.0 | - | 3.8 | 0.9 | 5.1 | - | 2.3 | . | 0.0 | 1.2 | 3.6 | - | 1.5 | 6.7 |
| Articulated Trucks | 0 | 1 | 52 | 0 | - | 53 | 0 | 1 | 35 | 0 | - | 36 | 0 | 1 | 0 | 3 | - | 4 | 0 | 0 | 2 | 0 | - | 2 | 95 |
| $\begin{aligned} & \hline \text { \% Articulated } \\ & \text { Trucks } \\ & \hline \end{aligned}$ | - | 3.2 | 11.6 | 0.0 | - | 10.4 | - | 2.1 | 7.9 | 0.0 | - | 6.9 | - | 3.8 | 0.0 | 7.7 | - | 2.3 | - | 0.0 | 2.4 | 0.0 | - | 1.5 | 7.1 |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 1 | 0 | - | 1 | 0 | 0 | 1 | 0 | - | 1 | 2 |
| $\begin{gathered} \text { \% Bicycles on } \\ \text { Road } \end{gathered}$ | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.9 | 0.0 | - | 0.6 | - | 0.0 | 1.2 | 0.0 | - | 0.8 | 0.1 |
| Pedestrians | - | - | - | - | 5 | - | - | - | - | - | 0 | - | - | - | - | - | 1 | - | - | - | - | - | 4 | - | - |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | - | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | 9575 W. Higgins Rd., Suite 400

Rosemont, Illinois, United States 60018 (847)518-9990

Count Name: Pershing Road with Wallace Street Site Code:
Plart Date: 04/27/2021
Page No: 4

Turning Movement Peak Hour Data (3:15 PM)

| Start Time | Pershing Road Eastbound |  |  |  |  |  | Pershing Road Westbound |  |  |  |  |  | Wallace Street Northbound |  |  |  |  |  | Wallace Street Southbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | App. | Int. Total |
| 3:15 PM | 0 | 10 | 141 | 15 | 0 | 166 | 0 | 19 | 128 | 9 | 0 | 156 | 0 | 5 | 30 | 18 | 0 | 53 | 0 | 3 | 38 | 14 | 0 | 55 | 430 |
| 3:30 PM | 0 | 10 | 171 | 21 | 0 | 202 | 0 | 16 | 179 | 6 | 0 | 201 | 0 | 6 | 27 | 15 | 0 | 48 | 0 | 6 | 38 | 14 |  | 58 | 509 |
| 3:45 PM | 0 | 10 | 104 | 14 | 2 | 128 | 0 | 25 | 163 | 12 | 0 | 200 | 0 | 4 | 29 | 15 | 0 | 48 | 0 | 2 | 24 | 6 | 0 | 32 | 408 |
| 4:00 PM | 0 | 6 | 104 | 16 | 0 | 126 | 0 | 21 | 144 | 8 | 5 | 173 | 0 | 9 | 26 | 14 | 0 | 49 | 0 | 7 | 31 | 5 | 0 | 43 | 391 |
| Total | 0 | 36 | 520 | 66 | 2 | 622 | 0 | 81 | 614 | 35 | 5 | 730 | 0 | 24 | 112 | 62 | 0 | 198 | 0 | 18 | 131 | 39 | 0 | 188 | 1738 |
| Approach \% | 0.0 | 5.8 | 83.6 | 10.6 | - | - | 0.0 | 11.1 | 84.1 | 4.8 | - | - | 0.0 | 12.1 | 56.6 | 31.3 | - | - | 0.0 | 9.6 | 69.7 | 20.7 | - | - | - |
| Total \% | 0.0 | 2.1 | 29.9 | 3.8 | - | 35.8 | 0.0 | 4.7 | 35.3 | 2.0 | - | 42.0 | 0.0 | 1.4 | 6.4 | 3.6 | - | 11.4 | 0.0 | 1.0 | 7.5 | 2.2 | - | 10.8 | - |
| PHF | 0.000 | 0.900 | 0.760 | 0.786 | - | 0.770 | 0.000 | 0.810 | 0.858 | 0.729 | - | 0.908 | 0.000 | 0.667 | 0.933 | 0.861 | - | 0.934 | 0.000 | 0.643 | 0.862 | 0.696 | - | 0.810 | 0.854 |
| Lights | 0 | 34 | 476 | 61 | - | 571 | 0 | 73 | 519 | 35 | - | 627 | 0 | 22 | 107 | 62 | - | 191 | 0 | 17 | 125 | 38 | - | 180 | 1569 |
| \% Lights | - | 94.4 | 91.5 | 92.4 | - | 91.8 | - | 90.1 | 84.5 | 100.0 | - | 85.9 | - | 91.7 | 95.5 | 100.0 | - | 96.5 | - | 94.4 | 95.4 | 97.4 | - | 95.7 | 90.3 |
| Buses | 0 | 0 | 6 | 2 | - | 8 | 0 | 3 | 11 | 0 | - | 14 | 0 | 1 | 4 | 0 | - | 5 | 0 | 1 | 4 | 0 | - | 5 | 32 |
| \% Buses | - | 0.0 | 1.2 | 3.0 | - | 1.3 | - | 3.7 | 1.8 | 0.0 | - | 1.9 | - | 4.2 | 3.6 | 0.0 | - | 2.5 | - | 5.6 | 3.1 | 0.0 | - | 2.7 | 1.8 |
| Single-Unit Trucks | 0 | 1 | 15 | 2 | - | 18 | 0 | 1 | 32 | 0 | - | 33 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 1 | - | 1 | 52 |
| $\begin{gathered} \hline \text { \% Single-Unit } \\ \text { Trucks } \\ \hline \end{gathered}$ | - | 2.8 | 2.9 | 3.0 | - | 2.9 | - | 1.2 | 5.2 | 0.0 | - | 4.5 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | 2.6 | - | 0.5 | 3.0 |
| Articulated Trucks | 0 | 1 | 22 | 0 | - | 23 | 0 | 4 | 52 | 0 | - | 56 | 0 | 1 | 0 | 0 | - | 1 | 0 | 0 | 0 | 0 | - | 0 | 80 |
| \% Articulated Trucks | - | 2.8 | 4.2 | 0.0 | - | 3.7 | . | 4.9 | 8.5 | 0.0 | - | 7.7 | - | 4.2 | 0.0 | 0.0 | - | 0.5 | . | 0.0 | 0.0 | 0.0 | - | 0.0 | 4.6 |
| Bicycles on Road | 0 | 0 | 1 | 1 | - | 2 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 1 | 0 | - | 1 | 0 | 0 | 2 | 0 | - | 2 | 5 |
| \% Bicycles on Road | - | 0.0 | 0.2 | 1.5 | - | 0.3 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.9 | 0.0 | - | 0.5 | . | 0.0 | 1.5 | 0.0 | - | 1.1 | 0.3 |
| Pedestrians | - | - | - | - | 2 | - | - | - | - | - | 5 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | - | - | - | - | - | - | - | - | - |

Count Name: Root Street with Normal Avenue Site Code:
Rosemont, Illinois, United States 60018
(847)518-9990
ate: 04/27/2021
Page No: 1

| Start Time | Root Street Eastbound |  |  |  |  |  | Root Street Westbound |  |  |  |  |  | Normal Avenue Northbound |  |  |  |  |  | Normal Avenue Southbound |  |  |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. <br> Total |  |
| 6:00 AM | 0 | 2 | 30 | 0 | 2 | 32 | 0 | 0 | 20 | 2 | 0 | 22 | 0 | 1 | 1 | 1 | 0 | 3 | 0 | 2 | 0 | 0 | 0 | 2 | 59 |
| 6:15 AM | 0 | 1 | 16 | 1 | 0 | 18 | 0 | 0 | 29 | 2 | 0 | 31 | 0 | 3 | 3 | 1 | 0 | 7 | 0 | 1 | 0 | 0 | 0 | 1 | 57 |
| 6:30 AM | 0 | 2 | 18 | 0 | 0 | 20 | 0 | 0 | 26 | 1 | 0 | 27 | 0 | 3 | 1 | 1 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 52 |
| 6:45 AM | 0 | 1 | 23 | 1 | 1 | 25 | 0 | 1 | 37 | 2 | 0 | 40 | 0 | 3 | 3 | 2 | 0 | 8 | 0 | 1 | 0 | 1 | 0 | 2 | 75 |
| Hourly Total | 0 | 6 | 87 | 2 | 3 | 95 | 0 | 1 | 112 | 7 | 0 | 120 | 0 | 10 | 8 | 5 | 0 | 23 | 0 | 4 | 0 | 1 | 0 | 5 | 243 |
| 7:00 AM | 0 | 3 | 34 | 1 | 1 | 38 | 0 | 0 | 24 | 1 | 0 | 25 | 0 | 1 | 1 | 2 | 0 | 4 | 0 | 1 | 1 | 1 | 0 | 3 | 70 |
| 7:15 AM | 0 | 0 | 22 | 1 | 0 | 23 | 0 | 0 | 21 | 1 | 1 | 22 | 0 | 4 | 3 | 3 | 1 | 10 | 0 | 3 | 2 | 2 | 0 | 7 | 62 |
| 7:30 AM | 0 | 1 | 17 | 2 | 0 | 20 | 0 | 2 | 32 | 5 | 0 | 39 | 0 | 3 | 3 | 3 | 1 | 9 | 0 | 0 | 2 | 0 | 0 | 2 | 70 |
| 7:45 AM | 0 | 3 | 29 | 0 | 1 | 32 | 0 | 5 | 27 | 2 | 1 | 34 | 0 | 3 | 4 | 3 | 1 | 10 | 0 | 2 | 2 | 1 | 1 | 5 | 81 |
| Hourly Total | 0 | 7 | 102 | 4 | 2 | 113 | 0 | 7 | 104 | 9 | 2 | 120 | 0 | 11 | 11 | 11 | 3 | 33 | 0 | 6 | 7 | 4 | 1 | 17 | 283 |
| 8:00 AM | 0 | 3 | 12 | 0 | 0 | 15 | 0 | 1 | 35 | 1 | 1 | 37 | 0 | 3 | 5 | 2 | 0 | 10 | 0 | 2 | 1 | 0 | 0 | 3 | 65 |
| 8:15 AM | 0 | 2 | 24 | 1 | 0 | 27 | 0 | 0 | 34 | 0 | 0 | 34 | 0 | 4 | 2 | 2 | 3 | 8 | 0 | 1 | 1 | 0 | 0 | 2 | 71 |
| 8:30 AM | 0 | 1 | 18 | 2 | 0 | 21 | 0 | 0 | 20 | 1 | 1 | 21 | 0 | 3 | 2 | 0 | 1 | 5 | 0 | 1 | 3 | 1 | 0 | 5 | 52 |
| 8:45 AM | 0 | 1 | 27 | 1 | 1 | 29 | 0 | 1 | 26 | 3 | 1 | 30 | 0 | 4 | 2 | 2 | 3 | 8 | 0 | 2 | 0 | 2 | 1 | 4 | 71 |
| Hourly Total | 0 | 7 | 81 | 4 | 1 | 92 | 0 | 2 | 115 | 5 | 3 | 122 | 0 | 14 | 11 | 6 | 7 | 31 | 0 | 6 | 5 | 3 | 1 | 14 | 259 |
| *** BREAK *** | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 3:00 PM | 0 | 2 | 45 | 3 | 0 | 50 | 0 | 0 | 22 | 0 | 0 | 22 | 0 | 5 | 9 | 2 | 2 | 16 | 0 | 2 | 2 | 2 | 0 | 6 | 94 |
| 3:15 PM | 0 | 2 | 40 | 6 | 1 | 48 | 0 | 3 | 36 | 5 | 0 | 44 | 0 | 5 | 6 | 1 | 0 | 12 | 0 | 0 | 3 | 1 | 0 | 4 | 108 |
| 3:30 PM | 0 | 3 | 50 | 6 | 1 | 59 | 0 | 5 | 23 | 1 | 1 | 29 | 0 | 3 | 3 | 2 | 0 | 8 | 0 | 0 | 4 | 1 | 0 | 5 | 101 |
| 3:45 PM | 1 | 2 | 33 | 7 | 0 | 43 | 0 | 0 | 24 | 4 | 2 | 28 | 0 | 3 | 4 | 1 | 0 | 8 | 0 | 1 | 4 | 1 | 0 | 6 | 85 |
| Hourly Total | 1 | 9 | 168 | 22 | 2 | 200 | 0 | 8 | 105 | 10 | 3 | 123 | 0 | 16 | 22 | 6 | 2 | 44 | 0 | 3 | 13 | 5 | 0 | 21 | 388 |
| 4:00 PM | 0 | 1 | 33 | 4 | 2 | 38 | 0 | 1 | 57 | 2 | 0 | 60 | 0 | 2 | 3 | 0 | 2 | 5 | 0 | 3 | 5 | 4 | 0 | 12 | 115 |
| 4:15 PM | 0 | 3 | 30 | 4 | 0 | 37 | 0 | 1 | 31 | 2 | 0 | 34 | 0 | 5 | 4 | 0 | 0 | 9 | 0 | 4 | 1 | 7 | 0 | 12 | 92 |
| 4:30 PM | 0 | 1 | 34 | 10 | 0 | 45 | 1 | 2 | 35 | 1 | 0 | 39 | 0 | 4 | 9 | 1 | 0 | 14 | 0 | 2 | 5 | 2 | 1 | 9 | 107 |
| 4:45 PM | 0 | 2 | 25 | 4 | 2 | 31 | 0 | 4 | 17 | 1 | 1 | 22 | 0 | 10 | 6 | 0 | 1 | 16 | 0 | 1 | 5 | 4 | 0 | 10 | 79 |
| Hourly Total | 0 | 7 | 122 | 22 | 4 | 151 | 1 | 8 | 140 | 6 | 1 | 155 | 0 | 21 | 22 | 1 | 3 | 44 | 0 | 10 | 16 | 17 | 1 | 43 | 393 |
| 5:00 PM | 0 | 4 | 30 | 6 | 2 | 40 | 0 | 2 | 34 | 4 | 0 | 40 | 0 | 5 | 6 | 0 | 6 | 11 | 0 | 6 | 4 | 3 | 0 | 13 | 104 |
| 5:15 PM | 0 | 2 | 31 | 3 | 1 | 36 | 0 | 3 | 28 | 2 | 0 | 33 | 0 | 0 | 5 | 0 | 3 | 5 | 0 | 3 | 1 | 3 | 0 | 7 | 81 |
| 5:30 PM | 0 | 2 | 23 | 3 | 0 | 28 | 0 | 4 | 24 | 0 | 0 | 28 | 0 | 5 | 9 | 0 | 4 | 14 | 0 | 1 | 4 | 1 | 0 | 6 | 76 |
| 5:45 PM | 0 | 2 | 31 | 3 | 2 | 36 | 0 | 2 | 30 | 2 | 0 | 34 | 0 | 3 | 6 | 1 | 2 | 10 | 0 | 0 | 5 | 2 | 0 | 7 | 87 |
| Hourly Total | 0 | 10 | 115 | 15 | 5 | 140 | 0 | 11 | 116 | 8 | 0 | 135 | 0 | 13 | 26 | 1 | 15 | 40 | 0 | 10 | 14 | 9 | 0 | 33 | 348 |
| Grand Total | 1 | 46 | 675 | 69 | 17 | 791 | 1 | 37 | 692 | 45 | 9 | 775 | 0 | 85 | 100 | 30 | 30 | 215 | 0 | 39 | 55 | 39 | 3 | 133 | 1914 |
| Approach \% | 0.1 | 5.8 | 85.3 | 8.7 | - | - | 0.1 | 4.8 | 89.3 | 5.8 | - | - | 0.0 | 39.5 | 46.5 | 14.0 | - | - | 0.0 | 29.3 | 41.4 | 29.3 | - | - | - |
| Total \% | 0.1 | 2.4 | 35.3 | 3.6 | - | 41.3 | 0.1 | 1.9 | 36.2 | 2.4 | - | 40.5 | 0.0 | 4.4 | 5.2 | 1.6 | - | 11.2 | 0.0 | 2.0 | 2.9 | 2.0 | - | 6.9 | - |
| Lights | 1 | 41 | 588 | 65 | - | 695 | 1 | 36 | 607 | 40 | - | 684 | 0 | 83 | 91 | 28 | - | 202 | 0 | 32 | 50 | 32 | - | 114 | 1695 |


| \% Lights | 100.0 | 89.1 | 87.1 | 94.2 | - | 87.9 | 100.0 | 97.3 | 87.7 | 88.9 | - | 88.3 | - | 97.6 | 91.0 | 93.3 | - | 94.0 | - | 82.1 | 90.9 | 82.1 | - | 85.7 | 88.6 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Buses | 0 | 0 | 55 | 0 | - | 55 | 0 | 0 | 39 | 2 | - | 41 | 0 | 0 | 1 | 1 |  | 2 | 0 | 0 | 0 | 0 |  | 0 | 98 |
| \% Buses | 0.0 | 0.0 | 8.1 | 0.0 | - | 7.0 | 0.0 | 0.0 | 5.6 | 4.4 | - | 5.3 | - | 0.0 | 1.0 | 3.3 | - | 0.9 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | 5.1 |
| Single-Unit Trucks | 0 | 1 | 27 | 1 | - | 29 | 0 | 0 | 31 | 0 | - | 31 | 0 | 1 | 3 | 0 | - | 4 | 0 | 3 | 0 | 2 | - | 5 | 69 |
| $\begin{gathered} \hline \text { \% Single-Unit } \\ \text { Trucks } \\ \hline \end{gathered}$ | 0.0 | 2.2 | 4.0 | 1.4 | - | 3.7 | 0.0 | 0.0 | 4.5 | 0.0 | - | 4.0 | - | 1.2 | 3.0 | 0.0 | - | 1.9 | - | 7.7 | 0.0 | 5.1 | - | 3.8 | 3.6 |
| Articulated Trucks | 0 | 2 | 3 | 0 | - | 5 | 0 | 0 | 10 | 2 | - | 12 | 0 | 1 | 3 | 0 | - | 4 | 0 | 4 | 2 | 4 | - | 10 | 31 |
| \% Articulated Trucks | 0.0 | 4.3 | 0.4 | 0.0 | - | 0.6 | 0.0 | 0.0 | 1.4 | 4.4 | - | 1.5 | - | 1.2 | 3.0 | 0.0 | - | 1.9 | - | 10.3 | 3.6 | 10.3 | - | 7.5 | 1.6 |
| Bicycles on Road | 0 | 2 | 2 | 3 | - | 7 | 0 | 1 | 5 | 1 | - | 7 | 0 | 0 | 2 | 1 | - | 3 | 0 | 0 | 3 | 1 | - | 4 | 21 |
| \% Bicycles on Road | 0.0 | 4.3 | 0.3 | 4.3 | - | 0.9 | 0.0 | 2.7 | 0.7 | 2.2 | - | 0.9 | - | 0.0 | 2.0 | 3.3 | - | 1.4 | - | 0.0 | 5.5 | 2.6 | - | 3.0 | 1.1 |
| Pedestrians | - | - | - | - | 17 | - | - | - | - | - | 9 | - | - | - | - | - | 30 | - | - | - | - | - | 3 | - | - |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - |

Kenig Lindgren O'Hara Aboona, Inc 9575 W. Higgins Rd., Suite 400

Rosemont, Illinois, United States 60018
Count Name: Root Street with Normal Avenue Site Code:
ate: 04/27/2021
(847)518-9990

Page No: 3

Turning Movement Peak Hour Data (7:15 AM)

| Start Time | Root Street Eastbound |  |  |  |  |  | Root Street Westbound |  |  |  |  |  | Normal Avenue Northbound |  |  |  |  |  | Normal Avenue Southbound |  |  |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. Total | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | $\begin{aligned} & \text { App. } \\ & \text { Total } \\ & \hline \end{aligned}$ |  |
| 7:15 AM | 0 | 0 | 22 | 1 | 0 | 23 | 0 | 0 | 21 | 1 | 1 | 22 | 0 | 4 | 3 | 3 | 1 | 10 | 0 | 3 | 2 | 2 | 0 | 7 | 62 |
| 7:30 AM | 0 | 1 | 17 | 2 | 0 | 20 | 0 | 2 | 32 | 5 | 0 | 39 | 0 | 3 | 3 | 3 | 1 | 9 | 0 | 0 | 2 | 0 | 0 | 2 | 70 |
| 7:45 AM | 0 | 3 | 29 | 0 | 1 | 32 | 0 | 5 | 27 | 2 | 1 | 34 | 0 | 3 | 4 | 3 | 1 | 10 | 0 | 2 | 2 | 1 | 1 | 5 | 81 |
| 8:00 AM | 0 | 3 | 12 | 0 | 0 | 15 | 0 | 1 | 35 | 1 | 1 | 37 | 0 | 3 | 5 | 2 | 0 | 10 | 0 | 2 | 1 | 0 | 0 | 3 | 65 |
| Total | 0 | 7 | 80 | 3 | 1 | 90 | 0 | 8 | 115 | 9 | 3 | 132 | 0 | 13 | 15 | 11 | 3 | 39 | 0 | 7 | 7 | 3 | 1 | 17 | 278 |
| Approach \% | 0.0 | 7.8 | 88.9 | 3.3 | - | - | 0.0 | 6.1 | 87.1 | 6.8 | - | - | 0.0 | 33.3 | 38.5 | 28.2 | - | - | 0.0 | 41.2 | 41.2 | 17.6 | - | - | - |
| Total \% | 0.0 | 2.5 | 28.8 | 1.1 | - | 32.4 | 0.0 | 2.9 | 41.4 | 3.2 | - | 47.5 | 0.0 | 4.7 | 5.4 | 4.0 | - | 14.0 | 0.0 | 2.5 | 2.5 | 1.1 | - | 6.1 | - |
| PHF | 0.000 | 0.583 | 0.690 | 0.375 | - | 0.703 | 0.000 | 0.400 | 0.821 | 0.450 | - | 0.846 | 0.000 | 0.813 | 0.750 | 0.917 | - | 0.975 | 0.000 | 0.583 | 0.875 | 0.375 | - | 0.607 | 0.858 |
| Lights | 0 | 6 | 61 | 3 | - | 70 | 0 | 8 | 102 | 9 | - | 119 | 0 | 13 | 13 | 10 | - | 36 | 0 | 4 | 6 | 2 | - | 12 | 237 |
| \% Lights | - | 85.7 | 76.3 | 100.0 | - | 77.8 | - | 100.0 | 88.7 | 100.0 | - | 90.2 | - | 100.0 | 86.7 | 90.9 | - | 92.3 | - | 57.1 | 85.7 | 66.7 | - | 70.6 | 85.3 |
| Buses | 0 | 0 | 11 | 0 | - | 11 | 0 | 0 | 5 | 0 | - | 5 | 0 | 0 | 0 | 1 | - | 1 | 0 | 0 | 0 | 0 | - | 0 | 17 |
| \% Buses | - | 0.0 | 13.8 | 0.0 | - | 12.2 | - | 0.0 | 4.3 | 0.0 | - | 3.8 | - | 0.0 | 0.0 | 9.1 | - | 2.6 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | 6.1 |
| Single-Unit Trucks | 0 | 0 | 7 | 0 | - | 7 | 0 | 0 | 5 | 0 | - | 5 | 0 | 0 | 1 | 0 | - | 1 | 0 | 2 | 0 | 0 | - | 2 | 15 |
| \% Single-Unit Trucks | - | 0.0 | 8.8 | 0.0 | - | 7.8 | - | 0.0 | 4.3 | 0.0 | - | 3.8 | - | 0.0 | 6.7 | 0.0 | - | 2.6 | - | 28.6 | 0.0 | 0.0 | - | 11.8 | 5.4 |
| Articulated Trucks | 0 | 1 | 0 | 0 | - | 1 | 0 | 0 | 2 | 0 | - | 2 | 0 | 0 | 1 | 0 | - | 1 | 0 | 1 | 1 | 1 | - | 3 | 7 |
| $\begin{gathered} \hline \text { \% Articulated } \\ \text { Trucks } \\ \hline \end{gathered}$ | - | 14.3 | 0.0 | 0.0 | - | 1.1 | - | 0.0 | 1.7 | 0.0 | - | 1.5 | - | 0.0 | 6.7 | 0.0 | - | 2.6 | - | 14.3 | 14.3 | 33.3 | - | 17.6 | 2.5 |
| Bicycles on Road | 0 | 0 | 1 | 0 | - | 1 | 0 | 0 | 1 | 0 | - | 1 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 2 |
| $\begin{gathered} \% \text { Bicycles on } \\ \text { Road } \end{gathered}$ | . | 0.0 | 1.3 | 0.0 | - | 1.1 | . | 0.0 | 0.9 | 0.0 | - | 0.8 | - | 0.0 | 0.0 | 0.0 | . | 0.0 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.7 |
| Pedestrians | - | - | - | - | 1 | - | - | - | - | - | 3 | - | - | - | - | - | 3 | - | - | - | - | - | 1 | - | - |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | 9575 W. Higgins Rd., Suite 400

Rosemont, Illinois, United States 60018 (847)518-9990

Count Name: Root Street with Normal Avenue Site Code:
ate: 04/27/2021
Page No: 4

Turning Movement Peak Hour Data (3:15 PM)

| Start Time | Root Street Eastbound |  |  |  |  |  | Root Street <br> Westbound |  |  |  |  |  | Normal Avenue Northbound |  |  |  |  |  | Normal Avenue Southbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | App. | Int. Total |
| 3:15 PM | 0 | 2 | 40 | 6 | 1 | 48 | 0 | 3 | 36 | 5 | 0 | 44 | 0 | 5 | 6 | 1 | 0 | 12 | 0 | 0 | 3 | 1 | 0 | 4 | 108 |
| 3:30 PM | 0 | 3 | 50 | 6 | 1 | 59 | 0 | 5 | 23 | 1 | 1 | 29 | 0 | 3 | 3 | 2 | 0 | 8 | 0 | 0 | 4 | 1 | 0 | 5 | 101 |
| 3:45 PM | 1 | 2 | 33 | 7 | 0 | 43 | 0 | 0 | 24 | 4 | 2 | 28 | 0 | 3 | 4 | 1 | 0 | 8 | 0 | 1 | 4 | 1 | 0 | 6 | 85 |
| 4:00 PM | 0 | 1 | 33 | 4 | 2 | 38 | 0 | 1 | 57 | 2 | 0 | 60 | 0 | 2 | 3 | 0 | 2 | 5 | 0 | 3 | 5 | 4 | 0 | 12 | 115 |
| Total | 1 | 8 | 156 | 23 | 4 | 188 | 0 | 9 | 140 | 12 | 3 | 161 | 0 | 13 | 16 | 4 | 2 | 33 | 0 | 4 | 16 | 7 | 0 | 27 | 409 |
| Approach \% | 0.5 | 4.3 | 83.0 | 12.2 | - | - | 0.0 | 5.6 | 87.0 | 7.5 | - | - | 0.0 | 39.4 | 48.5 | 12.1 | - | - | 0.0 | 14.8 | 59.3 | 25.9 | - | - | - |
| Total \% | 0.2 | 2.0 | 38.1 | 5.6 | - | 46.0 | 0.0 | 2.2 | 34.2 | 2.9 | - | 39.4 | 0.0 | 3.2 | 3.9 | 1.0 | - | 8.1 | 0.0 | 1.0 | 3.9 | 1.7 | - | 6.6 | - |
| PHF | 0.250 | 0.667 | 0.780 | 0.821 | - | 0.797 | 0.000 | 0.450 | 0.614 | 0.600 | - | 0.671 | 0.000 | 0.650 | 0.667 | 0.500 | - | 0.688 | 0.000 | 0.333 | 0.800 | 0.438 | - | 0.563 | 0.889 |
| Lights | 1 | 6 | 149 | 22 | - | 178 | 0 | 9 | 121 | 10 | - | 140 | 0 | 13 | 16 | 4 | - | 33 | 0 | 3 | 15 | 6 | - | 24 | 375 |
| \% Lights | 100.0 | 75.0 | 95.5 | 95.7 | - | 94.7 | - | 100.0 | 86.4 | 83.3 | - | 87.0 | - | 100.0 | 100.0 | 100.0 | - | 100.0 | - | 75.0 | 93.8 | 85.7 | - | 88.9 | 91.7 |
| Buses | 0 | 0 | 4 | 0 | - | 4 | 0 | 0 | 9 | 2 | - | 11 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 15 |
| \% Buses | 0.0 | 0.0 | 2.6 | 0.0 | - | 2.1 | - | 0.0 | 6.4 | 16.7 | - | 6.8 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | 3.7 |
| Single-Unit Trucks | 0 | 1 | 2 | 1 | - | 4 | 0 | 0 | 9 | 0 | - | 9 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 13 |
| \% Single-Unit Trucks | 0.0 | 12.5 | 1.3 | 4.3 | - | 2.1 | - | 0.0 | 6.4 | 0.0 | - | 5.6 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | 3.2 |
| Articulated Trucks | 0 | 0 | 1 | 0 | - | 1 | 0 | 0 | 1 | 0 | - | 1 | 0 | 0 | 0 | 0 | - | 0 | 0 | 1 | 0 | 1 | - | 2 | 4 |
| $\begin{gathered} \hline \text { \% Articulated } \\ \text { Trucks } \\ \hline \end{gathered}$ | 0.0 | 0.0 | 0.6 | 0.0 | - | 0.5 | - | 0.0 | 0.7 | 0.0 | - | 0.6 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 25.0 | 0.0 | 14.3 | - | 7.4 | 1.0 |
| Bicycles on Road | 0 | 1 | 0 | 0 | - | 1 | 0 | 0 | 0 | 0 | $\checkmark$ | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 1 | 0 | - | 1 | 2 |
| \% Bicycles on Road | 0.0 | 12.5 | 0.0 | 0.0 | - | 0.5 | . | 0.0 | 0.0 | 0.0 | - | 0.0 | . | 0.0 | 0.0 | 0.0 | - | 0.0 | . | 0.0 | 6.3 | 0.0 | - | 3.7 | 0.5 |
| Pedestrians | - | - | - | - | 4 | - | - | - | - | - | 3 | - | - | - | - | - | 2 | - | - | - | - | - | 0 | - | - |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | - | - | - |



| \% Lights | 100.0 | 78.0 | 89.7 | 97.6 | - | 88.2 | - | 96.3 | 88.0 | 86.4 | - | 88.1 | 50.0 | 99.0 | 96.6 | 94.3 | - | 96.6 | - | 78.4 | 96.3 | 86.1 | - | 90.0 | 90.2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Buses | 0 | 32 | 25 | 0 | - | 57 | 0 | 0 | 30 | 10 | - | 40 | 0 | 0 | 1 | 1 | - | 2 | 0 | 28 | 2 | 24 | - | 54 | 153 |
| \% Buses | 0.0 | 19.0 | 4.1 | 0.0 | - | 6.7 | - | 0.0 | 4.4 | 9.1 | - | 4.9 | 0.0 | 0.0 | 0.2 | 1.9 | - | 0.4 | - | 20.1 | 0.5 | 10.1 | - | 6.9 | 5.1 |
| Single-Unit Trucks | 0 | 1 | 26 | 2 | - | 29 | 0 | 0 | 34 | 2 | - | 36 | 0 | 1 | 6 | 1 | - | 8 | 0 | 1 | 6 | 4 | - | 11 | 84 |
| $\begin{aligned} & \hline \text { \% Single-Unit } \\ & \text { Trucks } \\ & \hline \end{aligned}$ | 0.0 | 0.6 | 4.3 | 2.4 | - | 3.4 | - | 0.0 | 5.0 | 1.8 | - | 4.4 | 0.0 | 1.0 | 1.5 | 1.9 | - | 1.4 | - | 0.7 | 1.5 | 1.7 | - | 1.4 | 2.8 |
| Articulated Trucks | 0 | 2 | 6 | 0 | - | 8 | 0 | 0 | 17 | 0 | - | 17 | 0 | 0 | 1 | 0 | - | 1 | 0 | 1 | 3 | 4 | - | 8 | 34 |
| \% Articulated Trucks | 0.0 | 1.2 | 1.0 | 0.0 | - | 0.9 | - | 0.0 | 2.5 | 0.0 | - | 2.1 | 0.0 | 0.0 | 0.2 | 0.0 | - | 0.2 | - | 0.7 | 0.7 | 1.7 | - | 1.0 | 1.1 |
| Bicycles on Road | 0 | 2 | 5 | 0 | - | 7 | 0 | 1 | 1 | 3 | - | 5 | 1 | 0 | 6 | 1 | - | 8 | 0 | 0 | 4 | 1 | - | 5 | 25 |
| $\begin{gathered} \text { \% Bicycles on } \\ \text { Road } \\ \hline \end{gathered}$ | 0.0 | 1.2 | 0.8 | 0.0 | - | 0.8 | - | 3.7 | 0.1 | 2.7 | - | 0.6 | 50.0 | 0.0 | 1.5 | 1.9 | - | 1.4 | - | 0.0 | 1.0 | 0.4 | - | 0.6 | 0.8 |
| Pedestrians | - | - | - | - | 22 | - | - | - | - | - | 18 | - | - | $-$ | - | - | 47 | - | - | - | - | - | 6 | - | $-$ |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - |

Kenig Lindgren O'Hara Aboona, Inc. 9575 W. Higgins Rd., Suite 400

Rosemont, Illinois, United States 60018
Count Name: Root Street with Wallace Stree Site Code:
Ptar No: 04/27/2021
(847)518-9990

Page No: 3

Turning Movement Peak Hour Data (7:15 AM)

| Start Time | Root Street Eastbound |  |  |  |  |  | Root Street Westbound |  |  |  |  |  | Wallace Street Northbound |  |  |  |  |  | Wallace Street Southbound |  |  |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | App. Total | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | $\begin{aligned} & \text { App } \\ & \text { Total } \end{aligned}$ |  |
| 7:15 AM | 0 | 5 | 18 | 1 | 2 | 24 | 0 | 0 | 21 | 7 | 0 | 28 | 0 | 5 | 33 | 3 | 1 | 41 | 0 | 1 | 18 | 2 | 0 | 21 | 114 |
| 7:30 AM | 0 | 11 | 17 | 0 | 1 | 28 | 0 | 0 | 28 | 5 | 2 | 33 | 0 | 6 | 24 | 3 | 2 | 33 | 0 | 0 | 21 | 8 | 1 | 29 | 123 |
| 7:45 AM | 0 | 4 | 24 | 4 | 0 | 32 | 0 | 2 | 29 | 3 | 0 | 34 | 0 | 5 | 15 | 3 | 0 | 23 | 0 | 4 | 19 | 5 | 1 | 28 | 117 |
| 8:00 AM | 0 | 5 | 13 | 5 | 0 | 23 | 0 | 0 | 34 | 4 | 0 | 38 | 0 | 0 | 15 | 1 | 1 | 16 | 0 | 4 | 10 | 3 | 0 | 17 | 94 |
| Total | 0 | 25 | 72 | 10 | 3 | 107 | 0 | 2 | 112 | 19 | 2 | 133 | 0 | 16 | 87 | 10 | 4 | 113 | 0 | 9 | 68 | 18 | 2 | 95 | 448 |
| Approach \% | 0.0 | 23.4 | 67.3 | 9.3 | - | - | 0.0 | 1.5 | 84.2 | 14.3 | - | - | 0.0 | 14.2 | 77.0 | 8.8 | - | - | 0.0 | 9.5 | 71.6 | 18.9 | - | - | - |
| Total \% | 0.0 | 5.6 | 16.1 | 2.2 | - | 23.9 | 0.0 | 0.4 | 25.0 | 4.2 | - | 29.7 | 0.0 | 3.6 | 19.4 | 2.2 | - | 25.2 | 0.0 | 2.0 | 15.2 | 4.0 | - | 21.2 | - |
| PHF | 0.000 | 0.568 | 0.750 | 0.500 | - | 0.836 | 0.000 | 0.250 | 0.824 | 0.679 | - | 0.875 | 0.000 | 0.667 | 0.659 | 0.833 | - | 0.689 | 0.000 | 0.563 | 0.810 | 0.563 | - | 0.819 | 0.911 |
| Lights | 0 | 23 | 55 | 9 | - | 87 | 0 | 2 | 98 | 18 | - | 118 | 0 | 16 | 85 | 10 | - | 111 | 0 | 3 | 61 | 12 | - | 76 | 392 |
| \% Lights | - | 92.0 | 76.4 | 90.0 | - | 81.3 | - | 100.0 | 87.5 | 94.7 | - | 88.7 | - | 100.0 | 97.7 | 100.0 | - | 98.2 | - | 33.3 | 89.7 | 66.7 | - | 80.0 | 87.5 |
| Buses | 0 | 2 | 6 | 0 | - | 8 | 0 | 0 | 5 | 0 | - | 5 | 0 | 0 | 0 | 0 | - | 0 | 0 | 6 | 1 | 5 | - | 12 | 25 |
| \% Buses | - | 8.0 | 8.3 | 0.0 | - | 7.5 | - | 0.0 | 4.5 | 0.0 | - | 3.8 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 66.7 | 1.5 | 27.8 | - | 12.6 | 5.6 |
| Single-Unit Trucks | 0 | 0 | 9 | 1 | - | 10 | 0 | 0 | 6 | 0 | - | 6 | 0 | 0 | 1 | 0 | - | 1 | 0 | 0 | 2 | 1 | - | 3 | 20 |
| \% Single-Unit Trucks | - | 0.0 | 12.5 | 10.0 | - | 9.3 | - | 0.0 | 5.4 | 0.0 | - | 4.5 | - | 0.0 | 1.1 | 0.0 | - | 0.9 | - | 0.0 | 2.9 | 5.6 | - | 3.2 | 4.5 |
| Articulated Trucks | 0 | 0 | 1 | 0 | - | 1 | 0 | 0 | 3 | 0 | - | 3 | 0 | 0 | 1 | 0 | - | 1 | 0 | 0 | 3 | 0 | - | 3 | 8 |
| $\begin{gathered} \hline \text { \% Articulated } \\ \text { Trucks } \\ \hline \end{gathered}$ | - | 0.0 | 1.4 | 0.0 | - | 0.9 | - | 0.0 | 2.7 | 0.0 | - | 2.3 | - | 0.0 | 1.1 | 0.0 | - | 0.9 | - | 0.0 | 4.4 | 0.0 | - | 3.2 | 1.8 |
| Bicycles on Road | 0 | 0 | 1 | 0 | - | 1 | 0 | 0 | 0 | 1 | - | 1 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 1 | 0 | - | 1 | 3 |
| $\begin{gathered} \% \text { Bicycles on } \\ \text { Road } \end{gathered}$ | . | 0.0 | 1.4 | 0.0 | - | 0.9 | . | 0.0 | 0.0 | 5.3 | - | 0.8 | - | 0.0 | 0.0 | 0.0 | . | 0.0 | - | 0.0 | 1.5 | 0.0 | - | 1.1 | 0.7 |
| Pedestrians | - | - | - | - | 3 | - | - | - | - | - | 2 | - | - | - | - | - | 4 | - | - | - | - | - | 2 | - | - |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | 9575 W. Higgins Rd., Suite 400

Rosemont, Illinois, United States 60018 (847)518-9990

Count Name: Root Street with Wallace Stree Site Code:
Ptar Date: 04/27/2021
Page No: 4

Turning Movement Peak Hour Data (3:15 PM)

| Start Time | Root Street Eastbound |  |  |  |  |  | Root Street Westbound |  |  |  |  |  | Wallace Street Northbound |  |  |  |  |  | Wallace Street Southbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | $\begin{aligned} & \text { App. } \\ & \text { Total } \end{aligned}$ | Int. Total |
| 3:15 PM | 0 | 6 | 40 | 3 | 0 | 49 | 0 | 0 | 31 | 7 | 0 | 38 | 0 | 4 | 17 | 4 | 0 | 25 | 0 | 7 | 25 | 16 | 0 | 48 | 160 |
| 3:30 PM | 0 | 9 | 47 | 5 | 0 | 61 | 0 | 0 | 23 | 4 | 0 | 27 | 0 | 5 | 18 | 1 | 1 | 24 | 0 | 11 | 30 | 20 | 0 | 61 | 173 |
| 3:45 PM | 0 | 8 | 28 | 10 | 2 | 46 | 0 | 3 | 23 | 5 | 1 | 31 | 0 | 5 | 23 | 4 | 1 | 32 | 0 | 6 | 23 | 17 | 0 | 46 | 155 |
| 4:00 PM | 0 | 8 | 33 | 4 | 3 | 45 | 0 | 5 | 51 | 9 | 1 | 65 | 0 | 3 | 20 | 2 | 1 | 25 | 0 | 5 | 28 | 17 | 0 | 50 | 185 |
| Total | 0 | 31 | 148 | 22 | 5 | 201 | 0 | 8 | 128 | 25 | 2 | 161 | 0 | 17 | 78 | 11 | 3 | 106 | 0 | 29 | 106 | 70 | 0 | 205 | 673 |
| Approach \% | 0.0 | 15.4 | 73.6 | 10.9 | - | - | 0.0 | 5.0 | 79.5 | 15.5 | - | - | 0.0 | 16.0 | 73.6 | 10.4 | - | - | 0.0 | 14.1 | 51.7 | 34.1 | - | - | - |
| Total \% | 0.0 | 4.6 | 22.0 | 3.3 | - | 29.9 | 0.0 | 1.2 | 19.0 | 3.7 | - | 23.9 | 0.0 | 2.5 | 11.6 | 1.6 | - | 15.8 | 0.0 | 4.3 | 15.8 | 10.4 | - | 30.5 | - |
| PHF | 0.000 | 0.861 | 0.787 | 0.550 | - | 0.824 | 0.000 | 0.400 | 0.627 | 0.694 | - | 0.619 | 0.000 | 0.850 | 0.848 | 0.688 | - | 0.828 | 0.000 | 0.659 | 0.883 | 0.875 | - | 0.840 | 0.909 |
| Lights | 0 | 21 | 139 | 22 | - | 182 | 0 | 8 | 110 | 22 | - | 140 | 0 | 16 | 75 | 9 | - | 100 | 0 | 28 | 102 | 63 | - | 193 | 615 |
| \% Lights | - | 67.7 | 93.9 | 100.0 | - | 90.5 | - | 100.0 | 85.9 | 88.0 | - | 87.0 | - | 94.1 | 96.2 | 81.8 | - | 94.3 | - | 96.6 | 96.2 | 90.0 | - | 94.1 | 91.4 |
| Buses | 0 | 9 | 3 | 0 | - | 12 | 0 | 0 | 6 | 3 | - | 9 | 0 | 0 | 1 | 0 | - | 1 | 0 | 1 | 1 | 4 | - | 6 | 28 |
| \% Buses | - | 29.0 | 2.0 | 0.0 | - | 6.0 | - | 0.0 | 4.7 | 12.0 | - | 5.6 | - | 0.0 | 1.3 | 0.0 | - | 0.9 | - | 3.4 | 0.9 | 5.7 | - | 2.9 | 4.2 |
| Single-Unit Trucks | 0 | 0 | 3 | 0 | - | 3 | 0 | 0 | 8 | 0 | - | 8 | 0 | 1 | 0 | 1 | - | 2 | 0 | 0 | 0 | 2 | - | 2 | 15 |
| \% Single-Unit Trucks | - | 0.0 | 2.0 | 0.0 | - | 1.5 | . | 0.0 | 6.3 | 0.0 | - | 5.0 | - | 5.9 | 0.0 | 9.1 | - | 1.9 | - | 0.0 | 0.0 | 2.9 | - | 1.0 | 2.2 |
| Articulated Trucks | 0 | 1 | 1 | 0 | - | 2 | 0 | 0 | 4 | 0 | - | 4 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 1 | - | 1 | 7 |
| $\begin{aligned} & \text { \% Articulated } \\ & \text { Trucks } \\ & \hline \end{aligned}$ | . | 3.2 | 0.7 | 0.0 | - | 1.0 | - | 0.0 | 3.1 | 0.0 | - | 2.5 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | 1.4 | - | 0.5 | 1.0 |
| Bicycles on Road | 0 | 0 | 2 | 0 | - | 2 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 2 | 1 | - | 3 | 0 | 0 | 3 | 0 | - | 3 | 8 |
| $\begin{gathered} \text { \% Bicycles on } \\ \text { Road } \end{gathered}$ | . | 0.0 | 1.4 | 0.0 | - | 1.0 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 2.6 | 9.1 | - | 2.8 | . | 0.0 | 2.8 | 0.0 | - | 1.5 | 1.2 |
| Pedestrians | - | - | - | - | 5 | - | - | - | - | - | 2 | - | - | - | - | - | 3 | - | - | - | - | - | 0 | - | - |
| \% Pedestrians | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | 100.0 | - | - | - | - | - | - | - | - |

## Preliminary Site Plan



## Level of Service Criteria

| Signalized Intersections |  |  |
| :---: | :---: | :---: |
| Level of Service | Interpretation | $\begin{array}{r} \text { Average Control } \\ \text { Delay } \\ \text { (seconds per vehicle) } \end{array}$ |
| A | Favorable progression. Most vehicles arrive during the green indication and travel through the intersection without stopping. | $\leq 10$ |
| B | Good progression, with more vehicles stopping than for Level of Service A. | >10-20 |
| C | Individual cycle failures (i.e., one or more queued vehicles are not able to depart as a result of insufficient capacity during the cycle) may begin to appear. Number of vehicles stopping is significant, although many vehicles still pass through the intersection without stopping. | >20-35 |
| D | The volume-to-capacity ratio is high and either progression is ineffective or the cycle length is too long. Many vehicles stop and individual cycle failures are noticeable. | > $35-55$ |
| E | Progression is unfavorable. The volume-to-capacity ratio is high and the cycle length is long. Individual cycle failures are frequent. | >55-80 |
| F | The volume-to-capacity ratio is very high, progression is very poor, and the cycle length is long. Most cycles fail to clear the queue. | >80.0 |
| Unsignalized Intersections |  |  |
| Level of Service Average T |  | tal Delay (SEC/VEH) |
|  | A | 0-10 |
|  | B | > $10-15$ |
|  | C | > 15-25 |
|  | D | > 25-35 |
|  | E | > $35-50$ |
|  | F | $>50$ |
| Source: Highway Capacity Manual, 2010. |  |  |

Capacity Analysis Summary Sheets Existing Weekday Morning Peak Hour Conditions

|  | 4 | $\rightarrow$ | $\checkmark$ | 7 |  |  | 4 | $\dagger$ | \% | $v$ |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1}$ | 中 ${ }^{\text {a }}$ |  | ${ }^{1}$ | 中 ${ }^{\text {a }}$ |  |  | \& |  |  | \& |  |
| Traffic Volume (vph) | 39 | 559 | 43 | 60 | 556 | 34 | 33 | 139 | 49 | 29 | 103 | 35 |
| Future Volume (vph) | 39 | 559 | 43 | 60 | 556 | 34 | 33 | 139 | 49 | 29 | 103 | 35 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 10 | 10 | 10 | 10 | 10 | 10 | 12 | 16 | 12 | 12 | 16 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 115 |  | 0 | 160 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 80 |  |  | 90 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Frt |  | 0.989 |  |  | 0.991 |  |  | 0.970 |  |  | 0.972 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  |  | 0.993 |  |  | 0.991 |  |
| Satd. Flow (prot) | 1491 | 2700 | 0 | 1535 | 2869 | 0 | 0 | 1661 | 0 | 0 | 1796 | 0 |
| Flt Permitted | 0.378 |  |  | 0.371 |  |  |  | 0.939 |  |  | 0.923 |  |
| Satd. Flow (perm) | 591 | 2700 | 0 | 599 | 2869 | 0 | 0 | 1570 | 0 | 0 | 1673 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 20 |  |  | 15 |  |  | 23 |  |  | 22 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 2690 |  |  | 679 |  |  | 1667 |  |  | 676 |  |
| Travel Time (s) |  | 61.1 |  |  | 15.4 |  |  | 37.9 |  |  | 15.4 |  |
| Confl. Peds. (\#/hr) | 4 |  | 1 | 1 |  | 4 | 5 |  |  |  |  | 5 |
| Confl. Bikes (\#/hr) |  |  | 2 |  |  |  |  |  | 1 |  |  | 2 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 13\% | 25\% | 0\% | 8\% | 16\% | 3\% | 12\% | 4\% | 27\% | 0\% | 3\% | 8\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 4 | 4 | 4 | 4 | 4 | 4 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 42 | 655 | 0 | 65 | 641 | 0 | 0 | 240 | 0 | 0 | 182 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Permitted Phases | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |  |
| Detector Phase | 2 | 2 |  | 6 | 6 |  | 8 | 8 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 40.0 | 40.0 |  | 40.0 | 40.0 |  | 25.0 | 25.0 |  | 25.0 | 25.0 |  |
| Total Split (s) | 40.0 | 40.0 |  | 40.0 | 40.0 |  | 25.0 | 25.0 |  | 25.0 | 25.0 |  |
| Total Split (\%) | 61.5\% | 61.5\% |  | 61.5\% | 61.5\% |  | 38.5\% | 38.5\% |  | 38.5\% | 38.5\% |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  |  | 4.0 |  |  | 4.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | Max | Max |  | Max | Max |  | Max | Max |  | Max | Max |  |
| Act Effct Green (s) | 36.0 | 36.0 |  | 36.0 | 36.0 |  |  | 21.0 |  |  | 21.0 |  |
| Actuated g/C Ratio | 0.55 | 0.55 |  | 0.55 | 0.55 |  |  | 0.32 |  |  | 0.32 |  |


|  | 4 |  |  | 1 |  |  | , | $\dagger$ | 7 | \% | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.13 | 0.44 |  | 0.20 | 0.40 |  |  | 0.46 |  |  | 0.33 |  |
| Control Delay | 8.2 | 9.4 |  | 23.2 | 24.2 |  |  | 19.2 |  |  | 16.6 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Delay | 8.2 | 9.4 |  | 23.2 | 24.2 |  |  | 19.2 |  |  | 16.6 |  |
| LOS | A | A |  | C | C |  |  | B |  |  | B |  |
| Approach Delay |  | 9.3 |  |  | 24.1 |  |  | 19.2 |  |  | 16.6 |  |
| Approach LOS |  | A |  |  | C |  |  | B |  |  | B |  |
| Queue Length 50th (tt) | 7 | 70 |  | 26 | 140 |  |  | 66 |  |  | 47 |  |
| Queue Length 95th (t) | 21 | 105 |  | 64 | 193 |  |  | 126 |  |  | 93 |  |
| Internal Link Dist (ft) |  | 2610 |  |  | 599 |  |  | 1587 |  |  | 596 |  |
| Turn Bay Length (tt) | 115 |  |  | 160 |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 327 | 1504 |  | 331 | 1595 |  |  | 522 |  |  | 555 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  |  | 0 |  |  | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  |  | 0 |  |  | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  |  | 0 |  |  | 0 |  |
| Reduced v/c Ratio | 0.13 | 0.44 |  | 0.20 | 0.40 |  |  | 0.46 |  |  | 0.33 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 65 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 65 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 40 ( $62 \%$ ), Referenced to phase 2:EBTL and 6:WBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 65 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Pretimed |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.46 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 17.1 |  |  |  | Intersection LOS: B |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 46.8\% |  |  |  | ICU Level of Service A |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Wallace Street \& Pershing Road




Splits and Phases: 2: Normal Avenue \& Pershing Road


| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 9.2 |
| Intersection LOS | A |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | \& |  |  | \& |  |  | $\uparrow$ |  |  | \& |  |
| Traffic Vol, veh/h | 31 | 90 | 13 | 3 | 140 | 24 | 20 | 109 | 13 | 11 | 85 | 23 |
| Future Vol, veh/h | 31 | 90 | 13 | 3 | 140 | 24 | 20 | 109 | 13 | 11 | 85 | 23 |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles, \% | 10 | 22 | 8 | 0 | 13 | 0 | 0 | 3 | 0 | 0 | 9 | 35 |
| Mvmt Flow | 34 | 99 | 14 | 3 | 154 | 26 | 22 | 120 | 14 | 12 | 93 | 25 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 9.3 |  |  | 9.2 |  |  | 9.2 |  |  | 8.9 |  |  |
| HCM LOS | A |  |  | A |  |  | A |  |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $14 \%$ | $23 \%$ | $2 \%$ | $9 \%$ |
| Vol Thru, \% | $77 \%$ | $67 \%$ | $84 \%$ | $71 \%$ |
| Vol Right, \% | $9 \%$ | $10 \%$ | $14 \%$ | $19 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 142 | 134 | 167 | 119 |
| LT Vol | 20 | 31 | 3 | 11 |
| Through Vol | 109 | 90 | 140 | 85 |
| RT Vol | 13 | 13 | 24 | 23 |
| Lane Flow Rate | 156 | 147 | 184 | 131 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.21 | 0.203 | 0.239 | 0.174 |
| Departure Headway (Hd) | 4.835 | 4.973 | 4.696 | 4.799 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 738 | 717 | 760 | 743 |
| Service Time | 2.892 | 3.034 | 2.754 | 2.86 |
| HCM Lane V/C Ratio | 0.211 | 0.205 | 0.242 | 0.176 |
| HCM Control Delay | 9.2 | 9.3 | 9.2 | 8.9 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.8 | 0.8 | 0.9 | 0.6 |


| Intersection |  |
| :--- | ---: |
| Intersection Delay, s/veh | 8.4 |
| Intersection LOS | A |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ |  |  | ${ }_{\text {¢ }}$ |  |  | ¢ |  |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 9 | 101 | 4 | 10 | 147 | 11 | 16 | 19 | 14 | 9 | 9 | 4 |
| Future Vol, veh/h | 9 | 101 | 4 | 10 | 147 | 11 | 16 | 19 | 14 | 9 | 9 | 4 |
| Peak Hour Factor | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 |
| Heavy Vehicles, \% | 11 | 19 | 0 | 0 | 12 | 0 | 0 | 16 | 7 | 44 | 11 | 25 |
| Mvmt Flow | 10 | 117 | 5 | 12 | 171 | 13 | 19 | 22 | 16 | 10 | 10 | 5 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 8.4 |  |  | 8.5 |  |  | 7.9 |  |  | 8.7 |  |  |
| HCM LOS | A |  |  | A |  |  | A |  |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $33 \%$ | $8 \%$ | $6 \%$ | $41 \%$ |
| Vol Thu, \% | $39 \%$ | $89 \%$ | $88 \%$ | $41 \%$ |
| Vol Right, \% | $29 \%$ | $4 \%$ | $7 \%$ | $18 \%$ |
| Sign Control | 49 | 114 | 168 | 22 |
| Traffic Vol by Lane | 16 | 9 | 10 | 9 |
| LT Vol | 19 | 101 | 147 | 9 |
| Through Vol | 14 | 4 | 11 | 4 |
| RT Vol | 57 | 133 | 195 | 26 |
| Lane Flow Rate | 1 | 1 | 1 | 1 |
| Geometry Grp | 0.072 | 0.165 | 0.229 | 0.039 |
| Degree of Util (X) | 4.561 | 4.486 | 4.22 | 5.427 |
| Departure Headway (Hd) | Yes | Yes | Yes | Yes |
| Convergence, Y/N | 787 | 802 | 854 | 661 |
| Cap | 2.58 | 2.5 | 2.234 | 3.447 |
| Service Time | 0.072 | 0.166 | 0.228 | 0.039 |
| HCM Lane V/C Ratio | 7.9 | 8.4 | 8.5 | 8.7 |
| HCM Control Delay | A | A | A | A |
| HCM Lane LOS | 0.2 | 0.6 | 0.9 | 0.1 |

Capacity Analysis Summary Sheets Existing Weekday Evening Peak Hour Conditions

|  | 4 | $\rightarrow$ | $\checkmark$ | 7 |  |  | 4 | $\dagger$ | \% | $v$ |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1}$ | 中 ${ }^{\text {a }}$ |  | ${ }^{1}$ | 中 ${ }^{\text {a }}$ |  |  | $\ddagger$ |  |  | \& |  |
| Traffic Volume (vph) | 40 | 572 | 73 | 89 | 675 | 39 | 26 | 123 | 68 | 20 | 144 | 43 |
| Future Volume (vph) | 40 | 572 | 73 | 89 | 675 | 39 | 26 | 123 | 68 | 20 | 144 | 43 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 10 | 10 | 10 | 10 | 10 | 10 | 12 | 16 | 12 | 12 | 16 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 115 |  | 0 | 160 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 80 |  |  | 90 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 1.00 |  |  |  |  |  | 0.99 |  |  | 1.00 |  |
| Frt |  | 0.983 |  |  | 0.992 |  |  | 0.958 |  |  | 0.972 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  |  | 0.994 |  |  | 0.995 |  |
| Satd. Flow (prot) | 1604 | 3069 | 0 | 1507 | 2880 | 0 | 0 | 1759 | 0 | 0 | 1814 | 0 |
| Flt Permitted | 0.289 |  |  | 0.325 |  |  |  | 0.947 |  |  | 0.959 |  |
| Satd. Flow (perm) | 488 | 3069 | 0 | 516 | 2880 | 0 | 0 | 1676 | 0 | 0 | 1748 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 34 |  |  | 14 |  |  | 37 |  |  | 22 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 2690 |  |  | 679 |  |  | 1667 |  |  | 676 |  |
| Travel Time (s) |  | 61.1 |  |  | 15.4 |  |  | 37.9 |  |  | 15.4 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  | 2 |  | 5 | 5 |  | 2 |
| Confl. Bikes (\#/hr) |  |  | 2 |  |  |  |  |  | 1 |  |  | 2 |
| Peak Hour Factor | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 5\% | 8\% | 5\% | 10\% | 16\% | 0\% | 8\% | 3\% | 0\% | 5\% | 3\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 4 | 4 | 4 | 4 | 4 | 4 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 47 | 750 | 0 | 103 | 830 | 0 | 0 | 252 | 0 | 0 | 240 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Permitted Phases | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |  |
| Detector Phase | 2 | 2 |  | 6 | 6 |  | 8 | 8 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 40.0 | 40.0 |  | 40.0 | 40.0 |  | 25.0 | 25.0 |  | 25.0 | 25.0 |  |
| Total Split (s) | 40.0 | 40.0 |  | 40.0 | 40.0 |  | 25.0 | 25.0 |  | 25.0 | 25.0 |  |
| Total Split (\%) | 61.5\% | 61.5\% |  | 61.5\% | 61.5\% |  | 38.5\% | 38.5\% |  | 38.5\% | 38.5\% |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  |  | 4.0 |  |  | 4.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | Max | Max |  | Max | Max |  | Max | Max |  | Max | Max |  |
| Act Effct Green (s) | 36.0 | 36.0 |  | 36.0 | 36.0 |  |  | 21.0 |  |  | 21.0 |  |
| Actuated g/C Ratio | 0.55 | 0.55 |  | 0.55 | 0.55 |  |  | 0.32 |  |  | 0.32 |  |



Splits and Phases: 1: Wallace Street \& Pershing Road


|  | $\rightarrow$ |  | 1 |  | 4 | $p$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 中 ${ }^{\text {a }}$ |  | ${ }^{4}$ | 44 | M |  |
| Traffic Volume (vph) | 647 | 13 | 26 | 774 | 29 | 18 |
| Future Volume (vph) | 647 | 13 | 26 | 774 | 29 | 18 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 2000 | 1900 | 1900 |
| Lane Width (ft) | 10 | 10 | 10 | 10 | 16 | 12 |
| Grade (\%) | 0\% |  |  | 0\% | 0\% |  |
| Storage Length (ft) |  | 0 | 115 |  | 0 | 0 |
| Storage Lanes |  | 0 | 1 |  | 1 | 0 |
| Taper Length (ft) |  |  | 80 |  | 25 |  |
| Lane Util. Factor | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  | 0.99 |  |
| Frt | 0.997 |  |  |  | 0.949 |  |
| Flt Protected |  |  | 0.950 |  | 0.970 |  |
| Satd. Flow (prot) | 3090 | 0 | 1167 | 3059 | 1733 | 0 |
| Flt Permitted |  |  | 0.315 |  | 0.970 |  |
| Satd. Flow (perm) | 3090 | 0 | 387 | 3059 | 1733 | 0 |
| Right Turn on Red |  | Yes |  |  |  | Yes |
| Satd. Flow (RTOR) | 4 |  |  |  | 20 |  |
| Link Speed (mph) | 30 |  |  | 30 | 30 |  |
| Link Distance (ft) | 679 |  |  | 2104 | 1670 |  |
| Travel Time (s) | 15.4 |  |  | 47.8 | 38.0 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  | 5 |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 8\% | 0\% | 42\% | 15\% | 0\% | 6\% |
| Bus Blockages (\#/hr) | 4 | 4 | 4 | 4 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  | 0 | 0 |
| Mid-Block Traffic (\%) | 0\% |  |  | 0\% | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |
| Lane Group Flow (vph) | 742 | 0 | 29 | 870 | 53 | 0 |
| Turn Type | NA |  | Perm | NA | Prot |  |
| Protected Phases | 2 |  |  | 6 | 8 |  |
| Permitted Phases |  |  | 6 |  |  |  |
| Detector Phase | 2 |  | 6 | 6 | 8 |  |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 |  | 5.0 | 5.0 | 5.0 |  |
| Minimum Split (s) | 37.0 |  | 37.0 | 37.0 | 28.0 |  |
| Total Split (s) | 37.0 |  | 37.0 | 37.0 | 28.0 |  |
| Total Split (\%) | 56.9\% |  | 56.9\% | 56.9\% | 43.1\% |  |
| Yellow Time (s) | 3.0 |  | 3.0 | 3.0 | 3.0 |  |
| All-Red Time (s) | 1.0 |  | 1.0 | 1.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 |  | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time (s) | 4.0 |  | 4.0 | 4.0 | 4.0 |  |
| Lead/Lag |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |
| Recall Mode | Max |  | Max | Max | Max |  |
| Act Effct Green (s) | 33.0 |  | 33.0 | 33.0 | 24.0 |  |
| Actuated g/C Ratio | 0.51 |  | 0.51 | 0.51 | 0.37 |  |



Splits and Phases: 2: Normal Avenue \& Pershing Road


| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 11.2 |
| Intersection LOS | B |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | \$ |  |  | * |  |  | \$ |  |  | \& |  |
| Traffic Vol, veh/h | 34 | 163 | 24 | 9 | 141 | 28 | 19 | 86 | 12 | 32 | 117 | 77 |
| Future Vol, veh/h | 34 | 163 | 24 | 9 | 141 | 28 | 19 | 86 | 12 | 32 | 117 | 77 |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles, \% | 32 | 5 | 0 | 0 | 14 | 11 | 5 | 1 | 8 | 3 | 1 | 10 |
| Mvmt Flow | 37 | 179 | 26 | 10 | 155 | 31 | 21 | 95 | 13 | 35 | 129 | 85 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 12.4 |  |  | 10.4 |  |  | 10.1 |  |  | 11.2 |  |  |
| HCM LOS | B |  |  | B |  |  | B |  |  | B |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $16 \%$ | $15 \%$ | $5 \%$ | $14 \%$ |
| Vol Thru, \% | $74 \%$ | $74 \%$ | $79 \%$ | $52 \%$ |
| Vol Right, \% | $10 \%$ | $11 \%$ | $16 \%$ | $34 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 117 | 221 | 178 | 226 |
| LT Vol | 19 | 34 | 9 | 32 |
| Through Vol | 86 | 163 | 141 | 117 |
| RT Vol | 12 | 24 | 28 | 77 |
| Lane Flow Rate | 129 | 243 | 196 | 248 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.2 | 0.388 | 0.286 | 0.361 |
| Departure Headway (Hd) | 5.605 | 5.758 | 5.271 | 5.23 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 639 | 624 | 681 | 688 |
| Service Time | 3.646 | 3.794 | 3.309 | 3.264 |
| HCM Lane V/C Ratio | 0.202 | 0.389 | 0.288 | 0.36 |
| HCM Control Delay | 10.1 | 12.4 | 10.4 | 11.2 |
| HCM Lane LOS | B | B | B | B |
| HCM 95th-tile Q | 0.7 | 1.8 | 1.2 | 1.6 |


| Intersection |  |
| :--- | ---: |
| Intersection Delay, s/veh | 8.9 |
| Intersection LOS | A |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | ${ }_{\text {¢ }}$ |  |  | ${ }_{\text {¢ }}$ |  |  | ¢ |  |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 10 | 172 | 25 | 10 | 156 | 13 | 14 | 18 | 4 | 4 | 18 | 8 |
| Future Vol, veh/h | 10 | 172 | 25 | 10 | 156 | 13 | 14 | 18 | 4 | 4 | 18 | 8 |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles, \% | 10 | 5 | 4 | 0 | 14 | 15 | 0 | 0 | 0 | 25 | 0 | 13 |
| Mvmt Flow | 11 | 193 | 28 | 11 | 175 | 15 | 16 | 20 | 4 | 4 | 20 | 9 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 9.2 |  |  | 8.7 |  |  | 8.2 |  |  | 8.5 |  |  |
| HCM LOS | A |  |  | A |  |  | A |  |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $39 \%$ | $5 \%$ | $6 \%$ | $13 \%$ |
| Vol Thu, $\%$ | $50 \%$ | $83 \%$ | $87 \%$ | $60 \%$ |
| Vol Right, \% | $11 \%$ | $12 \%$ | $7 \%$ | $27 \%$ |
| Sign Control | 36 | 207 | 179 | 30 |
| Traffic Vol by Lane | 14 | 10 | 10 | 4 |
| LT Vol | 18 | 172 | 156 | 18 |
| Through Vol | 4 | 25 | 13 | 8 |
| RT Vol | 40 | 233 | 201 | 34 |
| Lane Flow Rate | 1 | 1 | 1 | 1 |
| Geometry Grp | 0.055 | 0.285 | 0.24 | 0.049 |
| Degree of Util (X) | 4.918 | 4.405 | 4.303 | 5.209 |
| Departure Headway (Hd) | Yes | Yes | Yes | Yes |
| Convergence, Y/N | 728 | 819 | 837 | 688 |
| Cap | 2.948 | 2.421 | 2.32 | 3.238 |
| Service Time | 0.055 | 0.284 | 0.24 | 0.049 |
| HCM Lane V/C Ratio | 8.2 | 9.2 | 8.7 | 8.5 |
| HCM Control Delay | A | A | A | A |
| HCM Lane LOS | 0.2 | 1.2 | 0.9 | 0.2 |

# Capacity Analysis Summary Sheets 

 Total Projected Weekday Morning Peak Hour Conditions|  | 4 |  | $\checkmark$ | 7 |  |  | 4 | 4 | \% | $v$ |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1}$ | 中 ${ }^{\text {a }}$ |  | ${ }^{1}$ | 中 ${ }^{\text {a }}$ |  |  | \& |  |  | \$ |  |
| Traffic Volume (vph) | 40 | 584 | 78 | 92 | 574 | 35 | 39 | 143 | 54 | 30 | 106 | 36 |
| Future Volume (vph) | 40 | 584 | 78 | 92 | 574 | 35 | 39 | 143 | 54 | 30 | 106 | 36 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 10 | 10 | 10 | 10 | 10 | 10 | 12 | 16 | 12 | 12 | 16 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 115 |  | 0 | 160 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 80 |  |  | 90 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Frt |  | 0.982 |  |  | 0.991 |  |  | 0.969 |  |  | 0.972 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  |  | 0.992 |  |  | 0.991 |  |
| Satd. Flow (prot) | 1491 | 2704 | 0 | 1579 | 2846 | 0 | 0 | 1677 | 0 | 0 | 1762 | 0 |
| Flt Permitted | 0.367 |  |  | 0.339 |  |  |  | 0.930 |  |  | 0.919 |  |
| Satd. Flow (perm) | 574 | 2704 | 0 | 563 | 2846 | 0 | 0 | 1571 | 0 | 0 | 1634 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 36 |  |  | 15 |  |  | 25 |  |  | 22 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 2690 |  |  | 679 |  |  | 382 |  |  | 676 |  |
| Travel Time (s) |  | 61.1 |  |  | 15.4 |  |  | 8.7 |  |  | 15.4 |  |
| Confl. Peds. (\#/hr) | 4 |  | 1 | 1 |  | 4 | 6 |  |  |  |  | 6 |
| Confl. Bikes (\#/hr) |  |  | 2 |  |  |  |  |  | 1 |  |  | 2 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 13\% | 25\% | 0\% | 5\% | 17\% | 3\% | 10\% | 3\% | 24\% | 0\% | 8\% | 3\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 4 | 4 | 4 | 4 | 4 | 4 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 43 | 720 | 0 | 100 | 662 | 0 | 0 | 256 | 0 | 0 | 187 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Permitted Phases | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |  |
| Detector Phase | 2 | 2 |  | 6 | 6 |  | 8 | 8 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 40.0 | 40.0 |  | 40.0 | 40.0 |  | 25.0 | 25.0 |  | 25.0 | 25.0 |  |
| Total Split (s) | 40.0 | 40.0 |  | 40.0 | 40.0 |  | 25.0 | 25.0 |  | 25.0 | 25.0 |  |
| Total Split (\%) | 61.5\% | 61.5\% |  | 61.5\% | 61.5\% |  | 38.5\% | 38.5\% |  | 38.5\% | 38.5\% |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  |  | 4.0 |  |  | 4.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | Max | Max |  | Max | Max |  | Max | Max |  | Max | Max |  |
| Act Effct Green (s) | 36.0 | 36.0 |  | 36.0 | 36.0 |  |  | 21.0 |  |  | 21.0 |  |
| Actuated g/C Ratio | 0.55 | 0.55 |  | 0.55 | 0.55 |  |  | 0.32 |  |  | 0.32 |  |



Splits and Phases: 1: Wallace Street \& Pershing Road


|  | $\rightarrow$ |  | $\checkmark$ |  | 4 | 7 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 中 ${ }^{\text {a }}$ |  | ${ }^{1}$ | 44 | M |  |
| Traffic Volume (vph) | 652 | 16 | 27 | 679 | 22 | 25 |
| Future Volume (vph) | 652 | 16 | 27 | 679 | 22 | 25 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 2000 | 1900 | 1900 |
| Lane Width (ft) | 10 | 10 | 10 | 10 | 16 | 12 |
| Grade (\%) | 0\% |  |  | 0\% | 0\% |  |
| Storage Length (ft) |  | 0 | 115 |  | 0 | 0 |
| Storage Lanes |  | 0 | 1 |  | 1 | 0 |
| Taper Length (ft) |  |  | 80 |  | 25 |  |
| Lane Util. Factor | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |
| Frt | 0.996 |  |  |  | 0.929 |  |
| Flt Protected |  |  | 0.950 |  | 0.977 |  |
| Satd. Flow (prot) | 2681 | 0 | 1246 | 3059 | 1557 | 0 |
| Flt Permitted |  |  | 0.327 |  | 0.977 |  |
| Satd. Flow (perm) | 2681 | 0 | 429 | 3059 | 1557 | 0 |
| Right Turn on Red |  | Yes |  |  |  | Yes |
| Satd. Flow (RTOR) | 5 |  |  |  | 27 |  |
| Link Speed (mph) | 30 |  |  | 30 | 30 |  |
| Link Distance (ft) | 679 |  |  | 2104 | 258 |  |
| Travel Time (s) | 15.4 |  |  | 47.8 | 5.9 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 24\% | 31\% | 33\% | 15\% | 5\% | 20\% |
| Bus Blockages (\#/hr) | 4 | 4 | 4 | 4 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  | 0 | 0 |
| Mid-Block Traffic (\%) | 0\% |  |  | 0\% | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |
| Lane Group Flow (vph) | 718 | 0 | 29 | 730 | 51 | 0 |
| Turn Type | NA |  | Perm | NA | Prot |  |
| Protected Phases | 2 |  |  | 6 | 8 |  |
| Permitted Phases |  |  | 6 |  |  |  |
| Detector Phase | 2 |  | 6 | 6 | 8 |  |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 |  | 5.0 | 5.0 | 5.0 |  |
| Minimum Split (s) | 37.0 |  | 37.0 | 37.0 | 28.0 |  |
| Total Split (s) | 37.0 |  | 37.0 | 37.0 | 28.0 |  |
| Total Split (\%) | 56.9\% |  | 56.9\% | 56.9\% | 43.1\% |  |
| Yellow Time (s) | 3.0 |  | 3.0 | 3.0 | 3.0 |  |
| All-Red Time (s) | 1.0 |  | 1.0 | 1.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 |  | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time (s) | 4.0 |  | 4.0 | 4.0 | 4.0 |  |
| Lead/Lag |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |
| Recall Mode | Max |  | Max | Max | Max |  |
| Act Effct Green (s) | 33.0 |  | 33.0 | 33.0 | 24.0 |  |
| Actuated g/C Ratio | 0.51 |  | 0.51 | 0.51 | 0.37 |  |



Splits and Phases: 2: Normal Avenue \& Pershing Road


| Intersection |  |
| :--- | ---: |
| Intersection Delay, s/veh $\quad 9.4$ |  |
| Intersection LOS | A |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | \$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 40 | 96 | 13 | 3 | 144 | 32 | 21 | 112 | 13 | 12 | 88 | 26 |
| Future Vol, veh/h | 40 | 96 | 13 | 3 | 144 | 32 | 21 | 112 | 13 | 12 | 88 | 26 |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles, \% | 8 | 24 | 8 | 0 | 13 | 0 | 0 | 3 | 0 | 0 | 9 | 31 |
| Mumt Flow | 44 | 105 | 14 | 3 | 158 | 35 | 23 | 123 | 14 | 13 | 97 | 29 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 9.6 |  |  | 9.5 |  |  | 9.4 |  |  | 9.1 |  |  |
| HCM LOS | A |  |  | A |  |  | A |  |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $14 \%$ | $27 \%$ | $2 \%$ | $10 \%$ |
| Vol Thru, \% | $77 \%$ | $64 \%$ | $80 \%$ | $70 \%$ |
| Vol Right, \% | $9 \%$ | $9 \%$ | $18 \%$ | $21 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 146 | 149 | 179 | 126 |
| LT Vol | 21 | 40 | 3 | 12 |
| Through Vol | 112 | 96 | 144 | 88 |
| RT Vol | 13 | 13 | 32 | 26 |
| Lane Flow Rate | 160 | 164 | 197 | 138 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.219 | 0.228 | 0.259 | 0.188 |
| Departure Headway (Hd) | 4.924 | 5.01 | 4.736 | 4.876 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 724 | 711 | 751 | 730 |
| Service Time | 2.996 | 3.08 | 2.804 | 2.949 |
| HCM Lane V/C Ratio | 0.221 | 0.231 | 0.262 | 0.189 |
| HCM Control Delay | 9.4 | 9.6 | 9.5 | 9.1 |
| HCM Lane LOS | A | A | A | A |
| HCM 95th-tile Q | 0.8 | 0.9 | 1 | 0.7 |


| Intersection |  |
| :--- | ---: |
| Intersection Delay, s/veh | 8.7 |
| Intersection LOS | A |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | ${ }_{\text {¢ }}$ |  |  | ${ }_{\text {¢ }}$ |  |  | ¢ |  |  | \$ |  |
| Traffic Vol, veh/h | 12 | 105 | 4 | 10 | 159 | 14 | 16 | 20 | 14 | 9 | 9 | 4 |
| Future Vol, veh/h | 12 | 105 | 4 | 10 | 159 | 14 | 16 | 20 | 14 | 9 | 9 | 4 |
| Peak Hour Factor | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 |
| Heavy Vehicles, \% | 25 | 19 | 0 | 0 | 11 | 7 | 0 | 15 | 7 | 44 | 11 | 25 |
| Mvmt Flow | 14 | 122 | 5 | 12 | 185 | 16 | 19 | 23 | 16 | 10 | 10 | 5 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 8.9 |  |  | 8.7 |  |  | 8 |  |  | 8.8 |  |  |
| HCM LOS | A |  |  | A |  |  | A |  |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $32 \%$ | $10 \%$ | $5 \%$ | $41 \%$ |
| Vol Thu, $\%$ | $40 \%$ | $87 \%$ | $87 \%$ | $41 \%$ |
| Vol Right, $\%$ | $28 \%$ | $3 \%$ | $8 \%$ | $18 \%$ |
| Sign Control | 50 | Stop | Stop | Stop |
| Traffic Vol by Lane | 16 | 121 | 18 | 10 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.2 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | $\mathbf{F}$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 3 | 9 | 227 | 15 | 64 | 212 |
| Future Vol, veh/h | 3 | 9 | 227 | 15 | 64 | 212 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, \% | 0 | 0 | 10 | 0 | 0 | 6 |
| Mvmt Flow | 3 | 9 | 239 | 16 | 67 | 223 |


| Major/Minor M | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 604 | 247 | 0 | 0 | 255 | 0 |
| Stage 1 | 247 | - | - | - | - | - |
| Stage 2 | 357 | - | - | - | - | - |
| Critical Hdwy | 6.4 | 6.2 | - | - | 4.1 | - |
| Critical Hdwy Stg 1 | 5.4 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.4 | - | - | - | - | - |
| Follow-up Hdwy | 3.5 | 3.3 | - | - | 2.2 | - |
| Pot Cap-1 Maneuver | 465 | 797 | - | - | 1322 | - |
| Stage 1 | 799 | - | - | - | - | - |
| Stage 2 | 713 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 438 | 797 | - | - | 1322 | - |
| Mov Cap-2 Maneuver | 438 | - | - | - | - | - |
| Stage 1 | 799 | - | - | - | - | - |
| Stage 2 | 672 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 10.6 |  | 0 |  | 1.8 |  |
| HCM LOS | B |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 661 | 1322 | - |
| HCM Lane V/C Ratio |  | - | - | 0.019 | 0.051 | - |
| HCM Control Delay (s) |  | - | - | 10.6 | 7.9 | 0 |
| HCM Lane LOS |  | - | - | B | A | A |
| HCM 95th \%tile Q(veh) |  | - | - | 0.1 | 0.2 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



## Capacity Analysis Summary Sheets

Total Projected Weekday Evening Peak Hour Conditions

|  | 4 | $\rightarrow$ | $\checkmark$ | 7 |  |  | 4 | 4 | \% | $v$ |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1}$ | 中 ${ }^{\text {a }}$ |  | ${ }^{1}$ | 中 ${ }^{\text {a }}$ |  |  | \& |  |  | \$ |  |
| Traffic Volume (vph) | 41 | 590 | 80 | 96 | 699 | 40 | 57 | 127 | 96 | 21 | 148 | 44 |
| Future Volume (vph) | 41 | 590 | 80 | 96 | 699 | 40 | 57 | 127 | 96 | 21 | 148 | 44 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 10 | 10 | 10 | 10 | 10 | 10 | 12 | 16 | 12 | 12 | 16 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 115 |  | 0 | 160 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 80 |  |  | 90 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 1.00 |  |  |  |  |  | 0.99 |  |  | 1.00 |  |
| Frt |  | 0.982 |  |  | 0.992 |  |  | 0.954 |  |  | 0.972 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  |  | 0.990 |  |  | 0.995 |  |
| Satd. Flow (prot) | 1604 | 3066 | 0 | 1521 | 2880 | 0 | 0 | 1751 | 0 | 0 | 1814 | 0 |
| Flt Permitted | 0.277 |  |  | 0.312 |  |  |  | 0.902 |  |  | 0.951 |  |
| Satd. Flow (perm) | 468 | 3066 | 0 | 499 | 2880 | 0 | 0 | 1595 | 0 | 0 | 1733 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 36 |  |  | 14 |  |  | 43 |  |  | 21 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 2690 |  |  | 679 |  |  | 382 |  |  | 676 |  |
| Travel Time (s) |  | 61.1 |  |  | 15.4 |  |  | 8.7 |  |  | 15.4 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  | 2 |  | 6 | 6 |  | 2 |
| Confl. Bikes (\#/hr) |  |  | 2 |  |  |  |  |  | 1 |  |  | 2 |
| Peak Hour Factor | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 |
| Growth Factor | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 5\% | 8\% | 5\% | 9\% | 16\% | 0\% | 4\% | 3\% | 0\% | 5\% | 3\% | 2\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 4 | 4 | 4 | 4 | 4 | 4 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 48 | 779 | 0 | 112 | 860 | 0 | 0 | 326 | 0 | 0 | 247 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Permitted Phases | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |  |
| Detector Phase | 2 | 2 |  | 6 | 6 |  | 8 | 8 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 40.0 | 40.0 |  | 40.0 | 40.0 |  | 25.0 | 25.0 |  | 25.0 | 25.0 |  |
| Total Split (s) | 40.0 | 40.0 |  | 40.0 | 40.0 |  | 25.0 | 25.0 |  | 25.0 | 25.0 |  |
| Total Split (\%) | 61.5\% | 61.5\% |  | 61.5\% | 61.5\% |  | 38.5\% | 38.5\% |  | 38.5\% | 38.5\% |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  |  | 4.0 |  |  | 4.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | Max | Max |  | Max | Max |  | Max | Max |  | Max | Max |  |
| Act Effct Green (s) | 36.0 | 36.0 |  | 36.0 | 36.0 |  |  | 21.0 |  |  | 21.0 |  |
| Actuated g/C Ratio | 0.55 | 0.55 |  | 0.55 | 0.55 |  |  | 0.32 |  |  | 0.32 |  |



Splits and Phases: 1: Wallace Street \& Pershing Road




Splits and Phases: 2: Normal Avenue \& Pershing Road


| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 11.7 |
| Intersection LOS | B |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 37 | 168 | 25 | 9 | 147 | 30 | 20 | 89 | 12 | 39 | 121 | 87 |
| Future Vol, veh/h | 37 | 168 | 25 | 9 | 147 | 30 | 20 | 89 | 12 | 39 | 121 | 87 |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles, \% | 30 | 5 | 0 | 0 | 15 | 10 | 5 | 1 | 8 | 3 | 1 | 9 |
| Mumt Flow | 41 | 185 | 27 | 10 | 162 | 33 | 22 | 98 | 13 | 43 | 133 | 96 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 12.9 |  |  | 10.8 |  |  | 10.3 |  |  | 11.9 |  |  |
| HCM LOS | B |  |  | B |  |  | B |  |  | B |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $17 \%$ | $16 \%$ | $5 \%$ | $16 \%$ |
| Vol Thru, \% | $74 \%$ | $73 \%$ | $79 \%$ | $49 \%$ |
| Vol Right, \% | $10 \%$ | $11 \%$ | $16 \%$ | $35 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 121 | 230 | 186 | 247 |
| LT Vol | 20 | 37 | 9 | 39 |
| Through Vol | 89 | 168 | 147 | 121 |
| RT Vol | 12 | 25 | 30 | 87 |
| Lane Flow Rate | 133 | 253 | 204 | 271 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.212 | 0.41 | 0.306 | 0.4 |
| Departure Headway (Hd) | 5.731 | 5.844 | 5.392 | 5.311 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 625 | 614 | 664 | 676 |
| Service Time | 3.782 | 3.886 | 3.437 | 3.354 |
| HCM Lane V/C Ratio | 0.213 | 0.412 | 0.307 | 0.401 |
| HCM Control Delay | 10.3 | 12.9 | 10.8 | 11.9 |
| HCM Lane LOS | B | B | B | B |
| HCM 95th-tile Q | 0.8 | 2 | 1.3 | 1.9 |


| Intersection |  |
| :--- | :---: |
| Intersection Delay, s/veh $\quad 9$ |  |
| Intersection LOS | A |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ |  |  | ${ }_{\text {¢ }}$ |  |  | ¢ |  |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 10 | 183 | 26 | 10 | 162 | 13 | 14 | 19 | 4 | 7 | 19 | 10 |
| Future Vol, veh/h | 10 | 183 | 26 | 10 | 162 | 13 | 14 | 19 | 4 | 7 | 19 | 10 |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles, \% | 10 | 4 | 4 | 0 | 14 | 15 | 0 | 0 | 0 | 29 | 0 | 20 |
| Mvmt Flow | 11 | 206 | 29 | 11 | 182 | 15 | 16 | 21 | 4 | 8 | 21 | 11 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 9.4 |  |  | 8.8 |  |  | 8.3 |  |  | 8.7 |  |  |
| HCM LOS | A |  |  | A |  |  | A |  |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $38 \%$ | $5 \%$ | $5 \%$ | $19 \%$ |
| Vol Thu, \% | $51 \%$ | $84 \%$ | $88 \%$ | $53 \%$ |
| Vol Right, \% | $11 \%$ | $12 \%$ | $7 \%$ | $28 \%$ |
| Sign Control | 37 | 219 | 185 | 36 |
| Traffic Vol by Lane | 14 | 10 | 10 | 7 |
| LT Vol | 19 | 183 | 162 | 19 |
| Through Vol | 4 | 26 | 13 | 10 |
| RT Vol | 42 | 246 | 208 | 40 |
| Lane Flow Rate | 1 | 1 | 1 | 1 |
| Geometry Grp | 0.058 | 0.303 | 0.251 | 0.06 |
| Degree of Util (X) | 4.981 | 4.439 | 4.345 | 5.335 |
| Departure Headway (Hd) | Yes | Yes | Yes | Yes |
| Convergence, Y/N | 719 | 812 | 827 | 671 |
| Cap | 3.013 | 2.46 | 2.366 | 3.369 |
| Service Time | 0.058 | 0.303 | 0.252 | 0.06 |
| HCM Lane V/C Ratio | 8.3 | 9.4 | 8.8 | 8.7 |
| HCM Control Delay | A | A | A | A |
| HCM Lane LOS | 0.2 | 1.3 | 1 | 0.2 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.3 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | $\mathbf{F}$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 14 | 56 | 224 | 3 | 9 | 315 |
| Future Vol, veh/h | 14 | 56 | 224 | 3 | 9 | 315 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, \% | 0 | 0 | 3 | 0 | 0 | 5 |
| Mvmt Flow | 15 | 59 | 236 | 3 | 9 | 332 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



